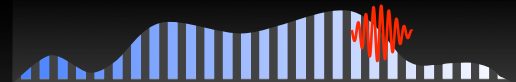


Optical frequency combs for stable radiation in the microwave, terahertz and optical domains

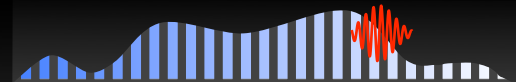


Qudsia Quraishi
Department of Physics, University of Colorado
Time and Frequency Division,
National Institute of Standards and Technology
Boulder, CO



stabilized frequency combs from mode-locked femtosecond lasers provide new opportunities for....

- § optical frequency metrology
- § optical clocks
- § measuring distance
- § time & frequency transfer
- § laboratory tests of fundamental physics
- § carrier-envelope phase control (key technology for attosecond science)
- § femtosecond pulse synthesis & arbitrary optical waveform generation
- § generation of ultralow noise microwaves
- § new spectroscopic techniques
- § harmonic generation
- § coherent control
- § spread-spectrum secure communications
- § part of a Nobel Prize!



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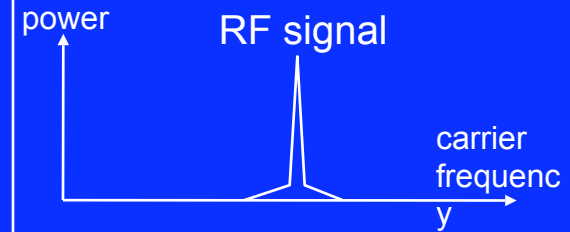
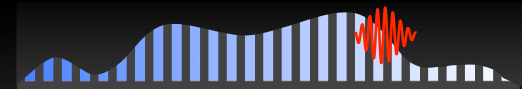


Jan Hall



Ted Hänsch

microwave frequency synthesizers



specifications

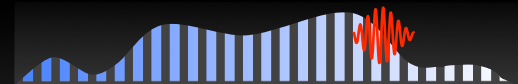
250 kHz – 20 GHz +
low phase noise

10, 007, 482, 279 GHz



Agilent E8257D frequency synthesizer

microwave frequency synthesizers

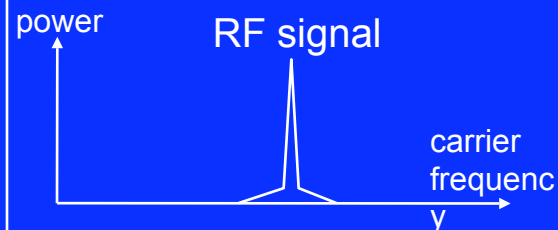


user defined:

- (a) frequency
- (b) amplitude
- (c) noise (to some extent)

uses:

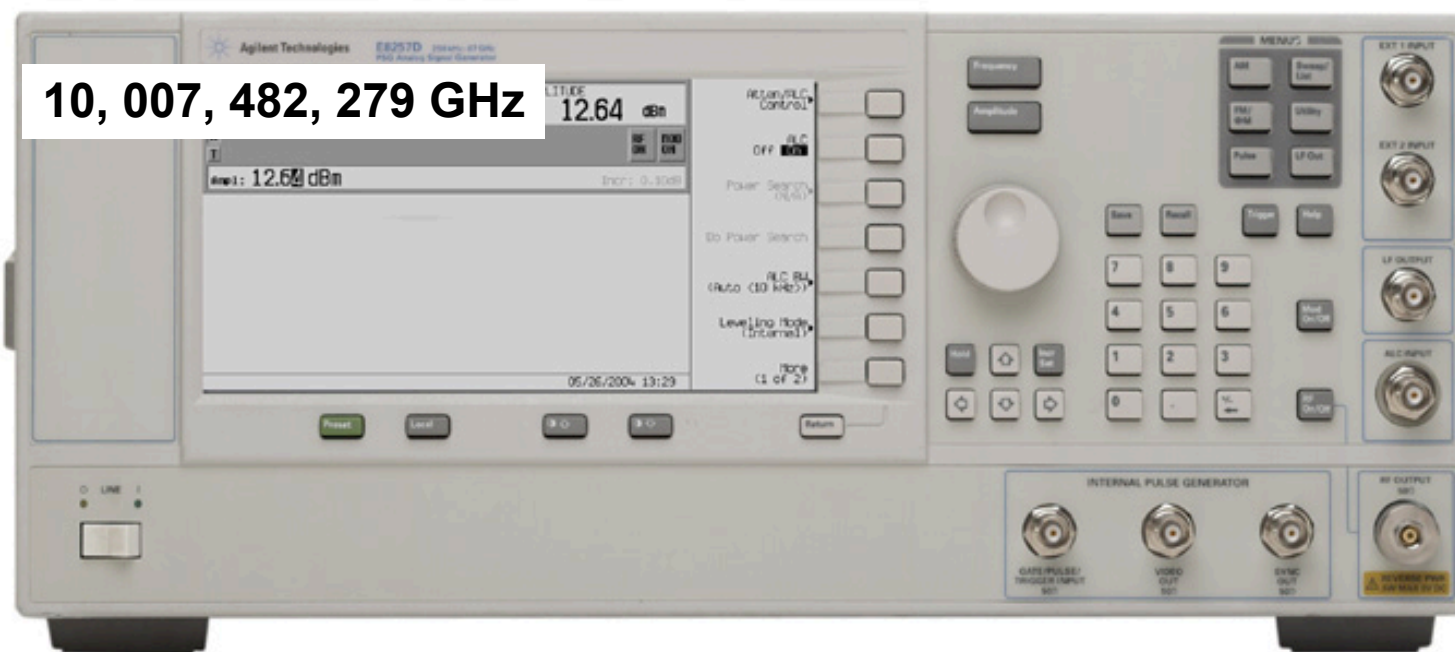
- (i) references
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- (iii) microwave electronics



specifications

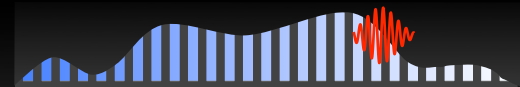
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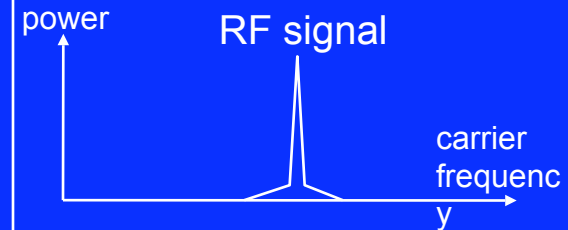


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specifications

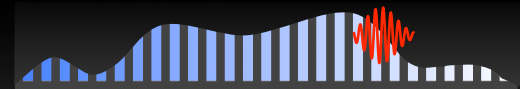
250 kHz – 20 GHz +
low phase noise

10, 007, 482, 279 GHz

pretty good...
1 part in 10^{10}



Agilent E8257D frequency synthesizer



idea: optical frequency synthesizer

FREQUENCY:

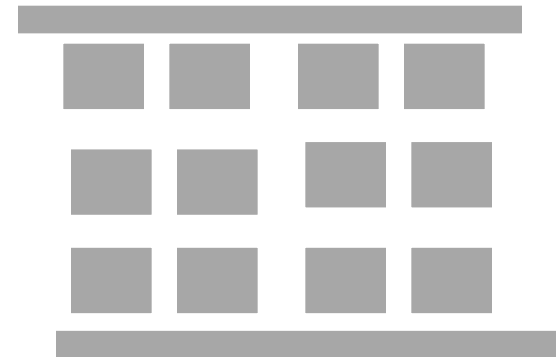
352, 567, 323, 826, 841 Hz

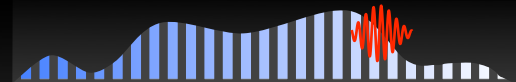
POWER: 2 nW

NOISE: -100 dBc/Hz at 1 Hz

port 1

port 2





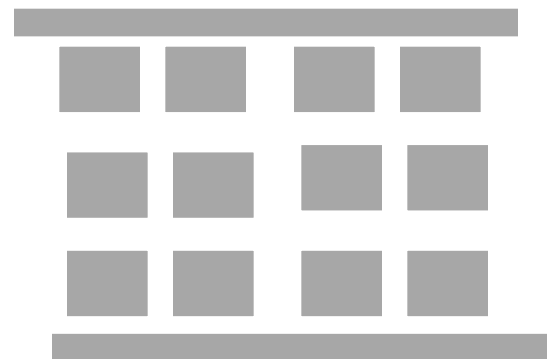
idea: optical frequency synthesizer

FREQUENCY:

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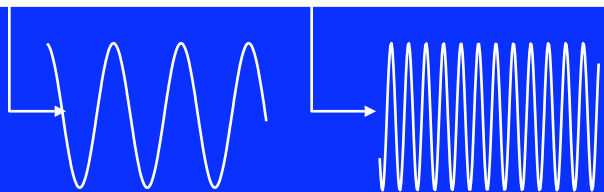
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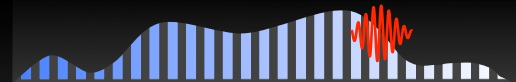


port 1

port 2



850 nm (352 THz)



idea: optical frequency synthesizer

FREQUENCY:

352, 567, 323, 826, 841 Hz

POWER: 2 nW

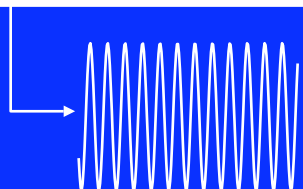
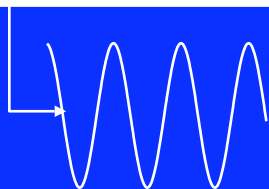
NOISE: -100 dBc/Hz

really good...

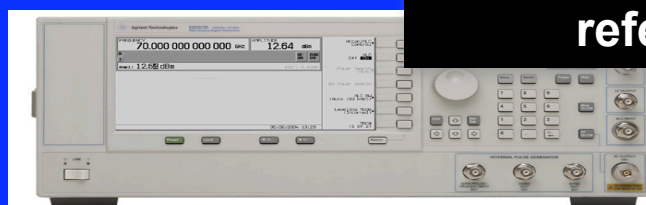
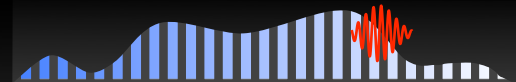
1 part in 10^{15} !

port 1

port 2



850 nm (352 THz)



**microwave or optical
reference**

atoms
or molecules

stable
cavity

your are only as good
as your reference

idea: optical frequency synthesizer

FREQUENCY:

352, 567, 323, 826, 841 Hz

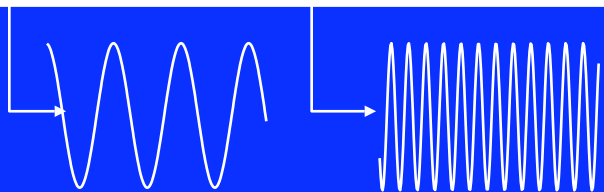
POWER: 2 nW

NOISE: -100 dBc/Hz

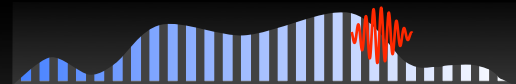
**really good...
1 part in 10^{15} !**

port 1

port 2



850 nm (352 THz)

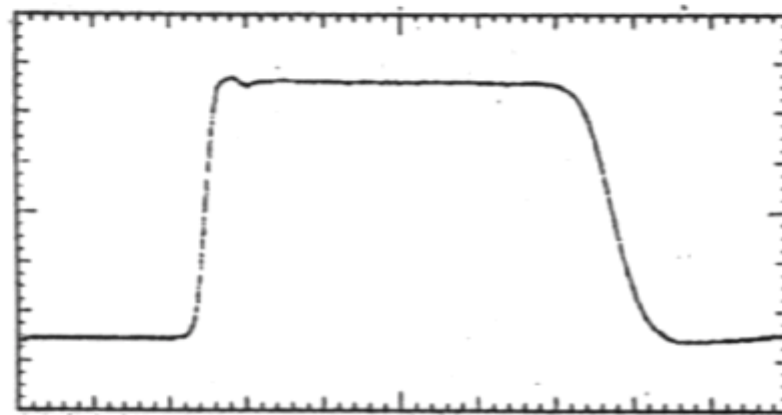


Picosecond Pulse Labs 2600C



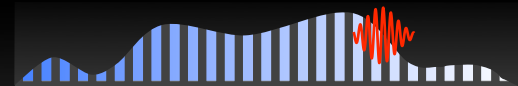
specifications

rise time 250 ps
dynamic range 70 dB
pulse duration 1 ns to 100 nsec
repetition rate 1 Hz – 100 kHz



10 V/div and 1 ns/div
Positive Pulse

optical pulse generators?



pulse duration:

20 fs

repetition rate:

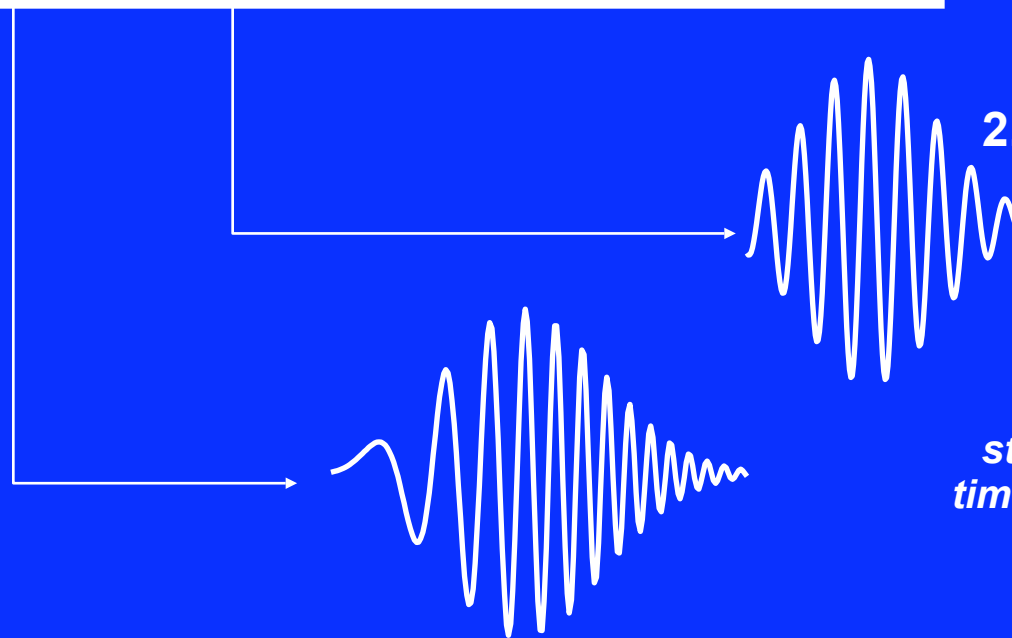
1 GHz

phase profile:

20 fs^2

port 1

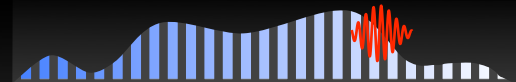
port 2



each cycle:
2.5 fs (800 nm)

*stabilized combs have subfs
timing jitter from pulse-to-pulse*

optical pulse generators?



pulse duration:

20 fs

repetition rate:

1 GHz

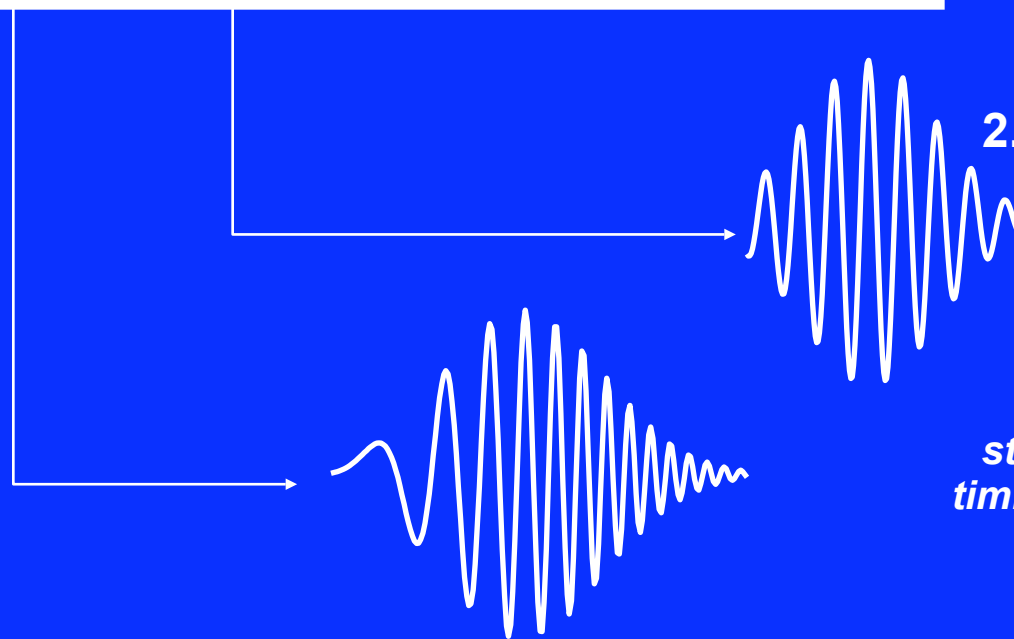
phase profile:

20 fs^2

**SUB FEMTOSECOND
phase stability !**

port 1

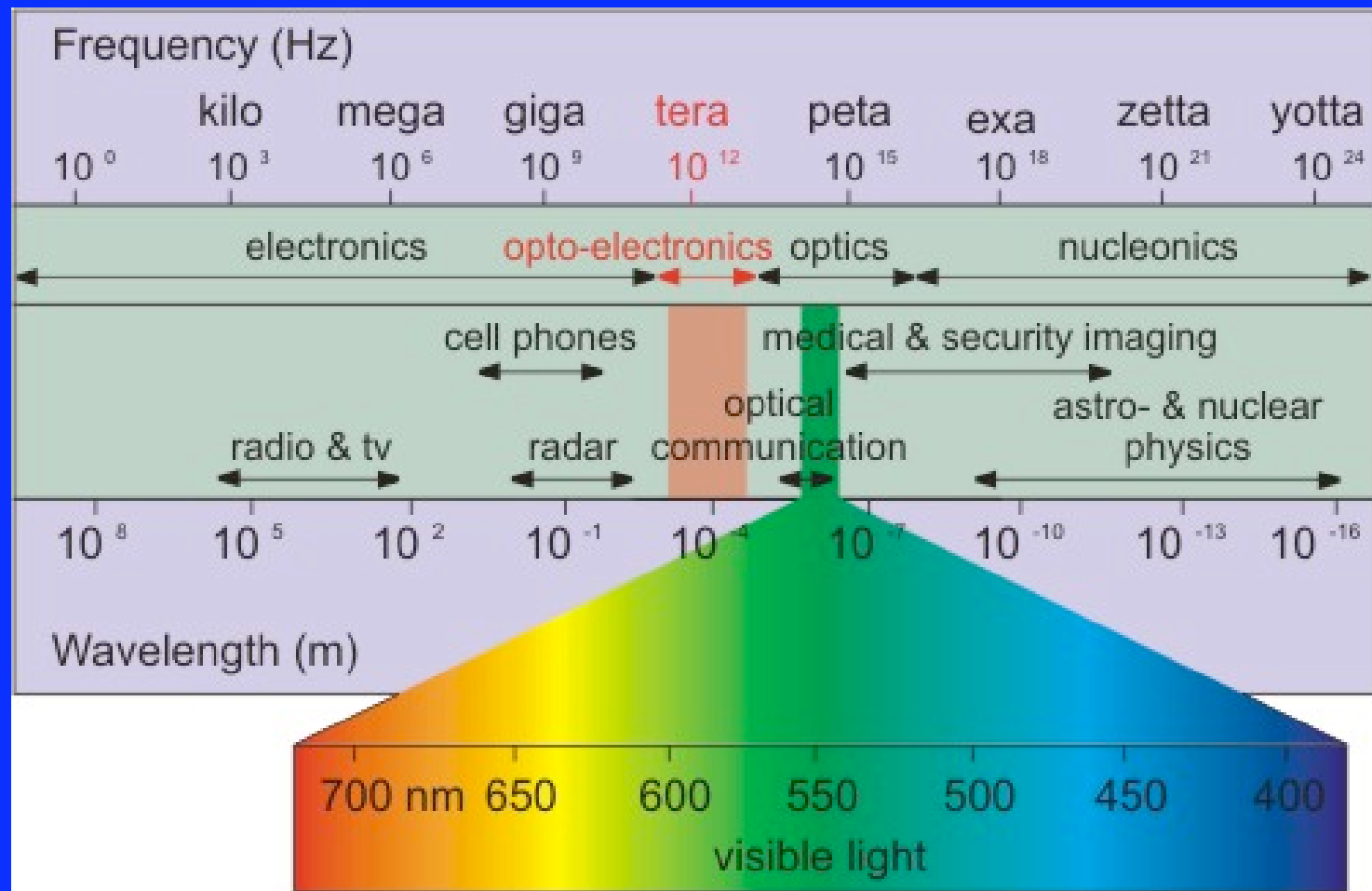
port 2



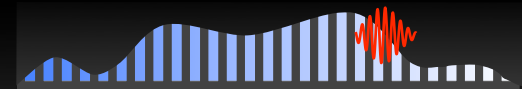
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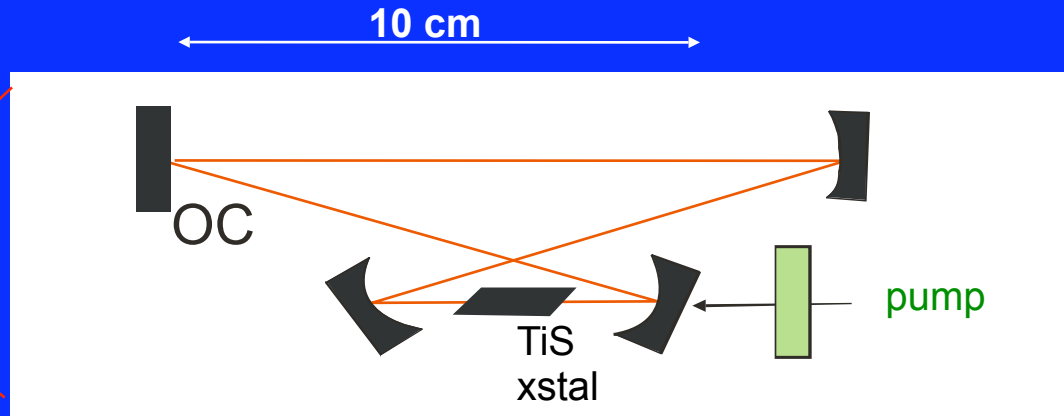
frequency combs are extending our ideas about user-defined frequency sources, *from the microwave to the optical*



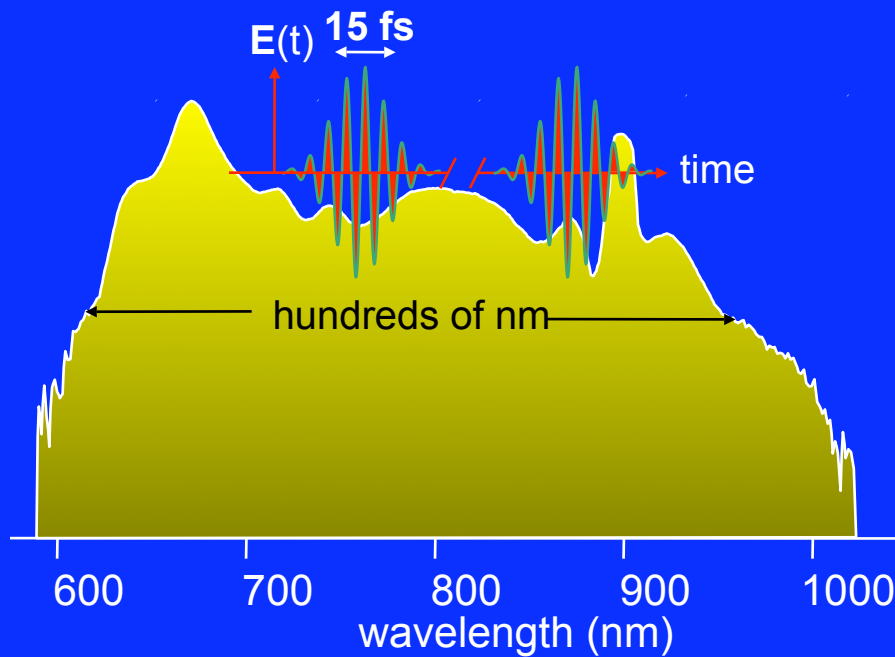
optical spectrum is discrete, appearing every fsep



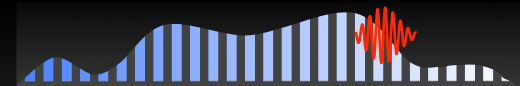
kerr lens modelocked
frequency comb



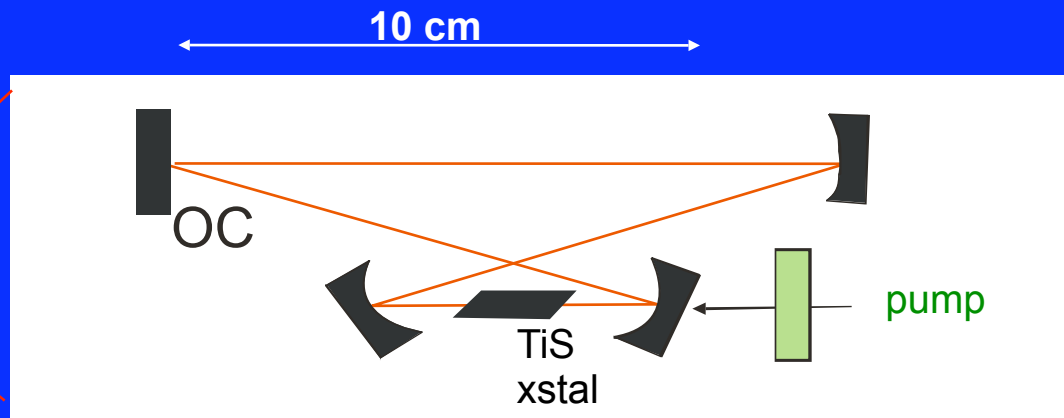
600 mW modelocked power
1 GHz repetition rate pulses
8.5 W pump beam at 532 nm



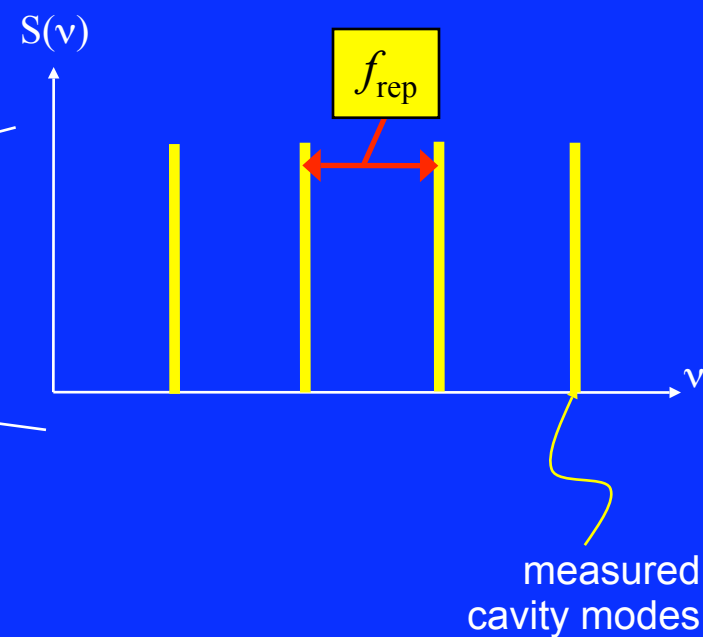
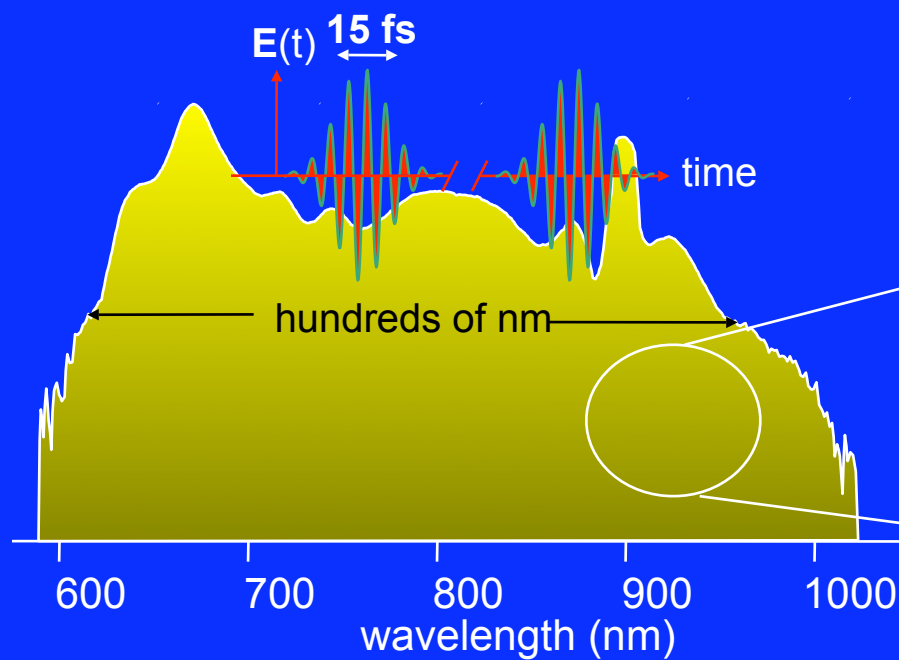
optical spectrum is discrete, appearing every f_{rep}



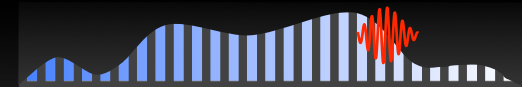
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frequency comb



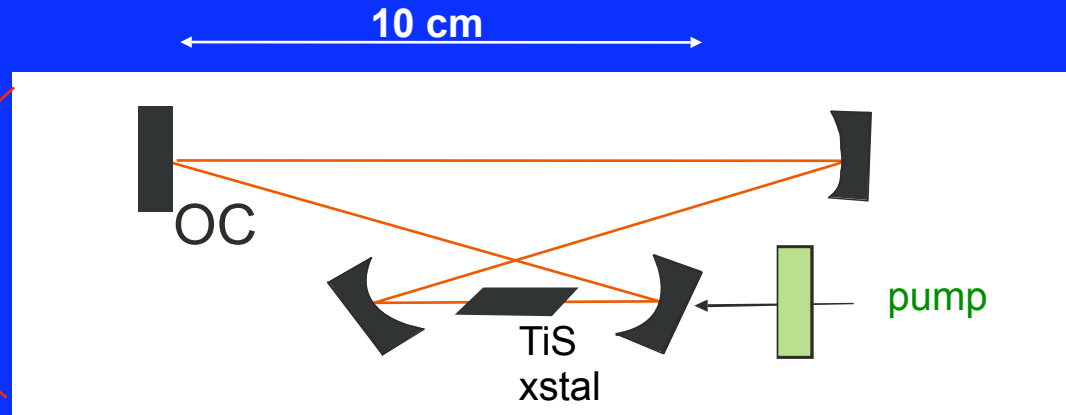
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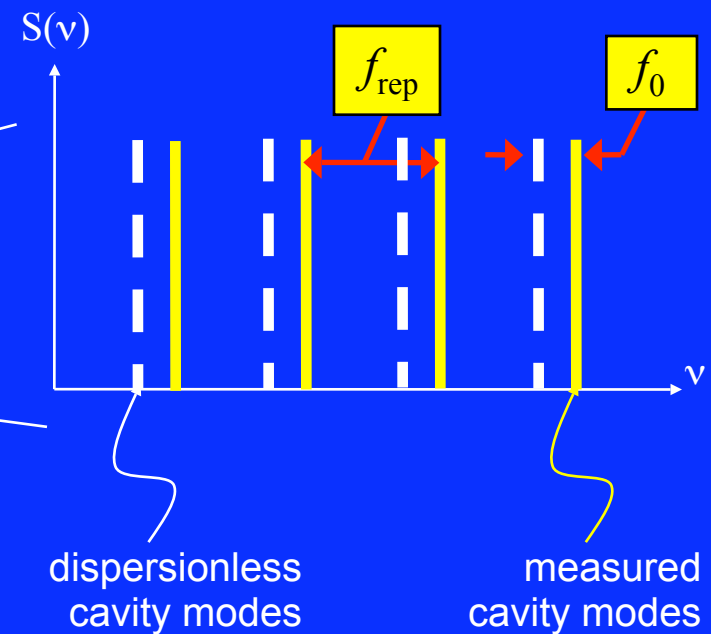
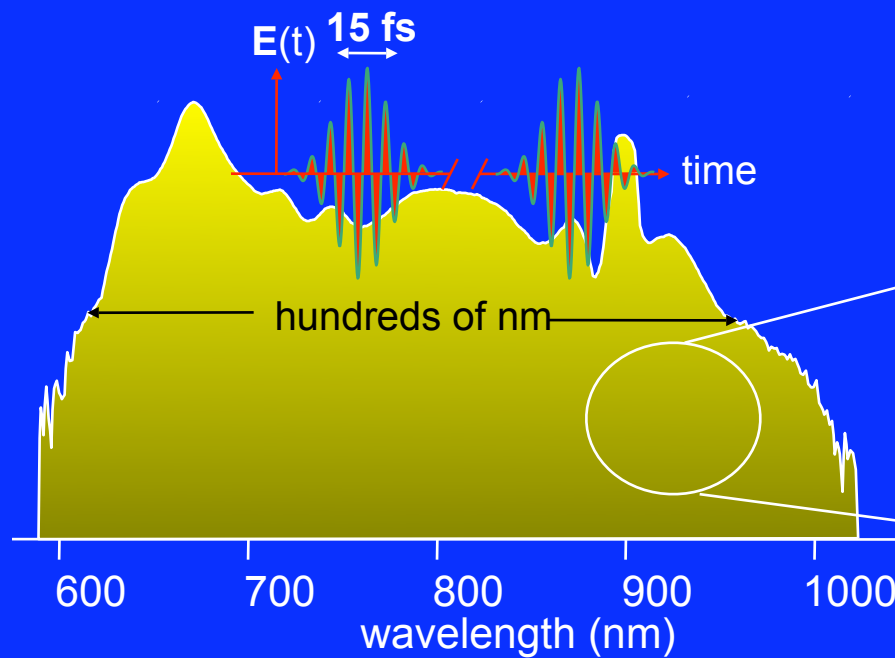
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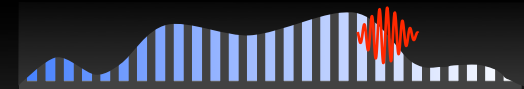
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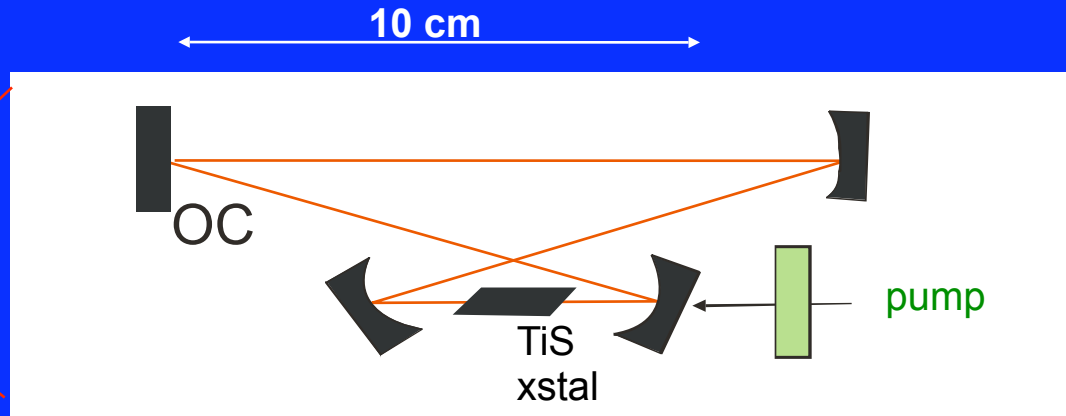
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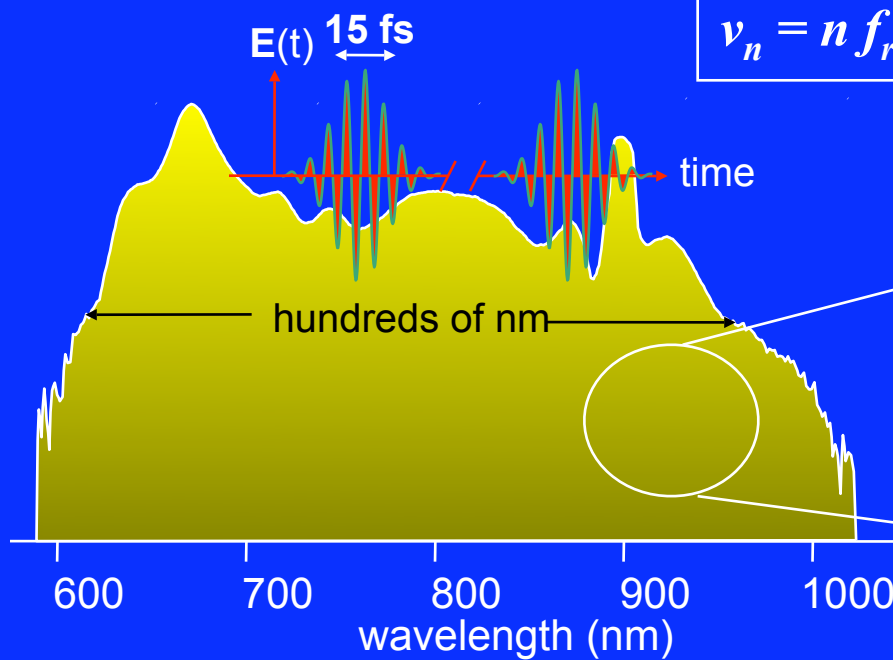
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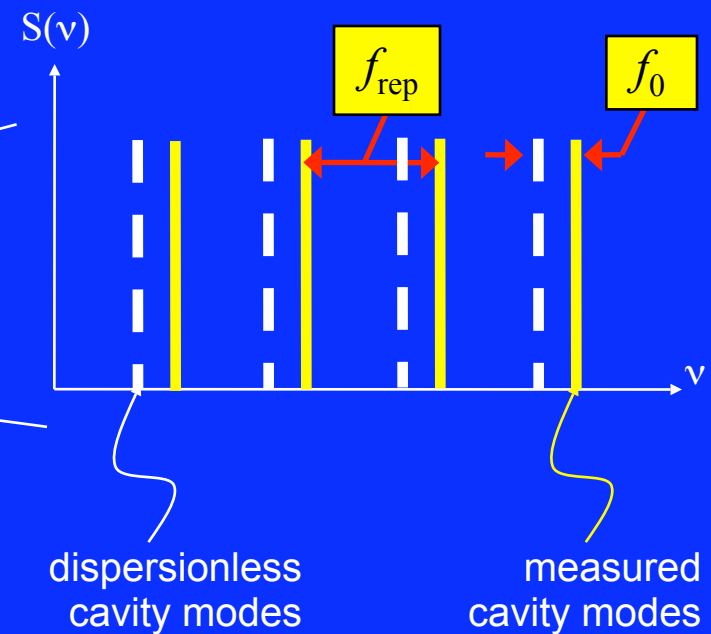
kerr lens modelocked
frequency comb



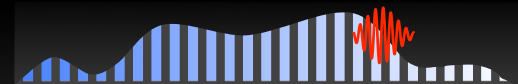
600 mW modelocked power
1 GHz repetition rate pulses
8.5 W pump beam at 532 nm



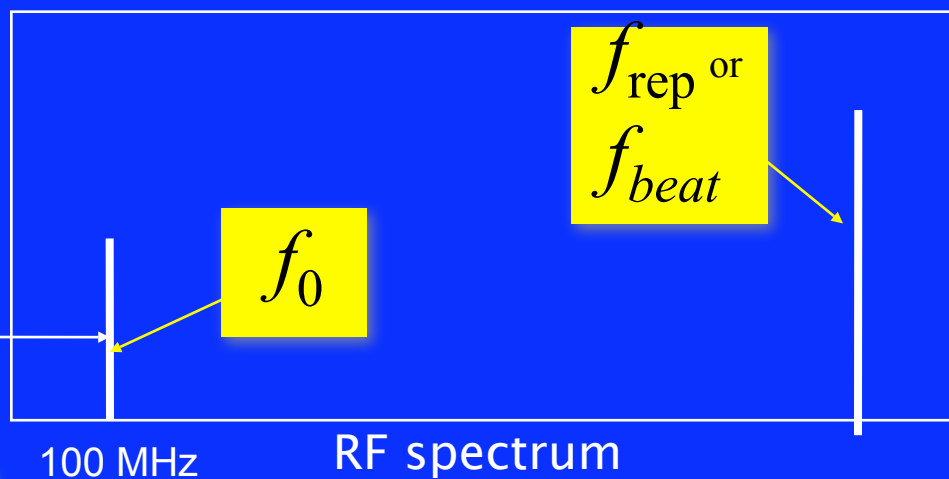
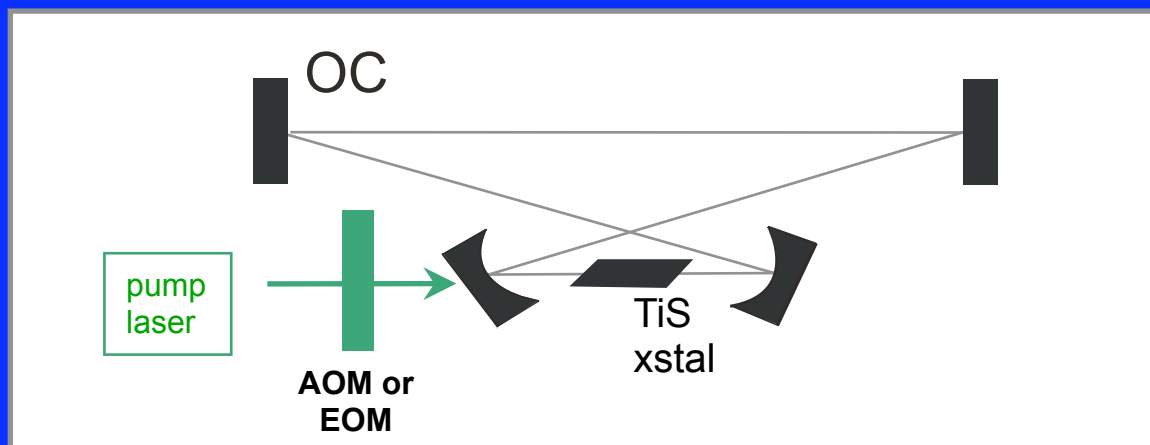
$$\nu_n = n f_{\text{rep}} + f_0$$



stabilization of optical frequency comb

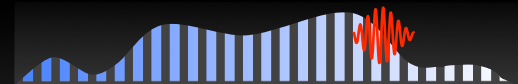


- offset controlled by modulating pump
- rep. rate or beatnote (with CW laser) controlled with cavity mirror

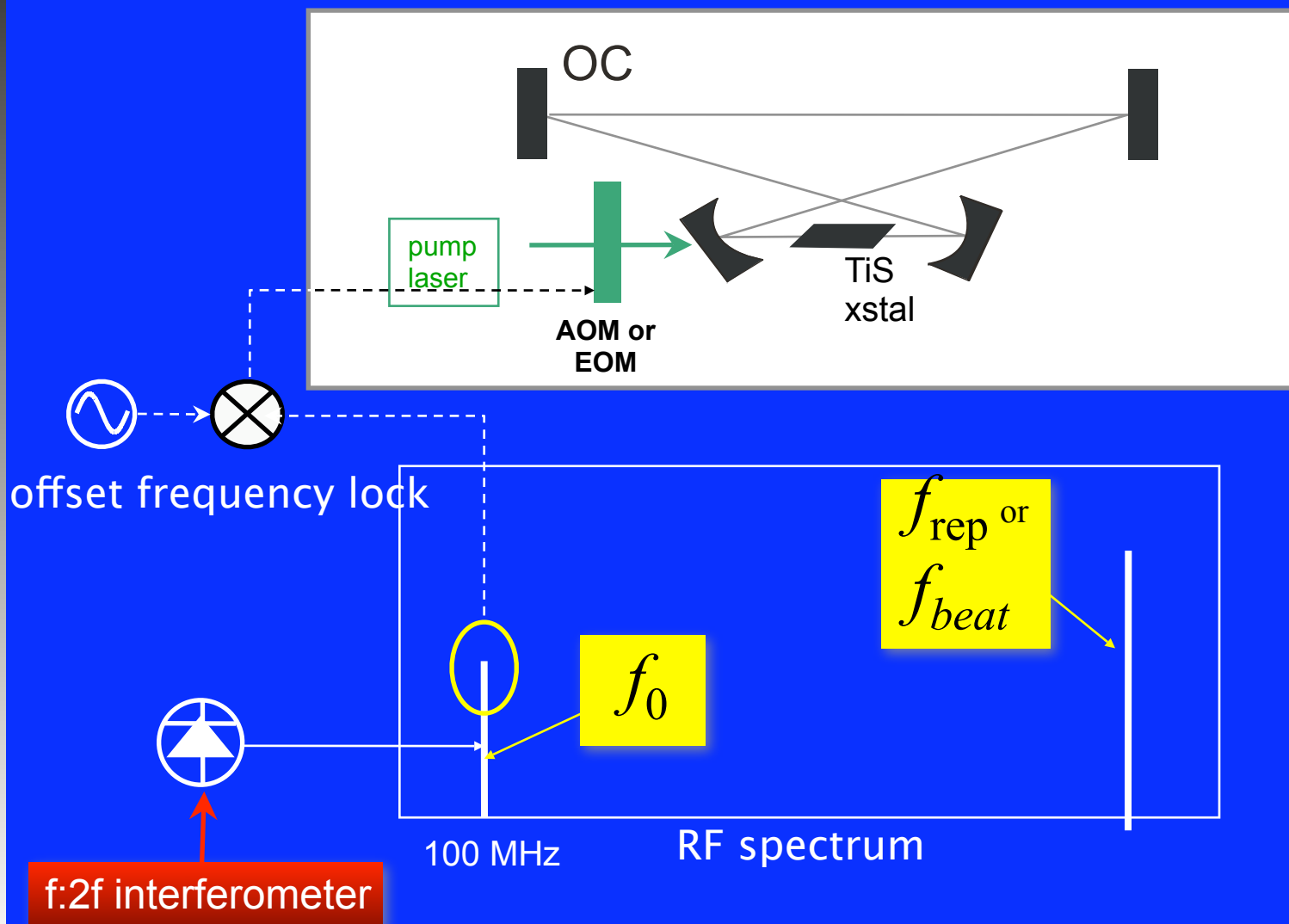


f:2f interferometer

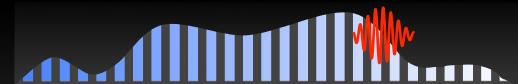
stabilization of optical frequency comb



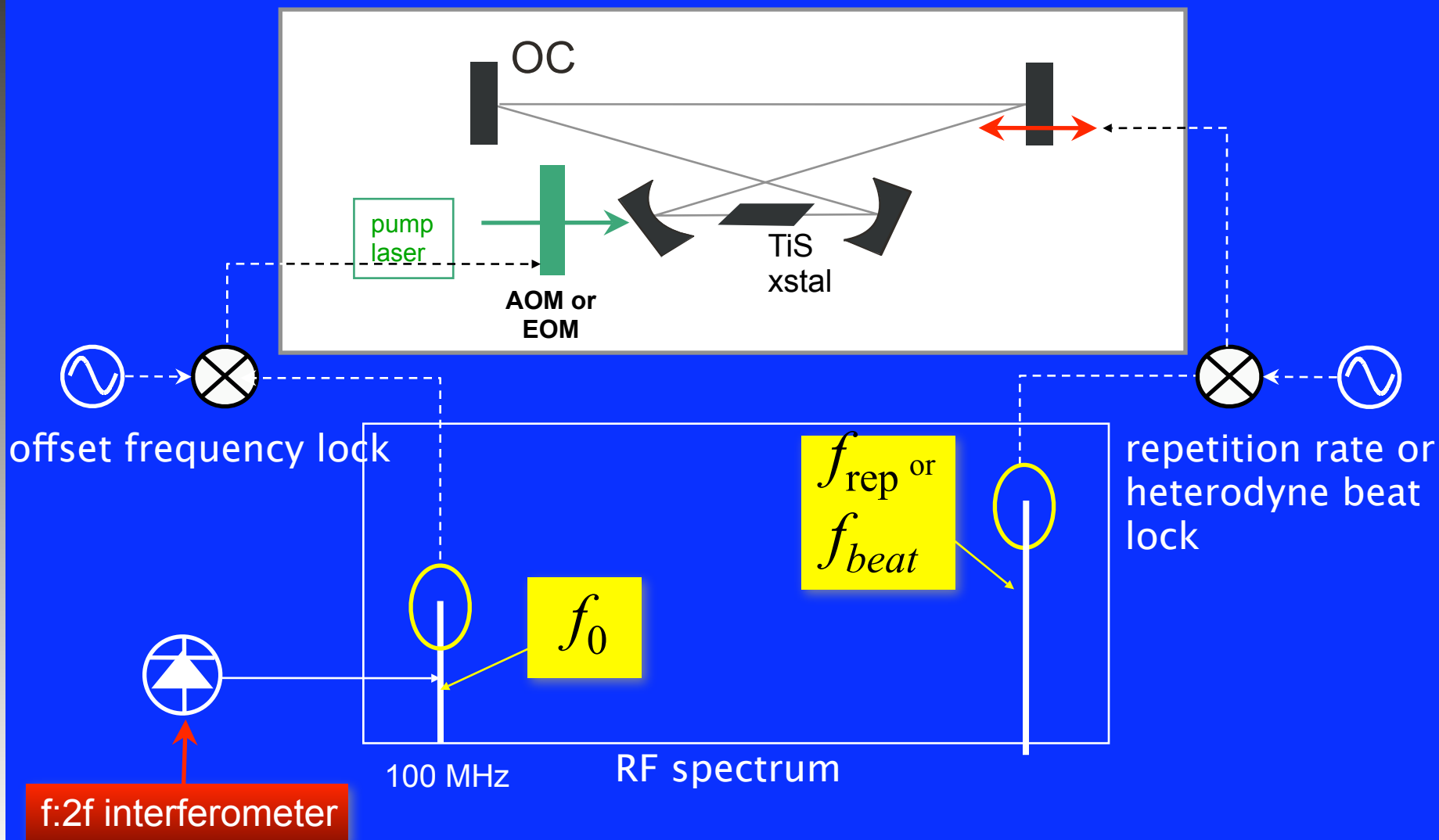
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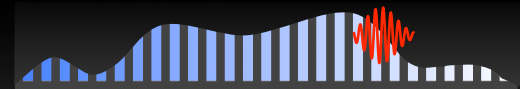


stabilization of optical frequency comb

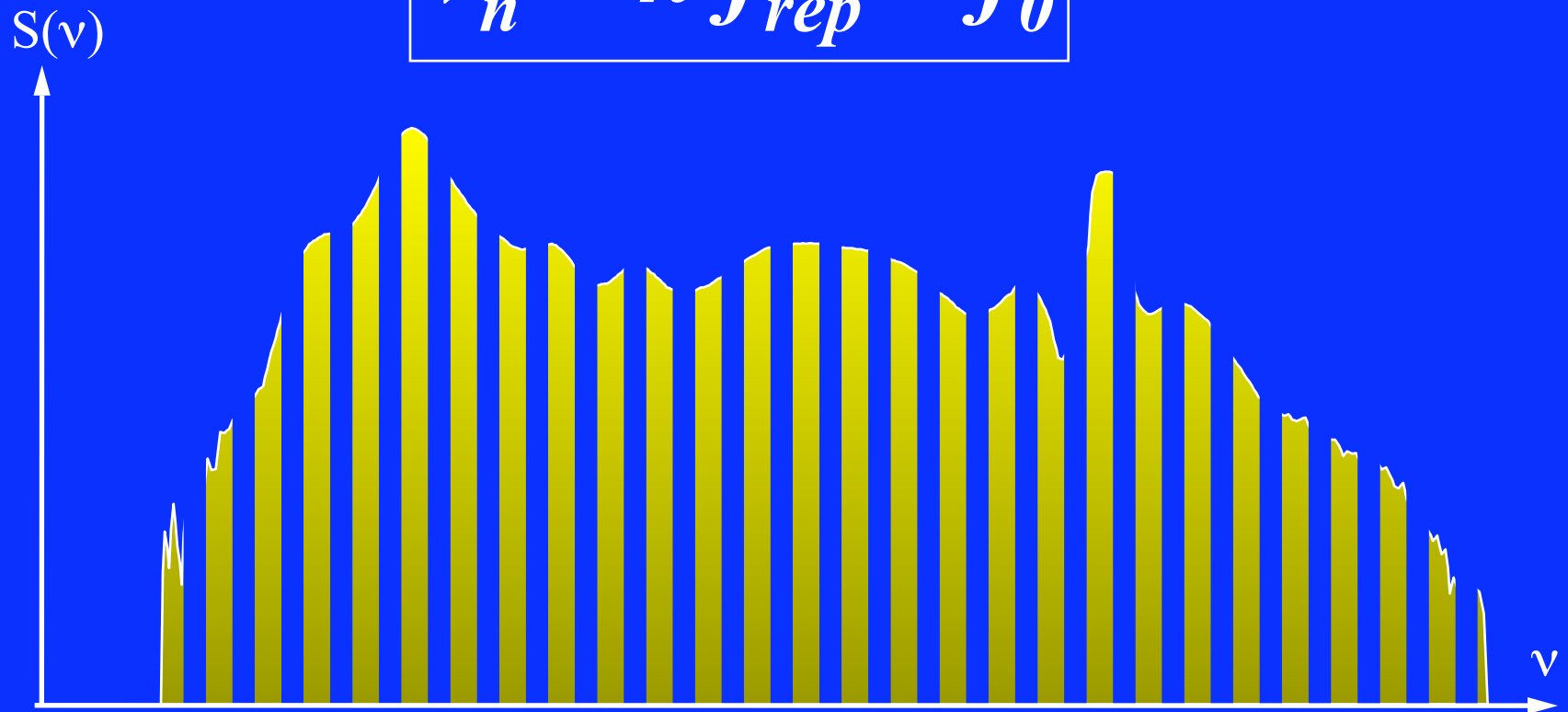


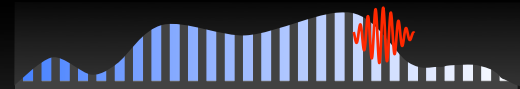
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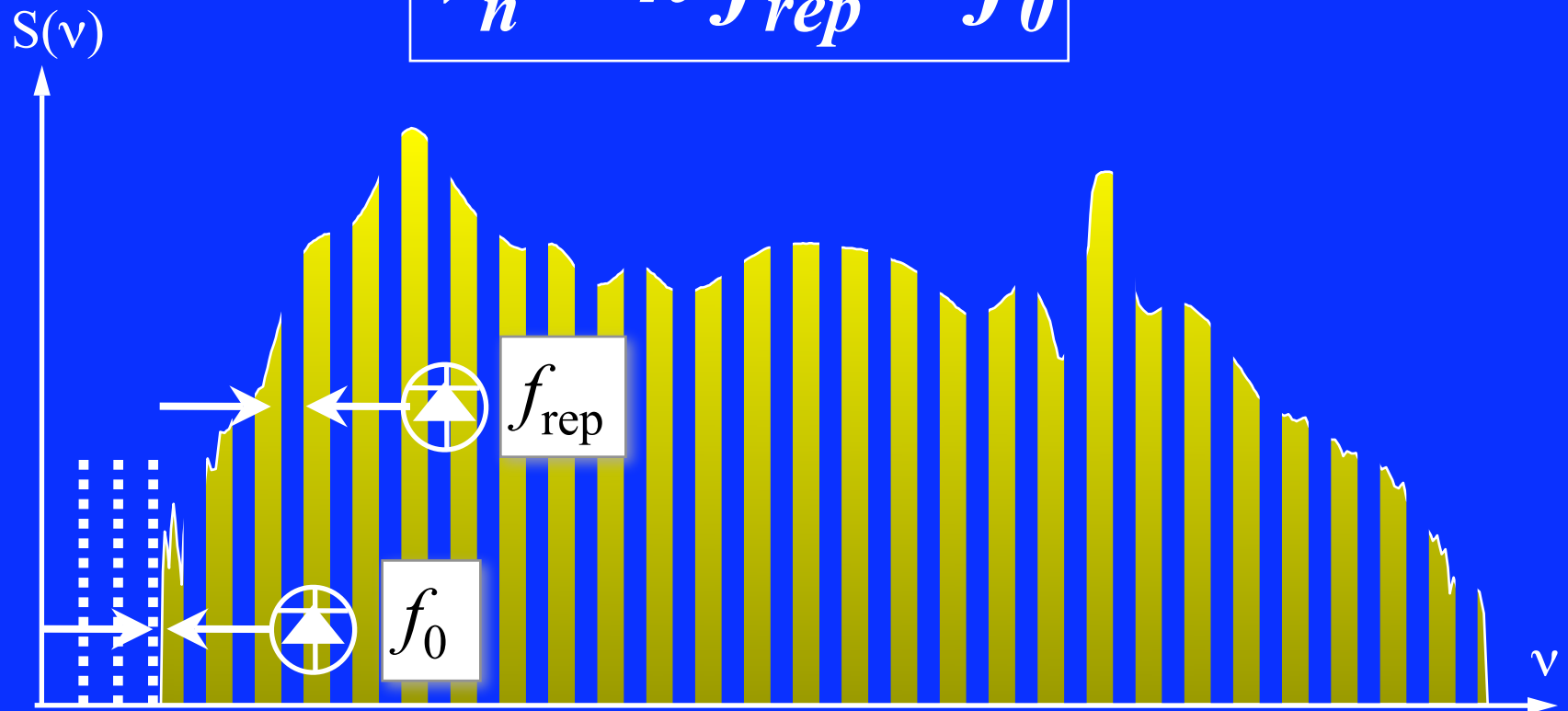


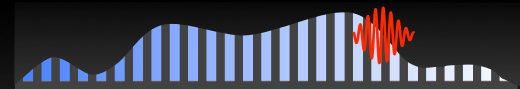
$$\nu_n = n f_{rep} + f_0$$



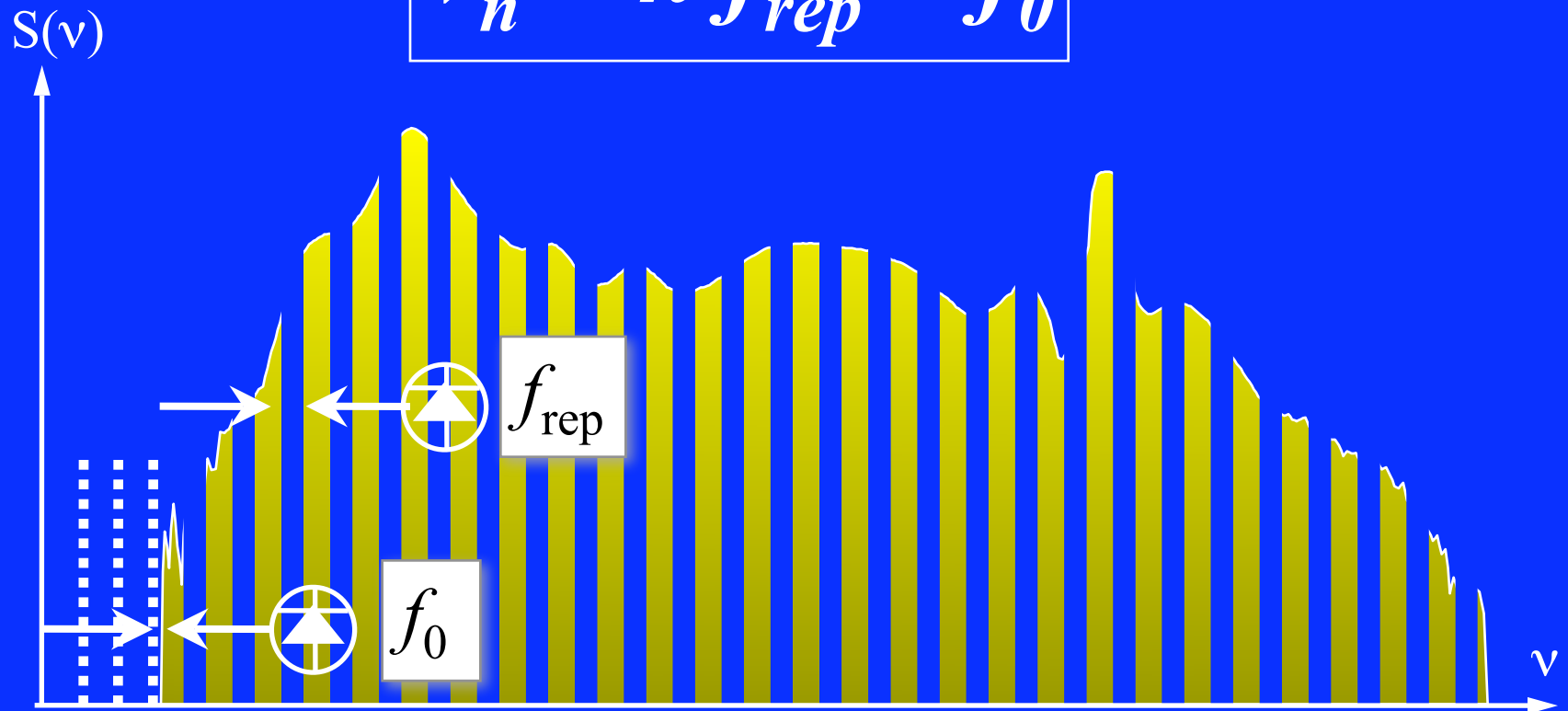


$$\nu_n = n f_{\text{rep}} + f_0$$





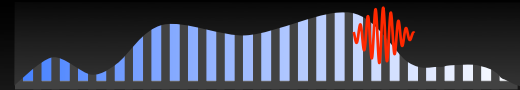
$$\nu_n = n f_{\text{rep}} + f_0$$



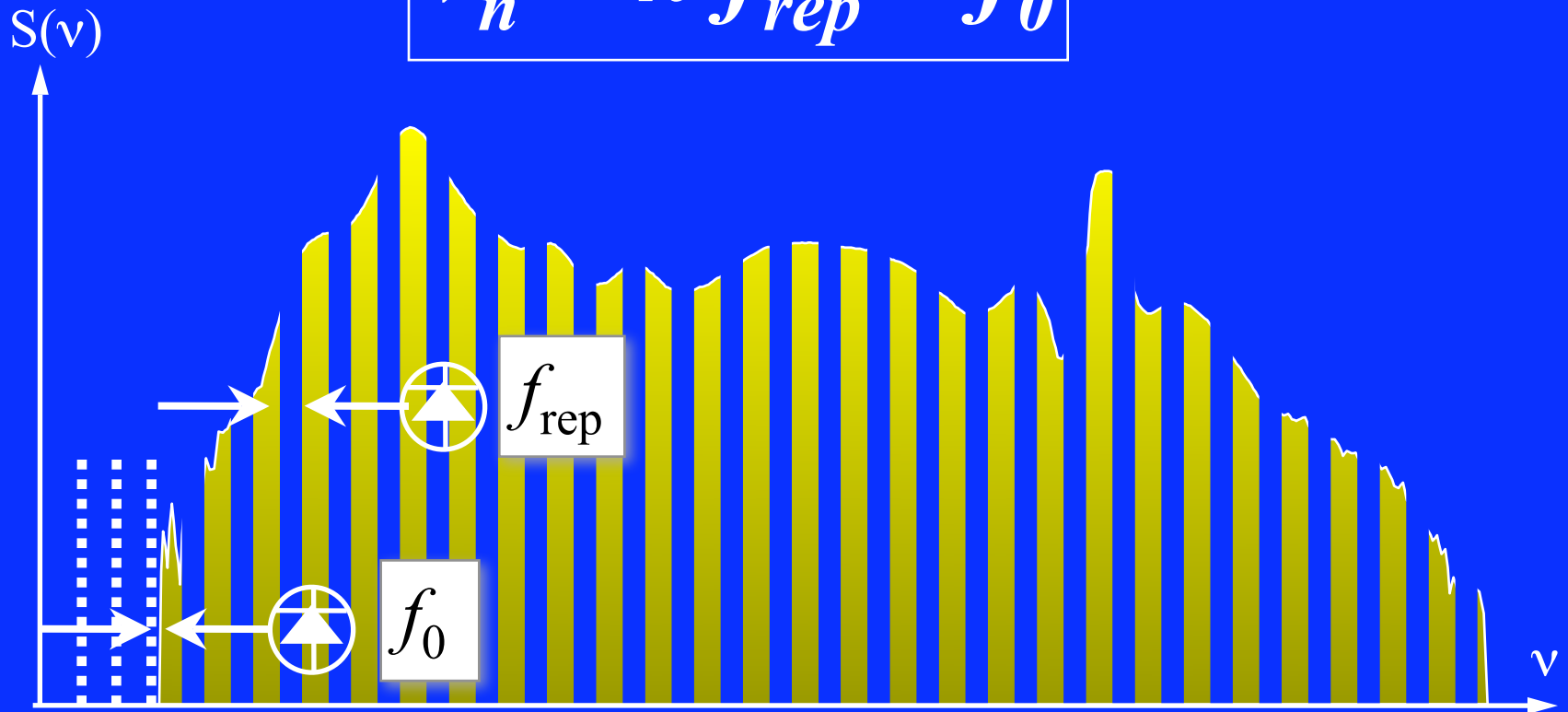
meaning that if I measure:

$$f_0 = 120 \text{ MHz}$$

$$f_{\text{rep}} = 1000 \text{ MHz}$$



$$\nu_n = n f_{rep} + f_0$$



meaning that if I measure:

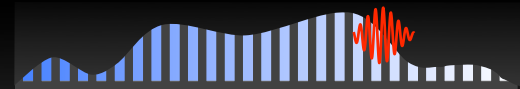
$$f_0 = 120 \text{ MHz}$$

$$f_{rep} = 1000 \text{ MHz}$$

then I know *all* the optical frequencies:

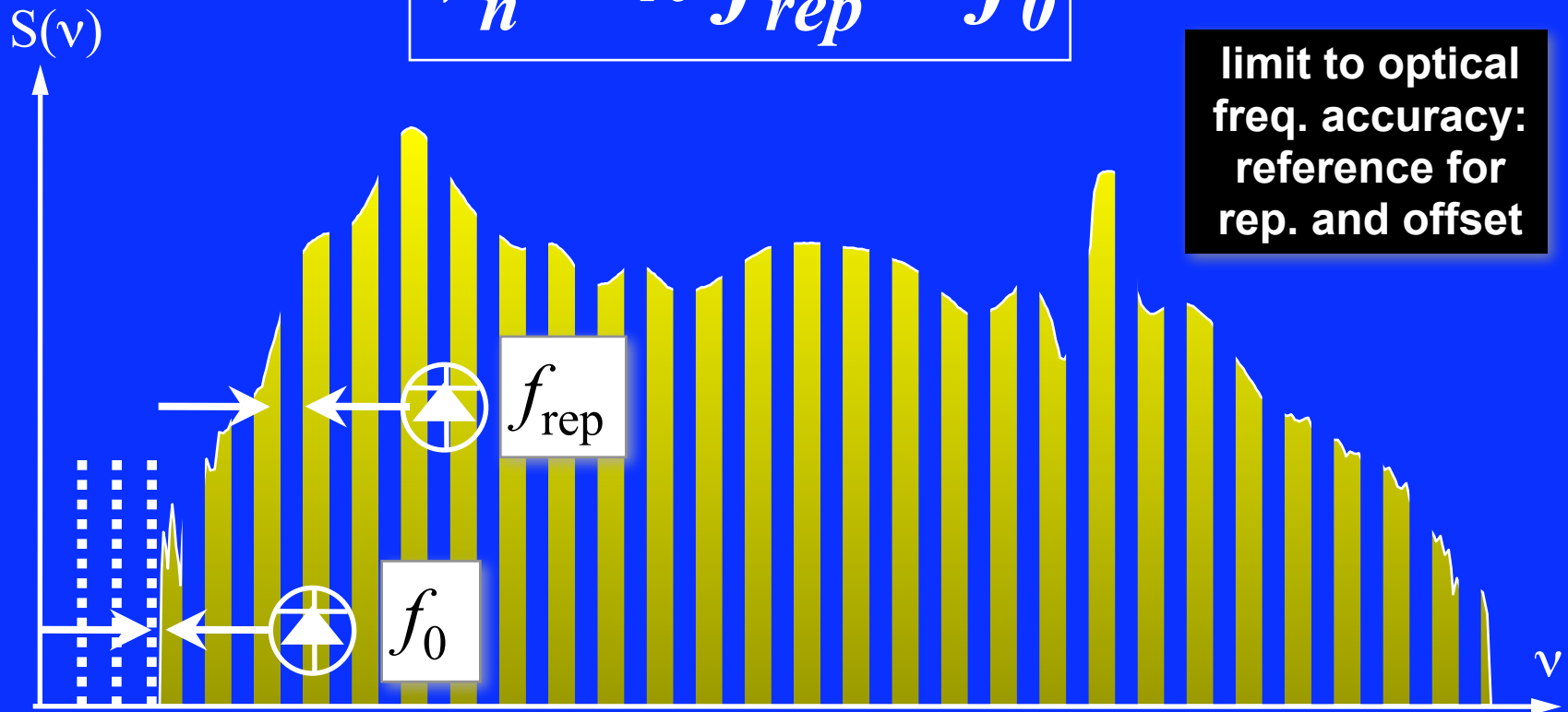
the $n=500,000$ mode has a freq. of:

$$\begin{aligned} \nu_n &= n f_{rep} + f_0 = 5e5(1\text{GHz}) + 120 \text{ MHz} \\ &= 500,000,120,000,000 \text{ Hz} \end{aligned}$$



$$\nu_n = n f_{rep} + f_0$$

limit to optical
freq. accuracy:
reference for
rep. and offset



meaning that if I measure:

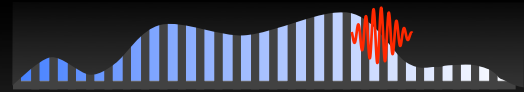
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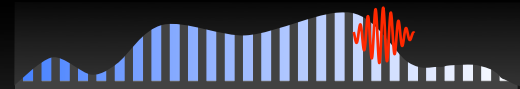
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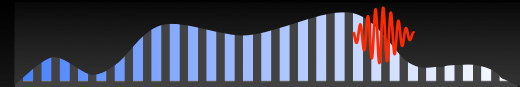
...on the other hand...

...we can extract microwave signals from stabilized combs.

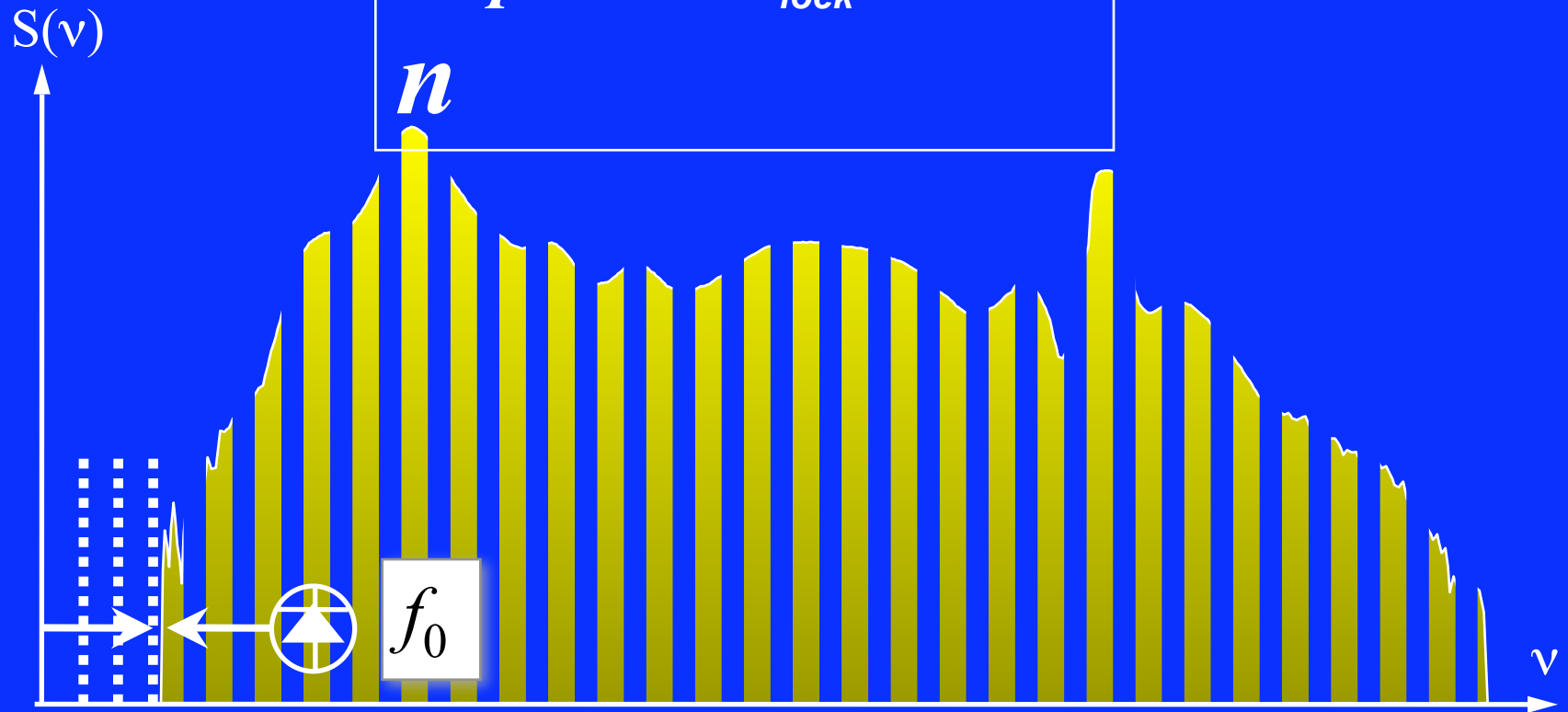


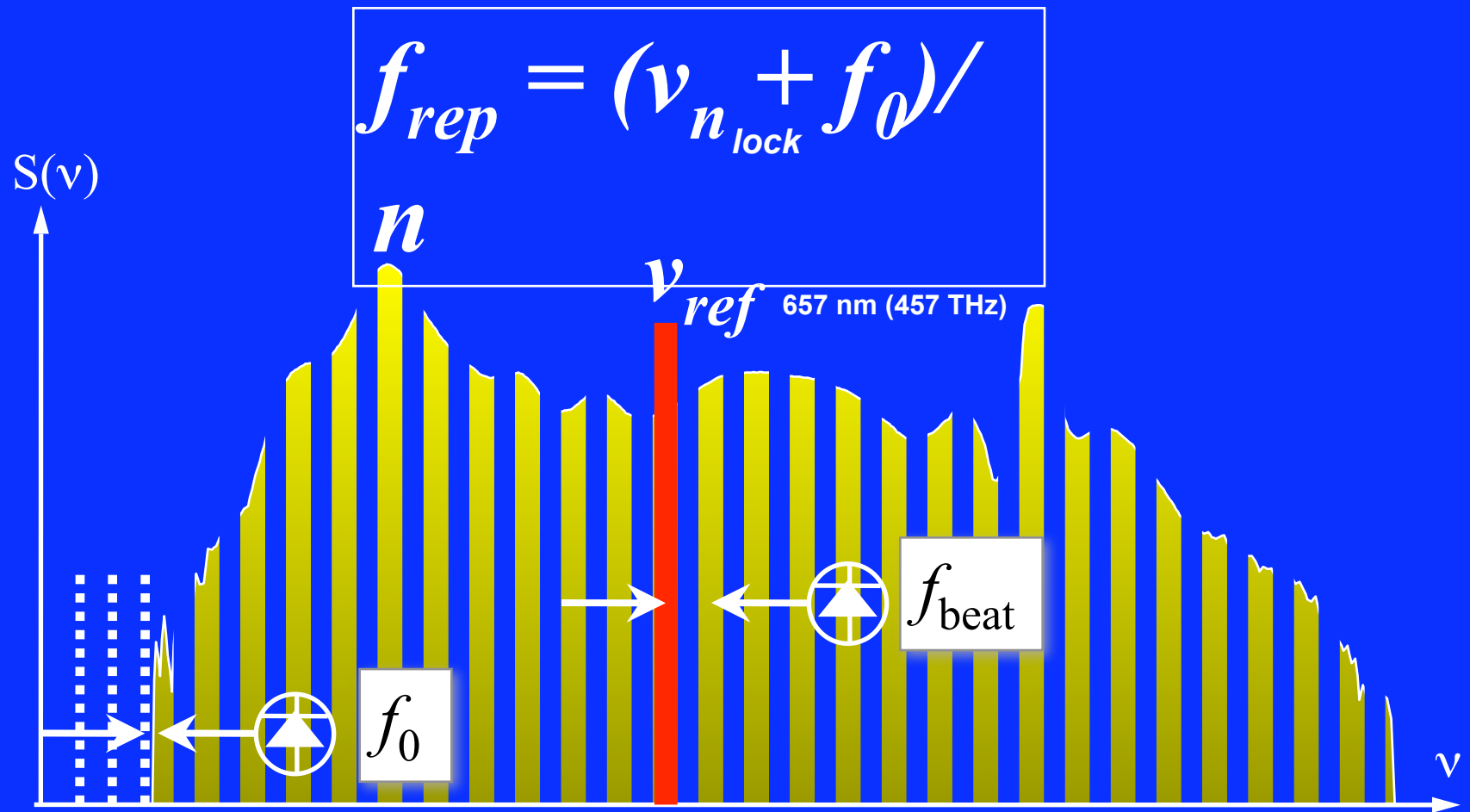
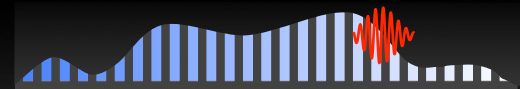
$$f_{rep} = (v_{n_{lock}} + f_0) / n$$

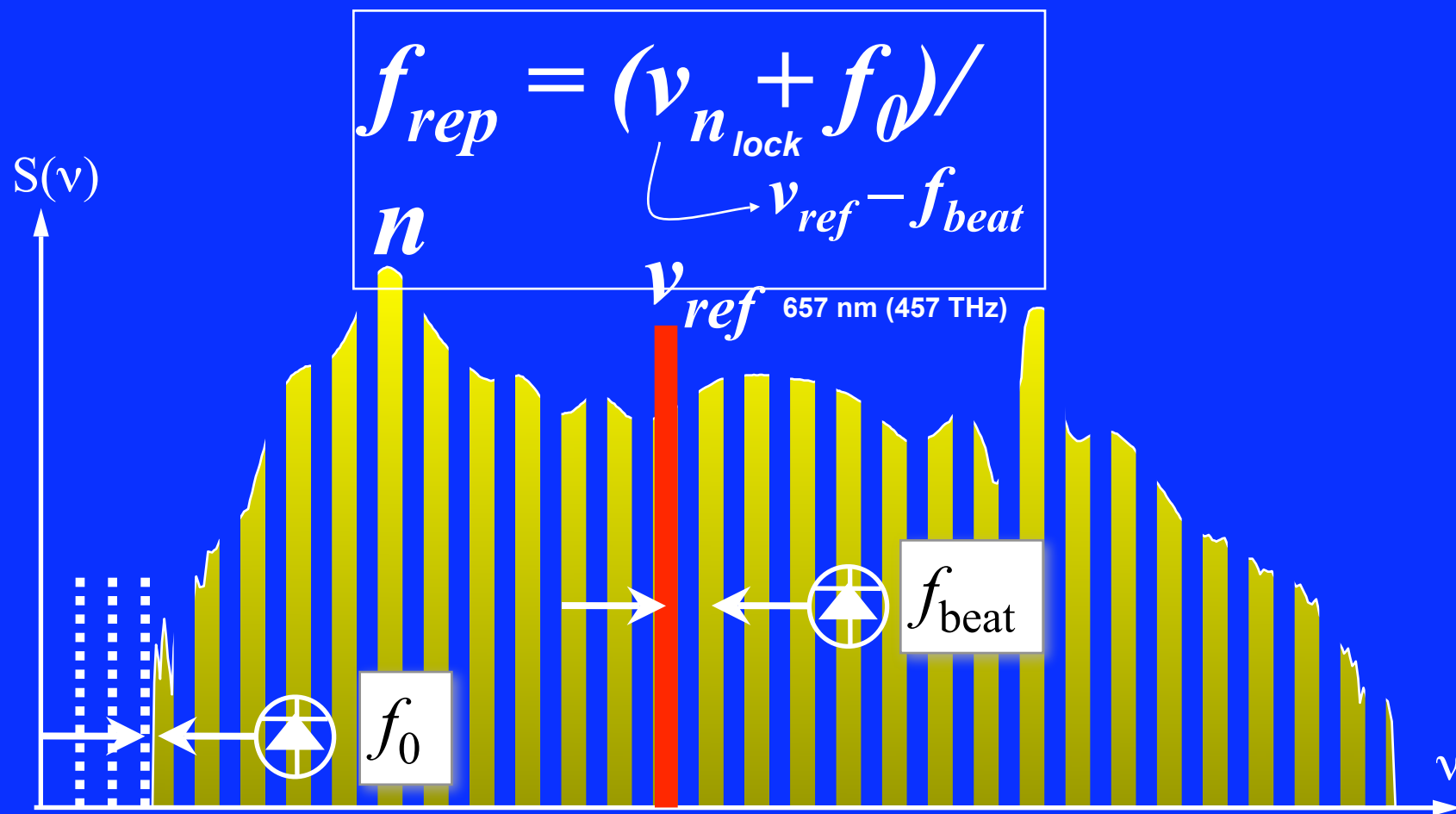
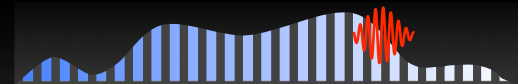


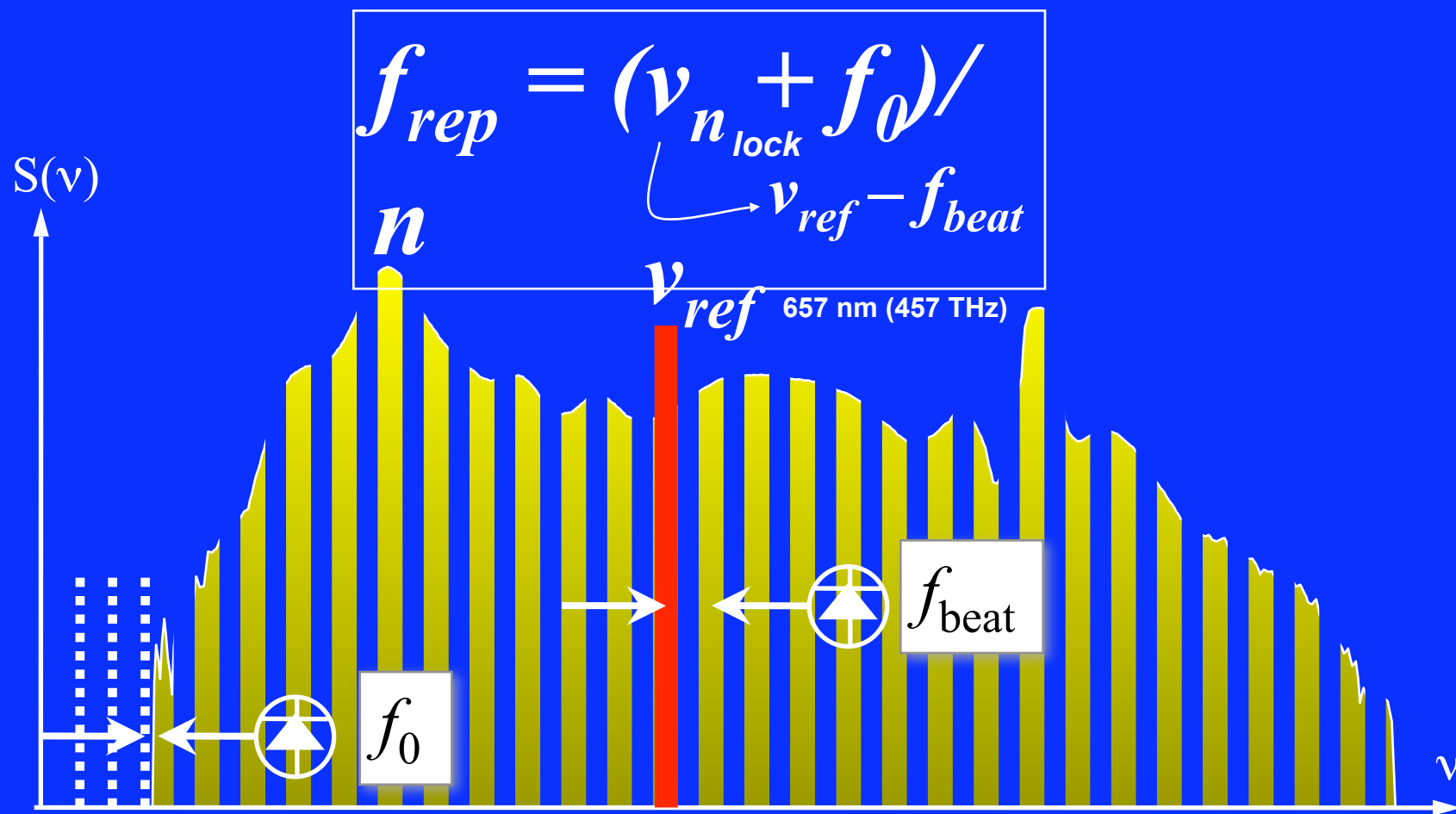
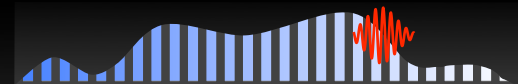


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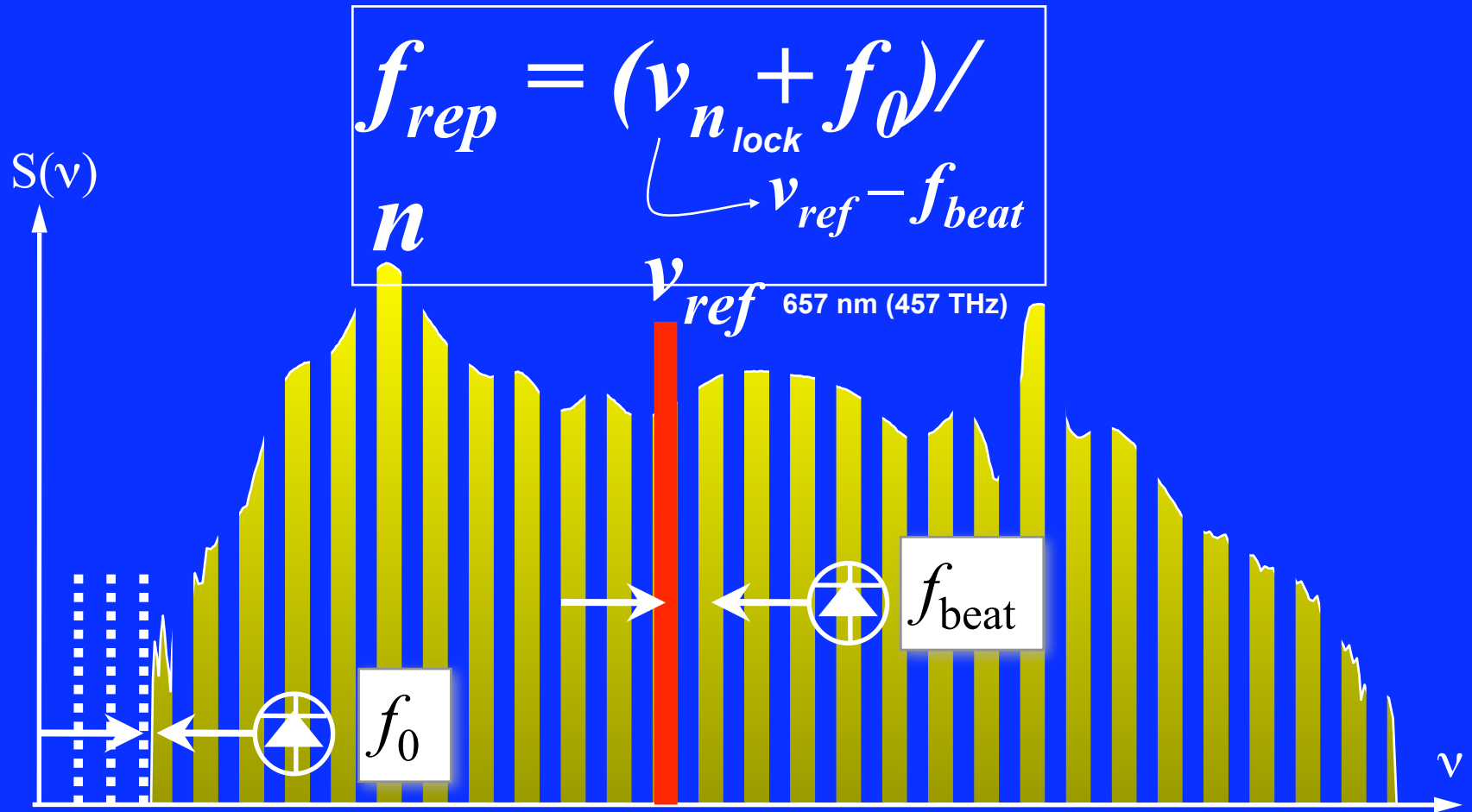
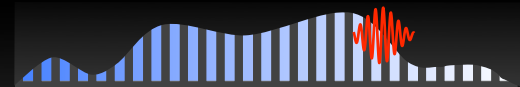




meaning that if I measure:

$$f_0 = 120 \text{ MHz}$$

$$f_{beat} = 300 \text{ MHz}$$



meaning that if I measure:

$$f_0 = 120 \text{ MHz}$$

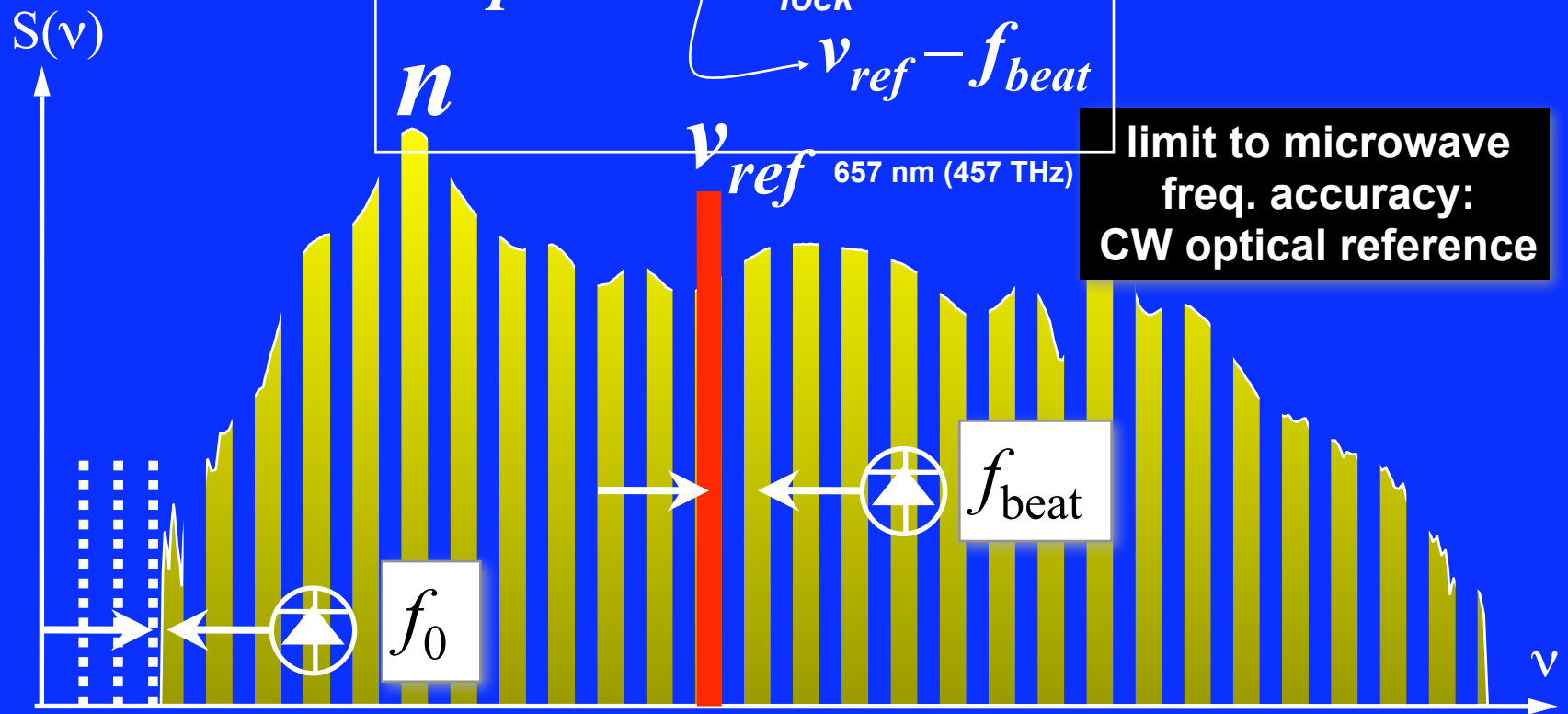
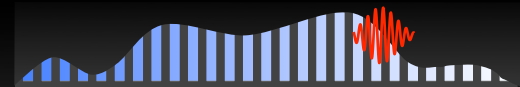
$$f_{beat} = 300 \text{ MHz}$$

then I know *all* the microwave frequencies:

the $n=500,000$ divided mode is:

$$f_{rep} = (457 \text{e}12 - 300 \text{ MHz} - 120 \text{ MHz}) / n$$

$$= 914 \text{ MHz} \quad (\text{this moves with CW reference say, 1 Hz per second})$$



meaning that if I measure:

$$f_0 = 120 \text{ MHz}$$

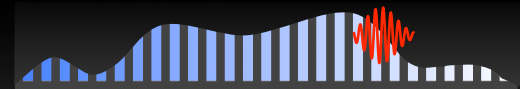
$$f_{\text{beat}} = 300 \text{ MHz}$$

then I know *all* the microwave frequencies:

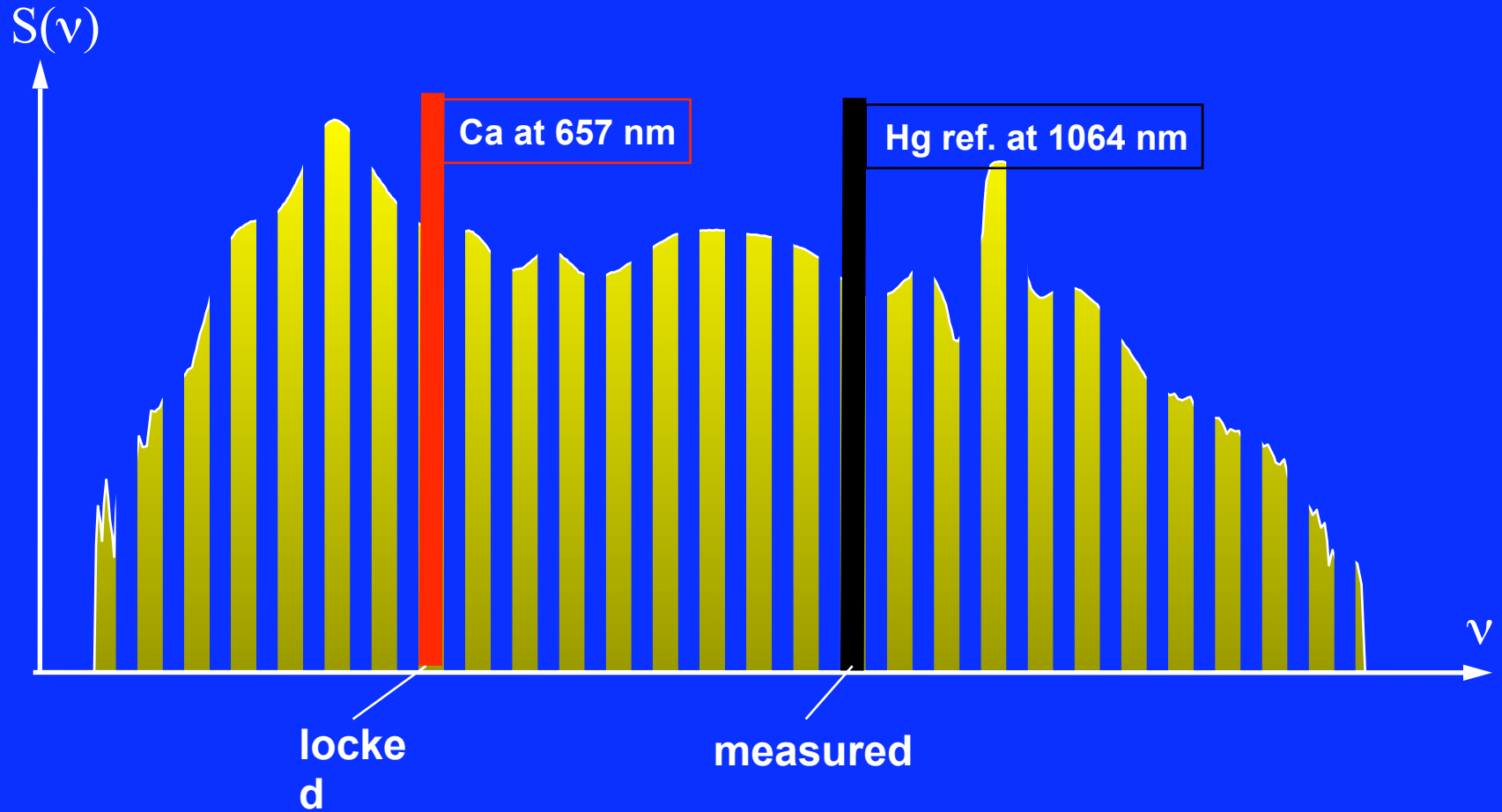
the $n=500,000$ divided mode is:

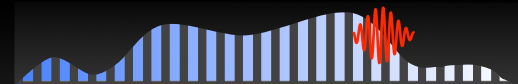
$$f_{\text{rep}} = (457\text{e}12 - 300 \text{ MHz} - 120 \text{ MHz})/n$$

$$= 914 \text{ MHz} \quad (\text{this moves with CW reference say, 1 Hz per second})$$

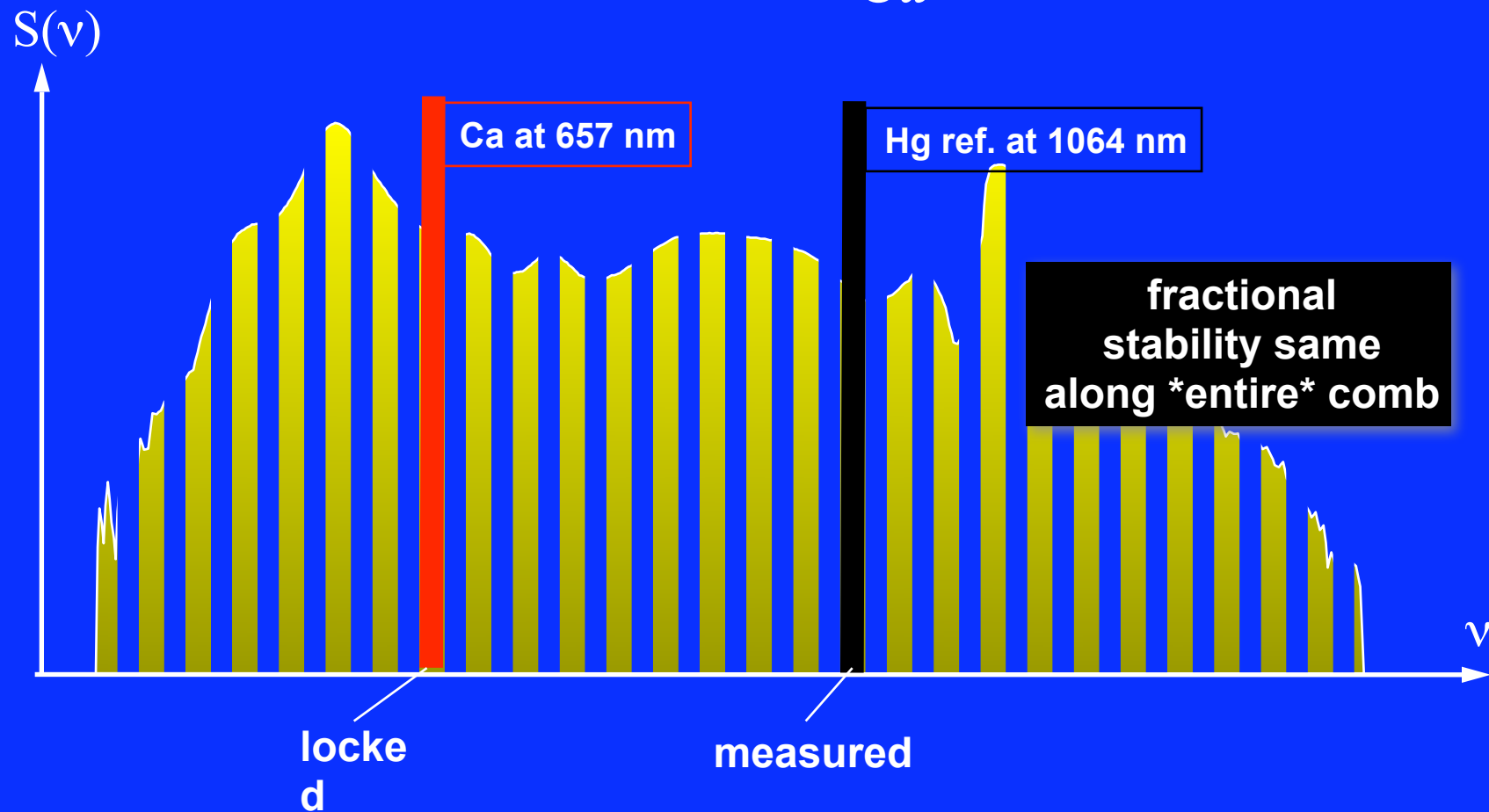


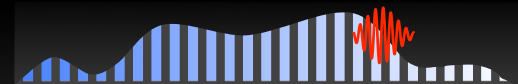
combs stability $\frac{\delta \nu_0}{\nu_0}$



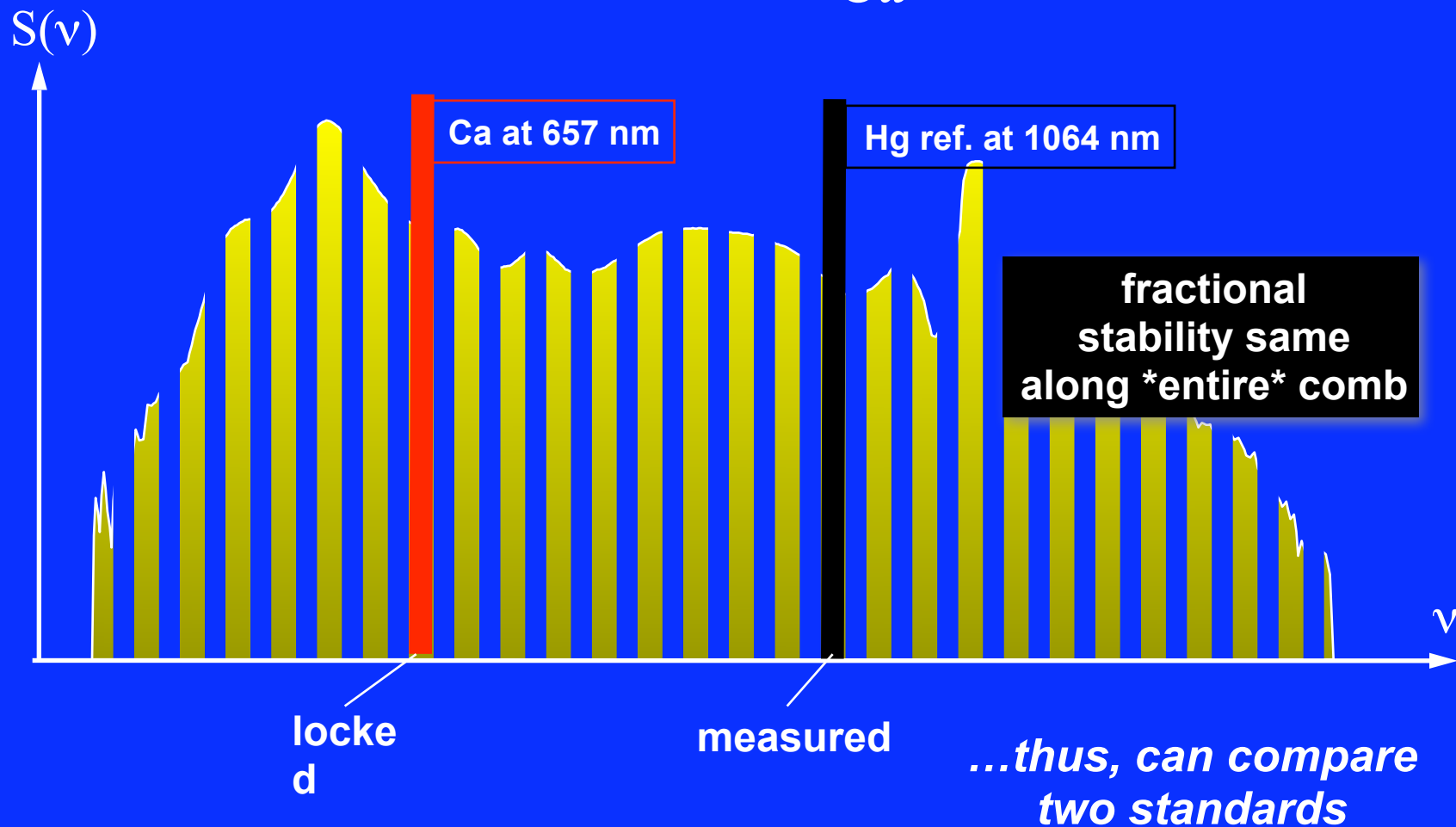


combs stability $\frac{\delta \nu_0}{\nu_0} \approx \frac{\delta \nu_{Ca}}{\nu_{Ca}}$ optical reference stability

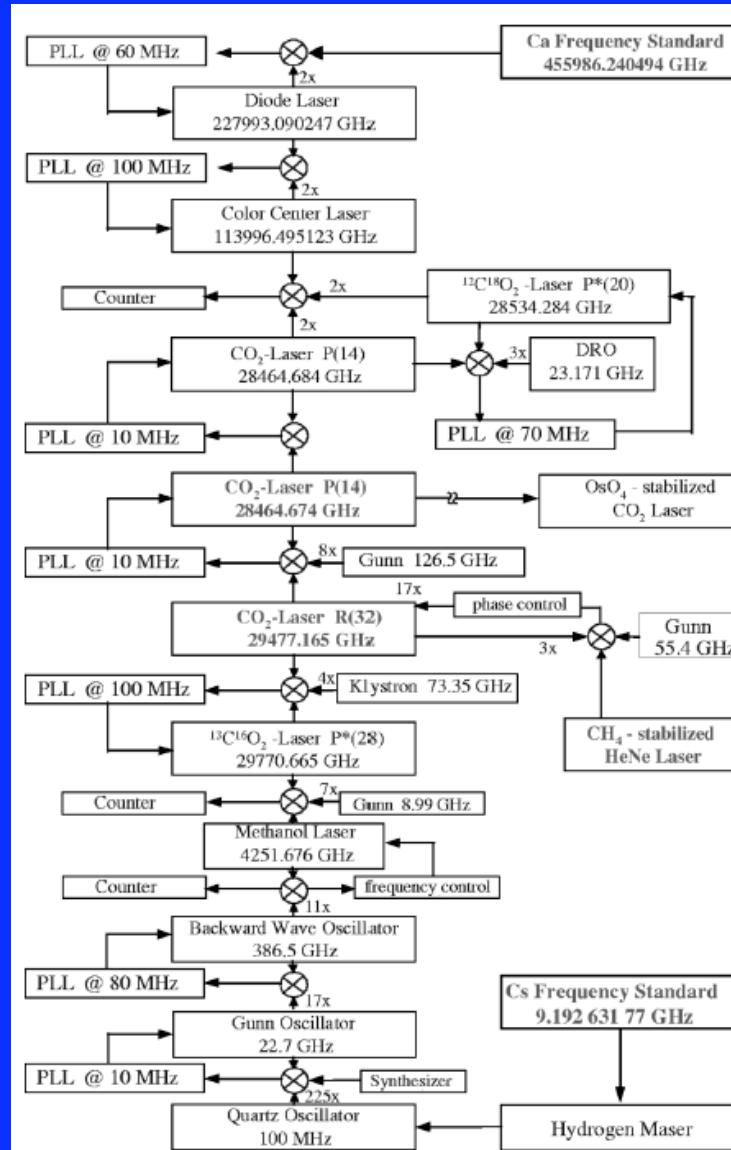
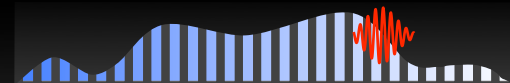


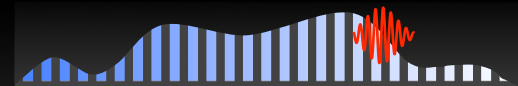


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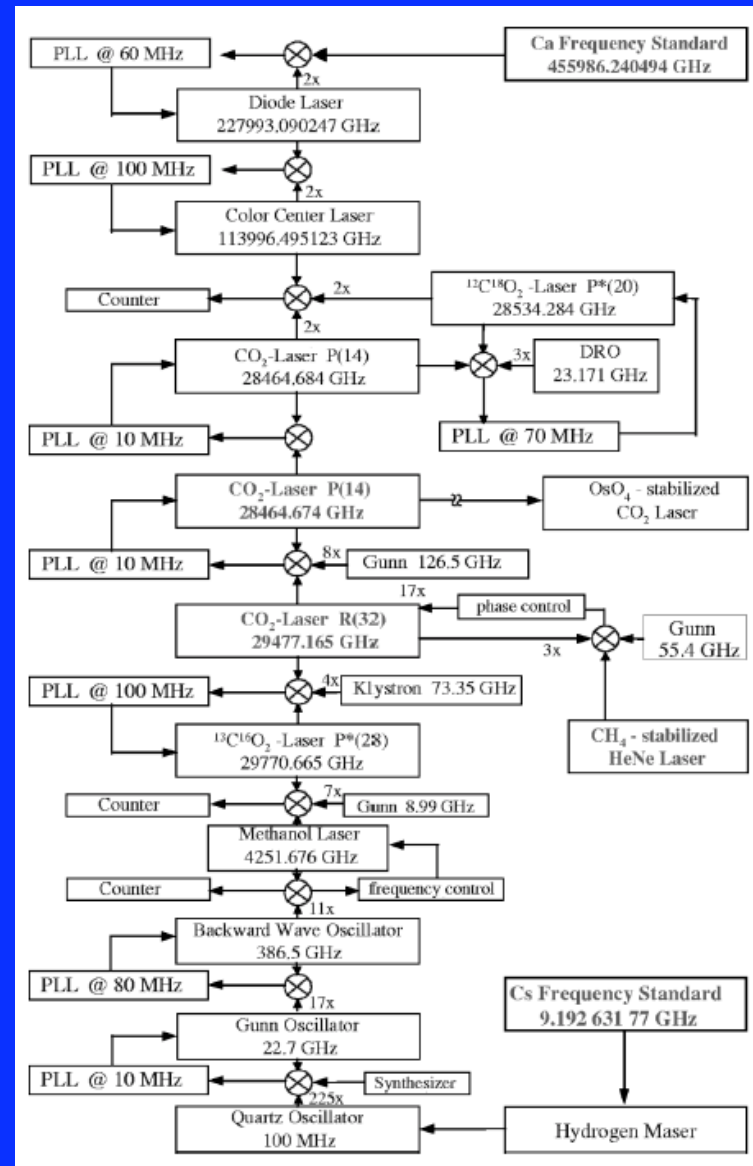
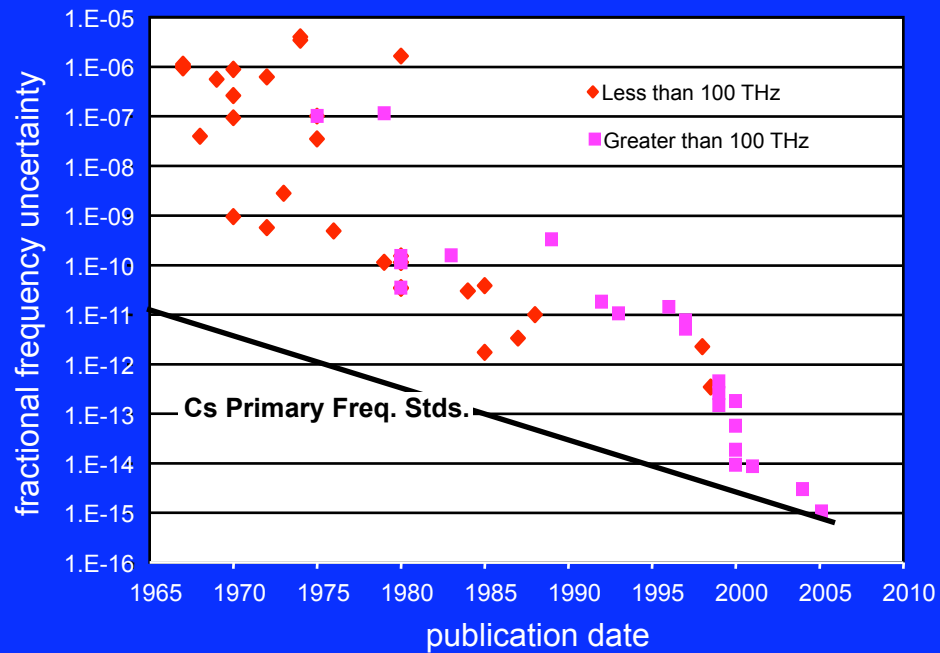
frequency measurements: simplified with combs

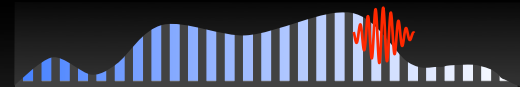




stabilized
frequency comb

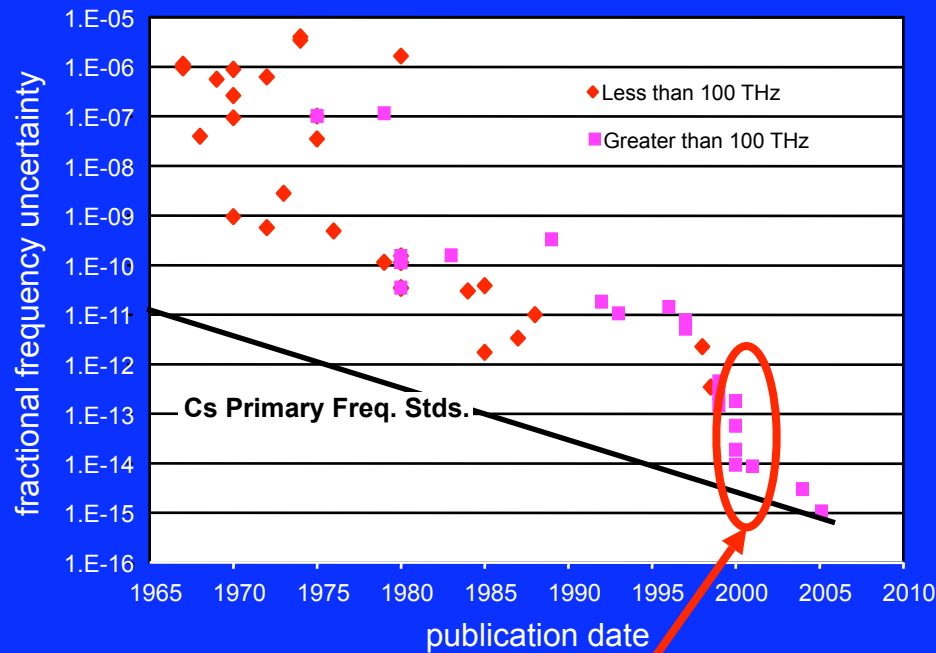
frequency measurements of laser-based frequency standards



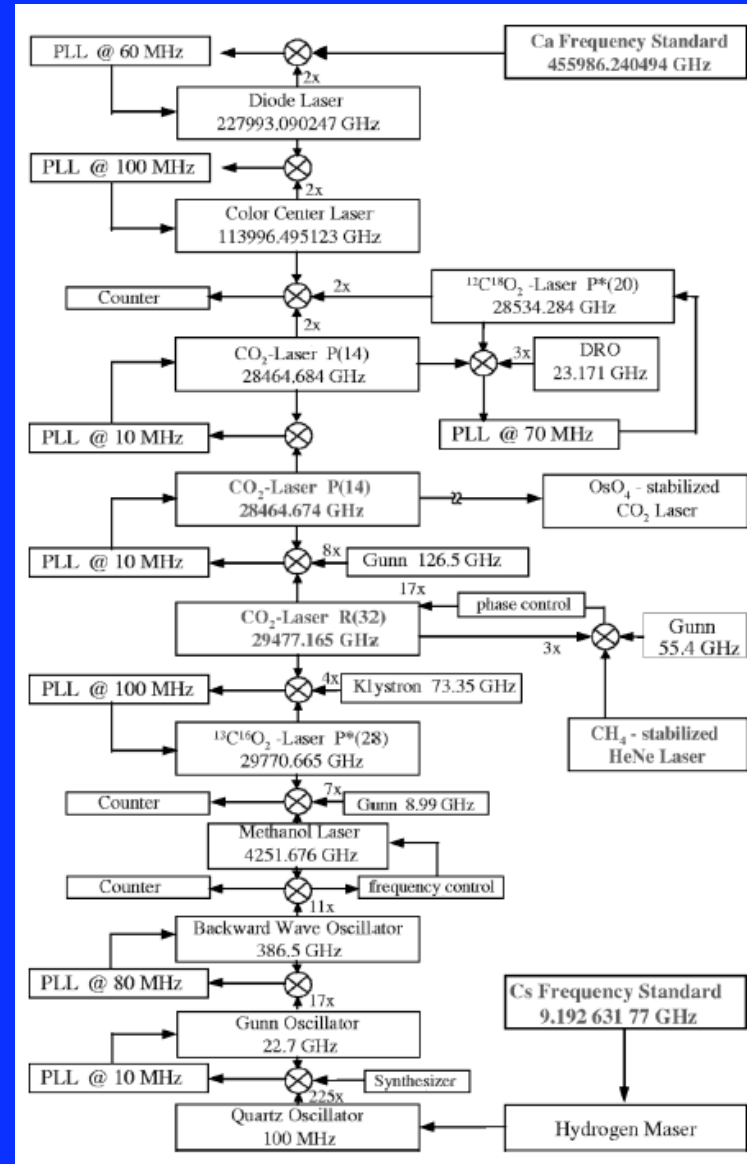


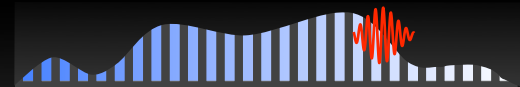
stabilized
frequency comb

frequency measurements of laser-based frequency standards



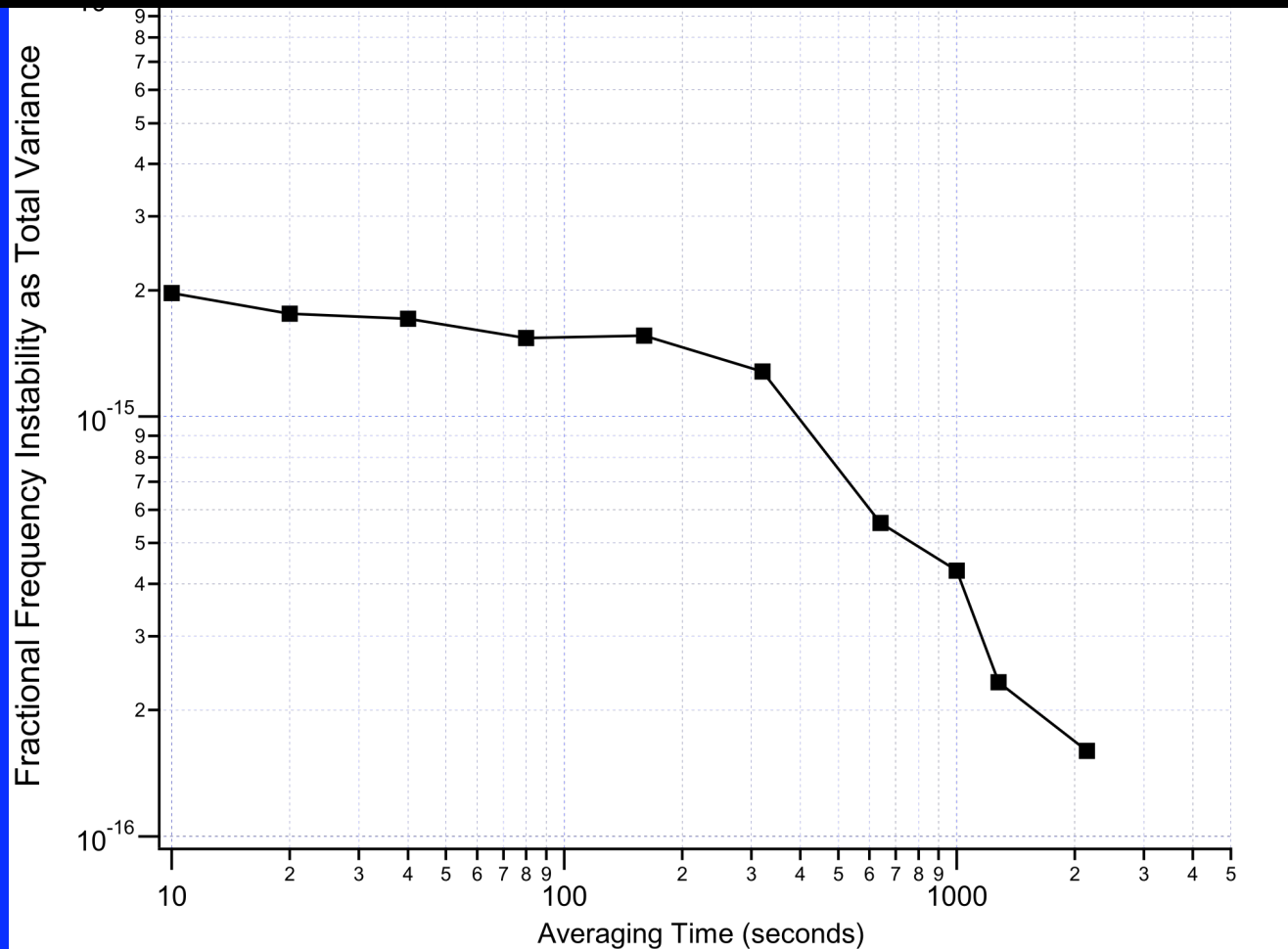
optical frequency metrology now routinely
(as of year 2000) involves
frequency combs for measurements

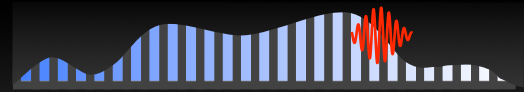




neutral Ca atoms: 457 THz (657 nm)
Hg+: 563 THz (532 nm)

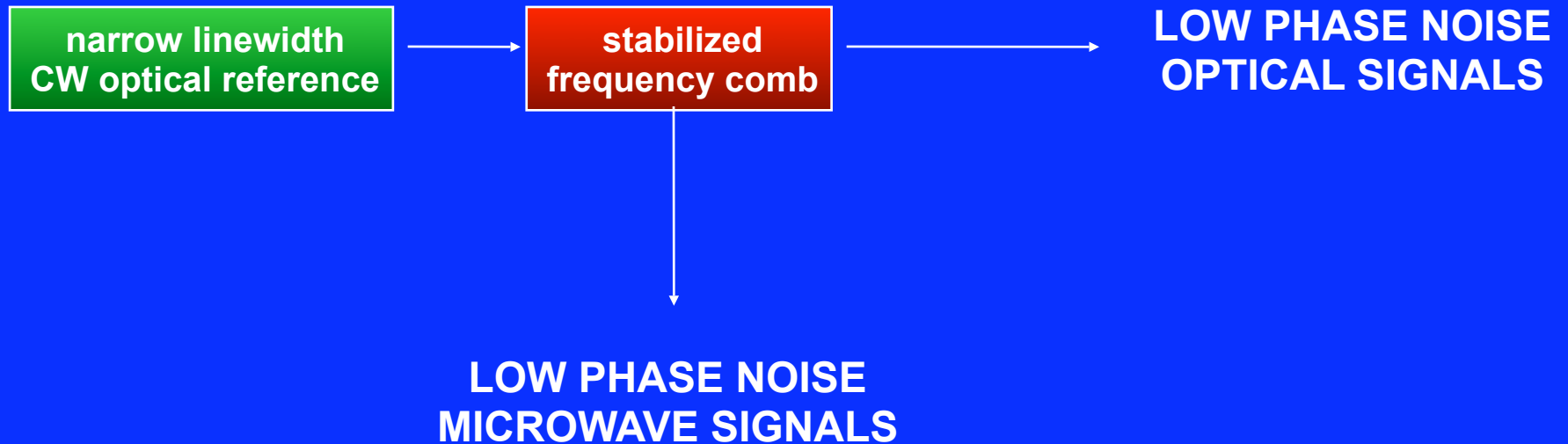
frequency comb as gearwork for optical-atomic clocks



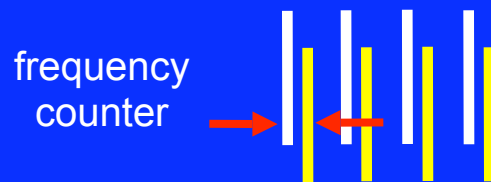
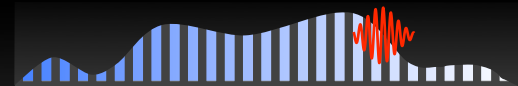


much of the work with combs relies on low phase noise

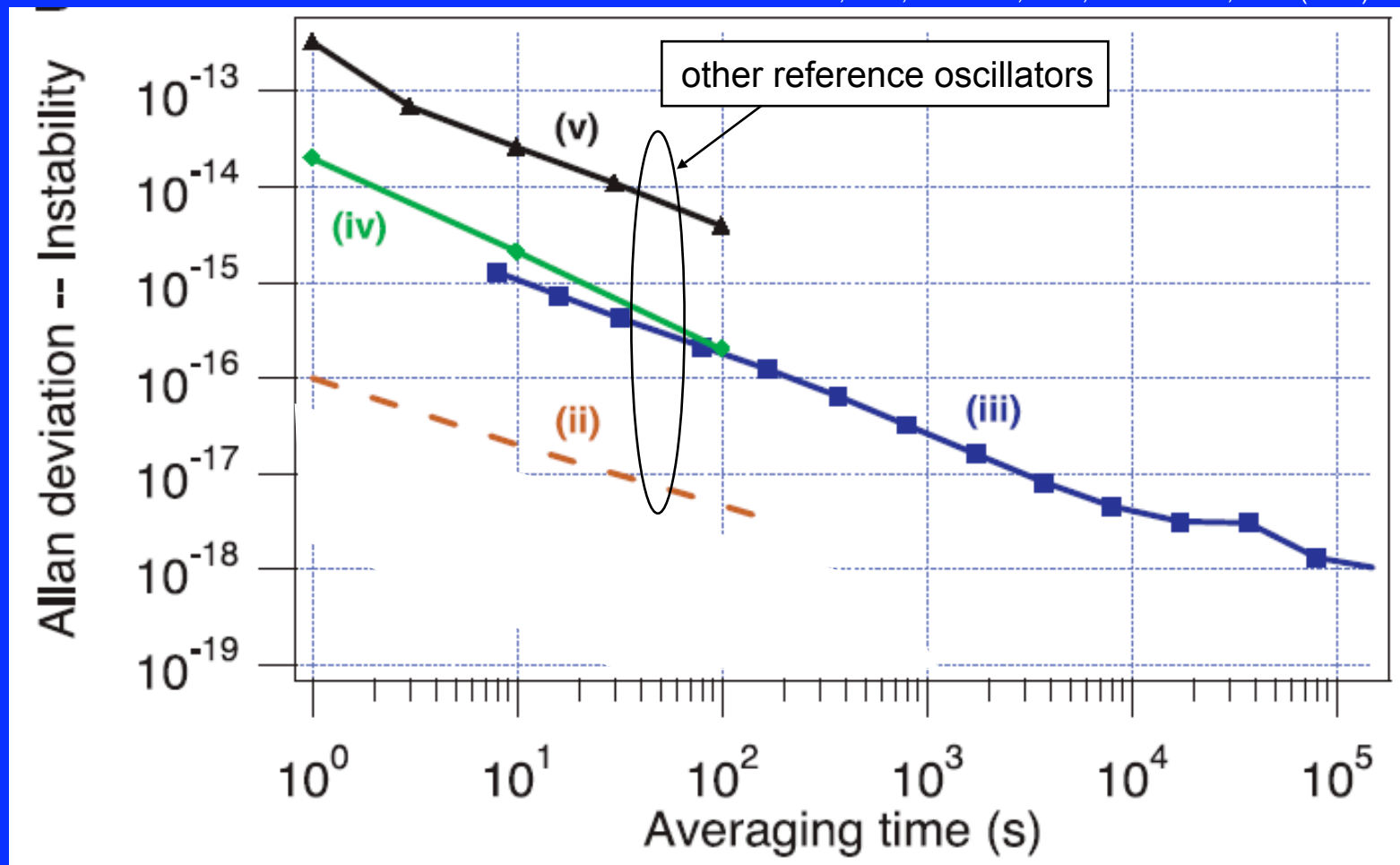
at NIST, we are interested in performance in both regimes



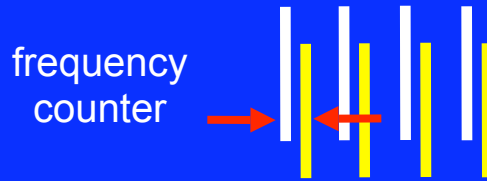
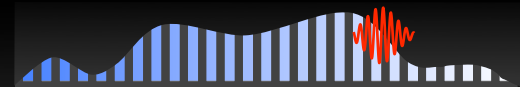
first step: establish frequency stability of comb



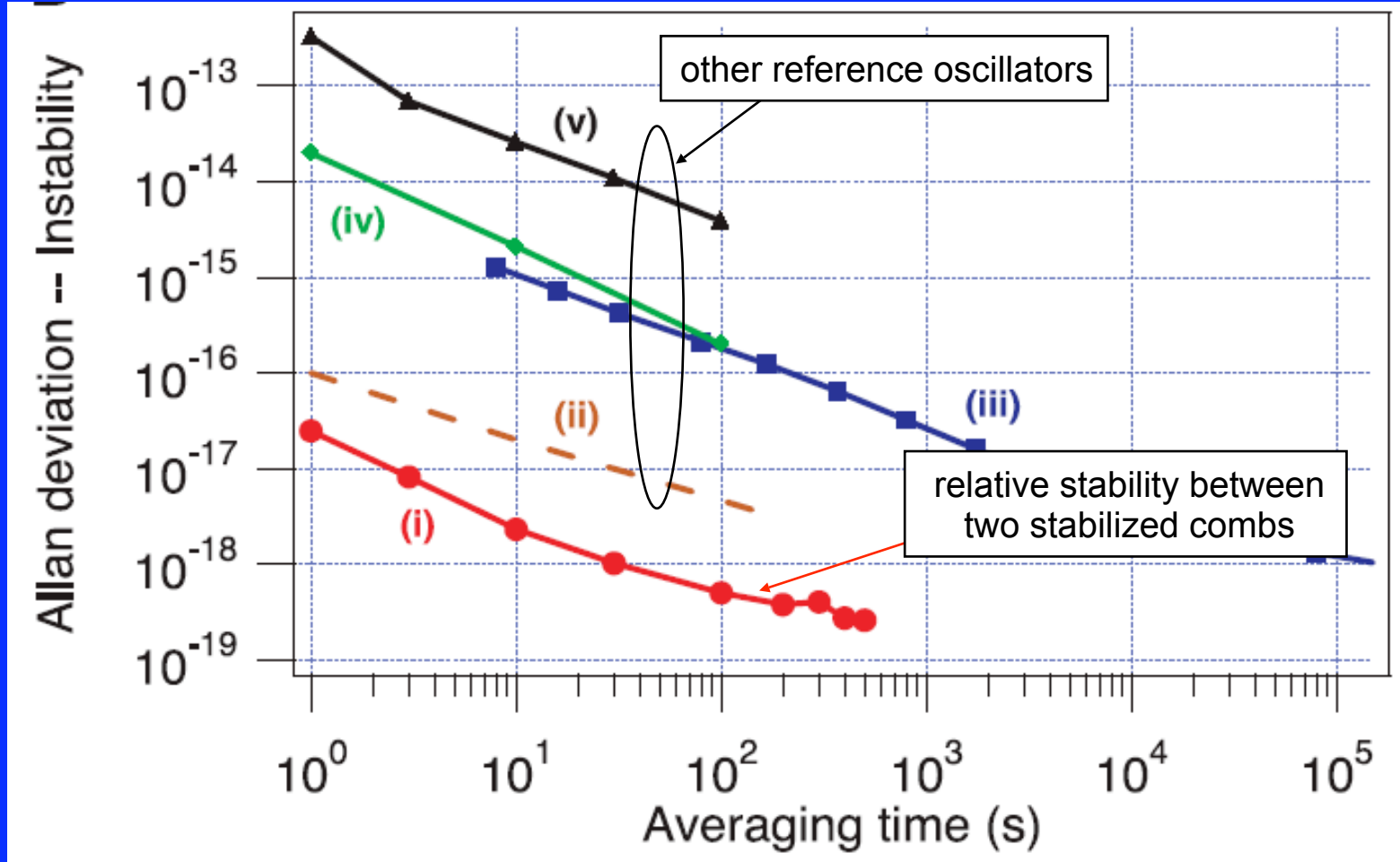
L.-S. Ma, Z. Bi, A. Bartels, *et al.*, Science **303**, 1843 (2004).



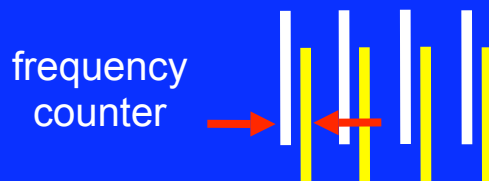
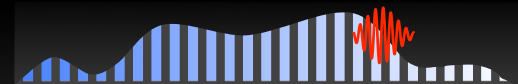
first step: establish frequency stability of comb



L.-S. Ma, Z. Bi, A. Bartels, *et al.*, Science **303**, 1843 (2004).

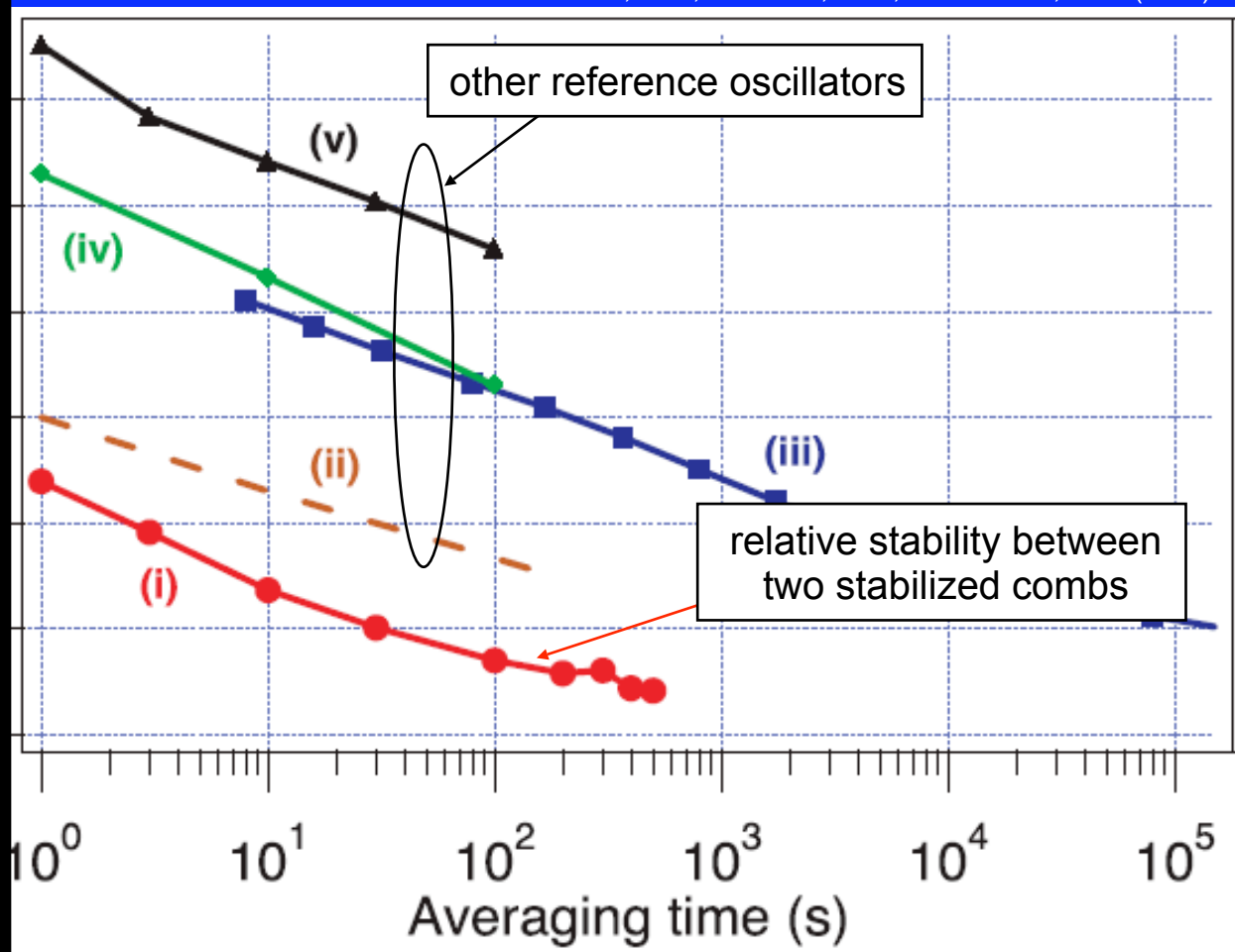


first step: establish frequency stability of comb

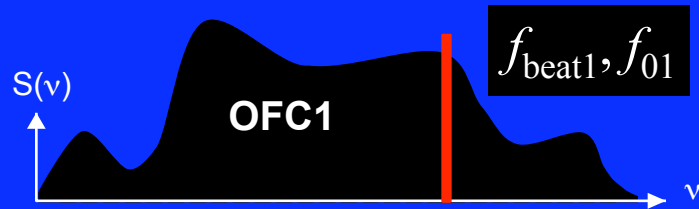
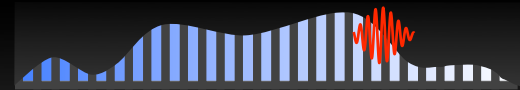


L.-S. Ma, Z. Bi, A. Bartels, *et al.*, Science **303**, 1843 (2004).

?

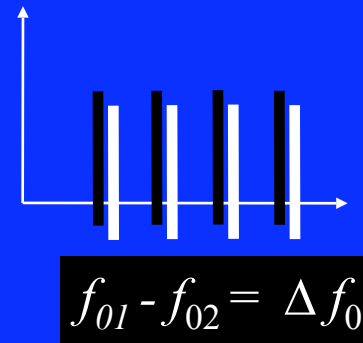
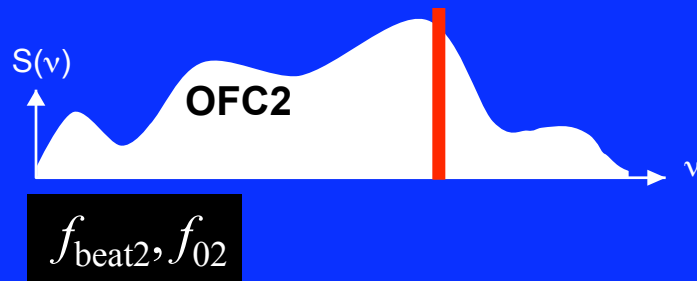


methods for measuring optical coherence

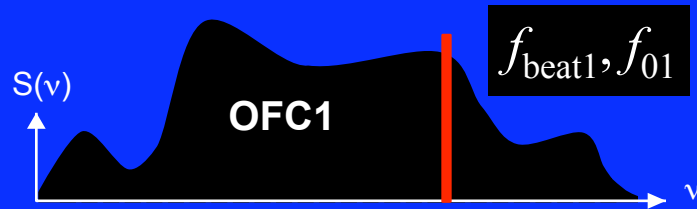
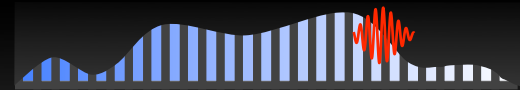


relative phase noise measurement

to compare different spectral regions,
...can extract RF parameter from each region

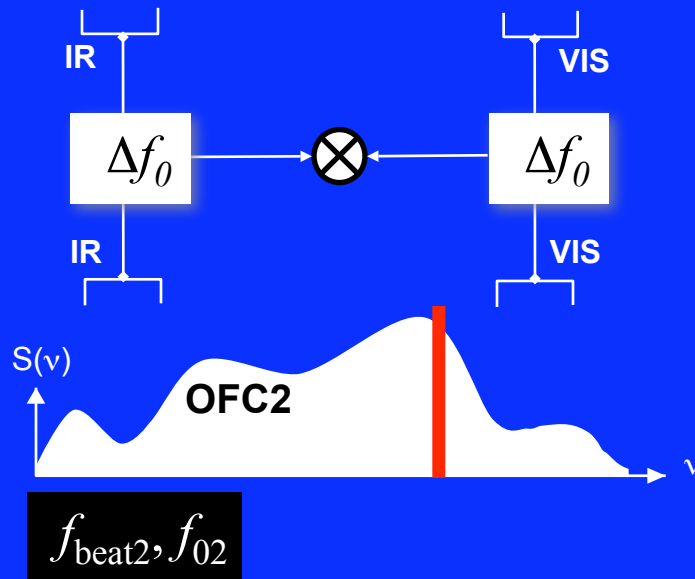


methods for measuring optical coherence

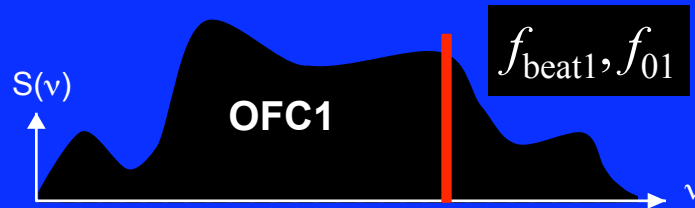
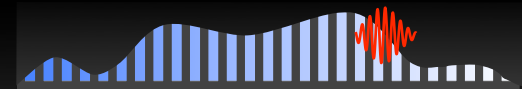


relative phase noise measurement

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methods for measuring optical coherence

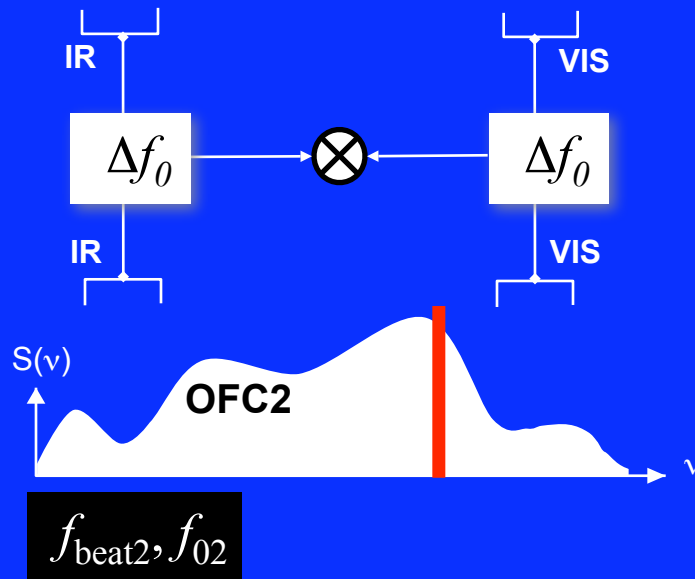


relative phase noise measurement

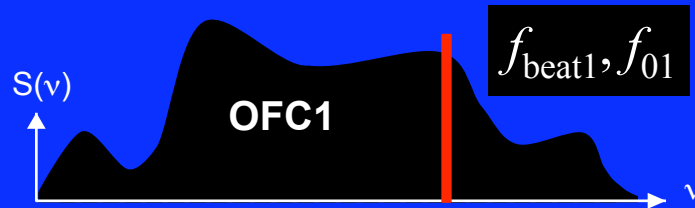
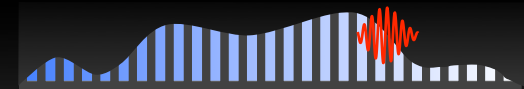
to compare different spectral regions,
...can extract RF parameter from each region

with this technique we can:
§ downconvert optical noise into RF parameter
§ compare noise at different spectral regions

...that is, look at dynamics of comb...

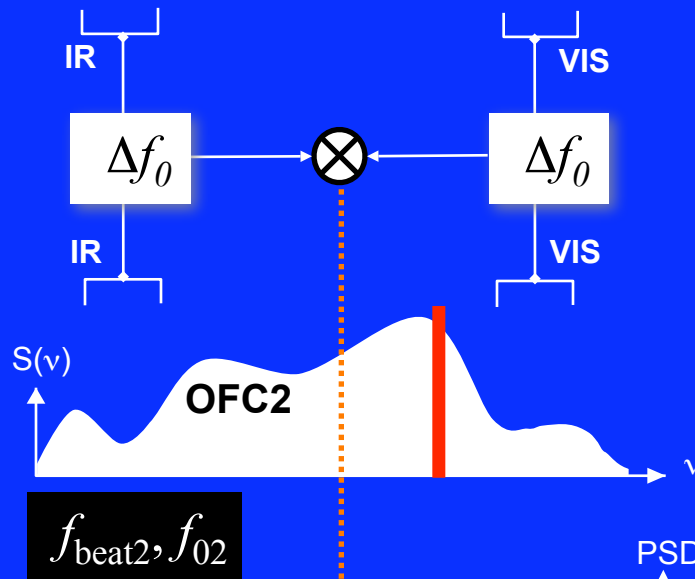


methods for measuring optical coherence



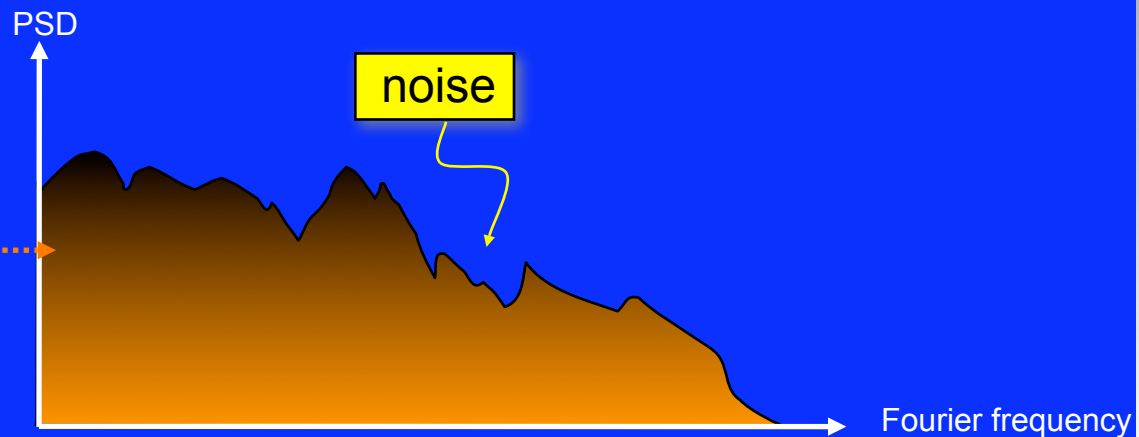
relative phase noise measurement

to compare different spectral regions,
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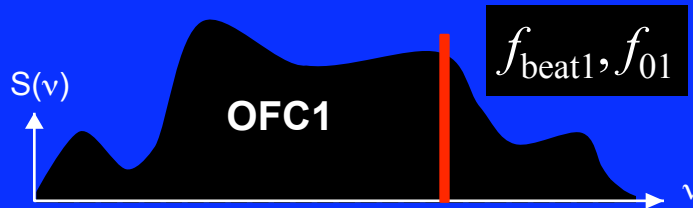
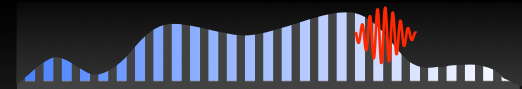


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methods for measuring optical coherence



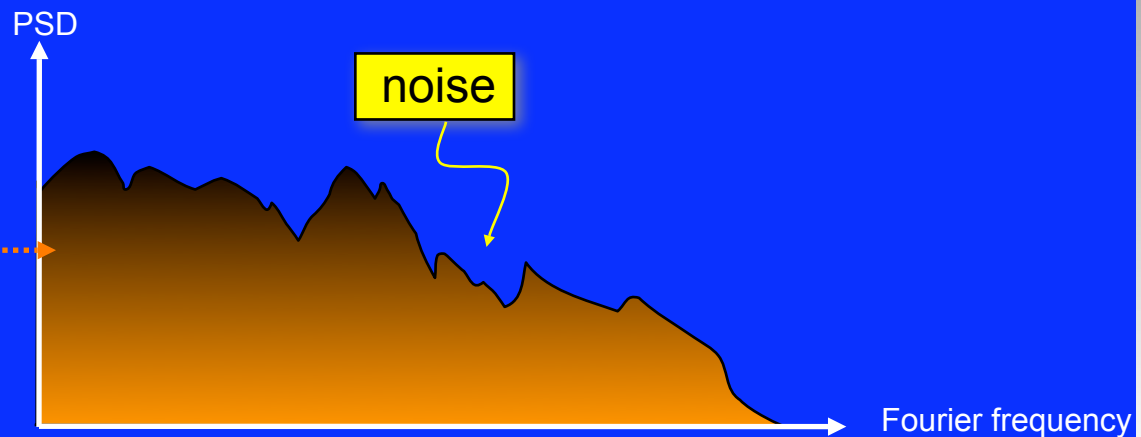
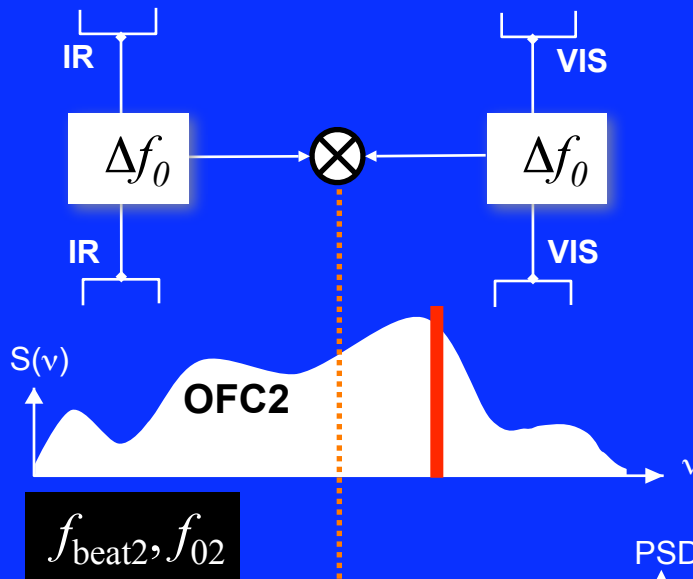
relative phase noise measurement

to compare different spectral regions,
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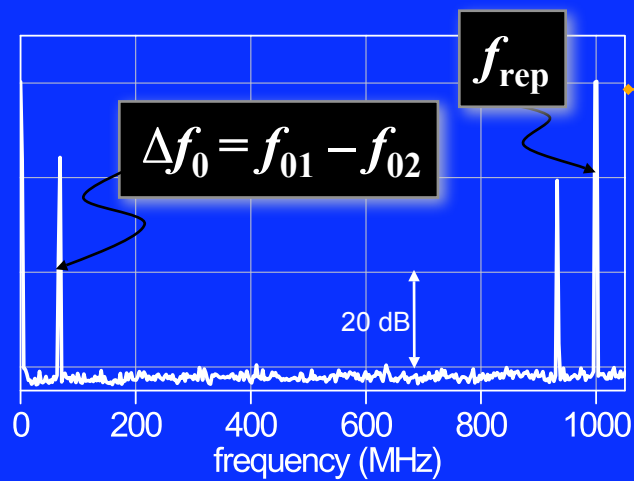
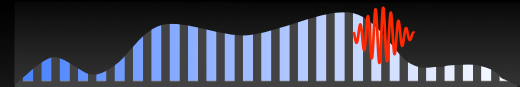
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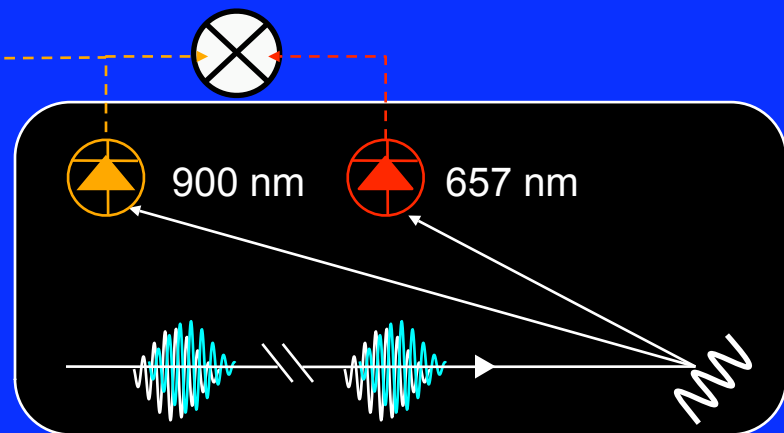
§ how does the phase noise vary across comb?
§ can the comb equation predict the measured noise?



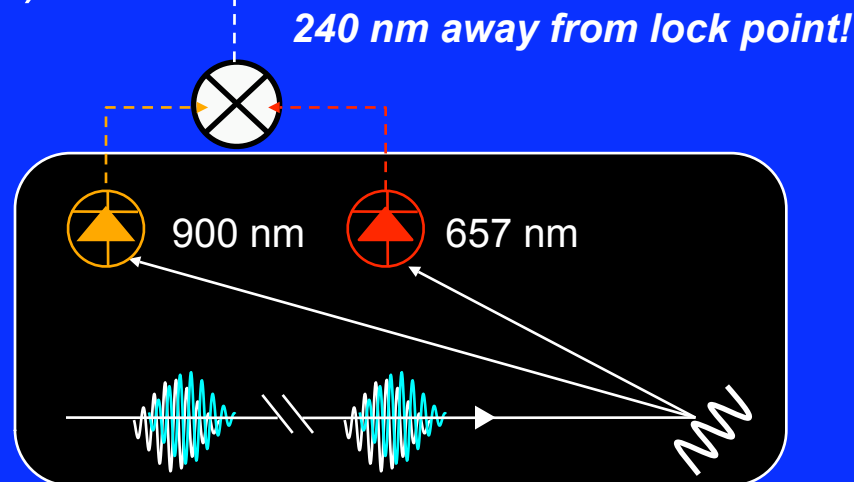
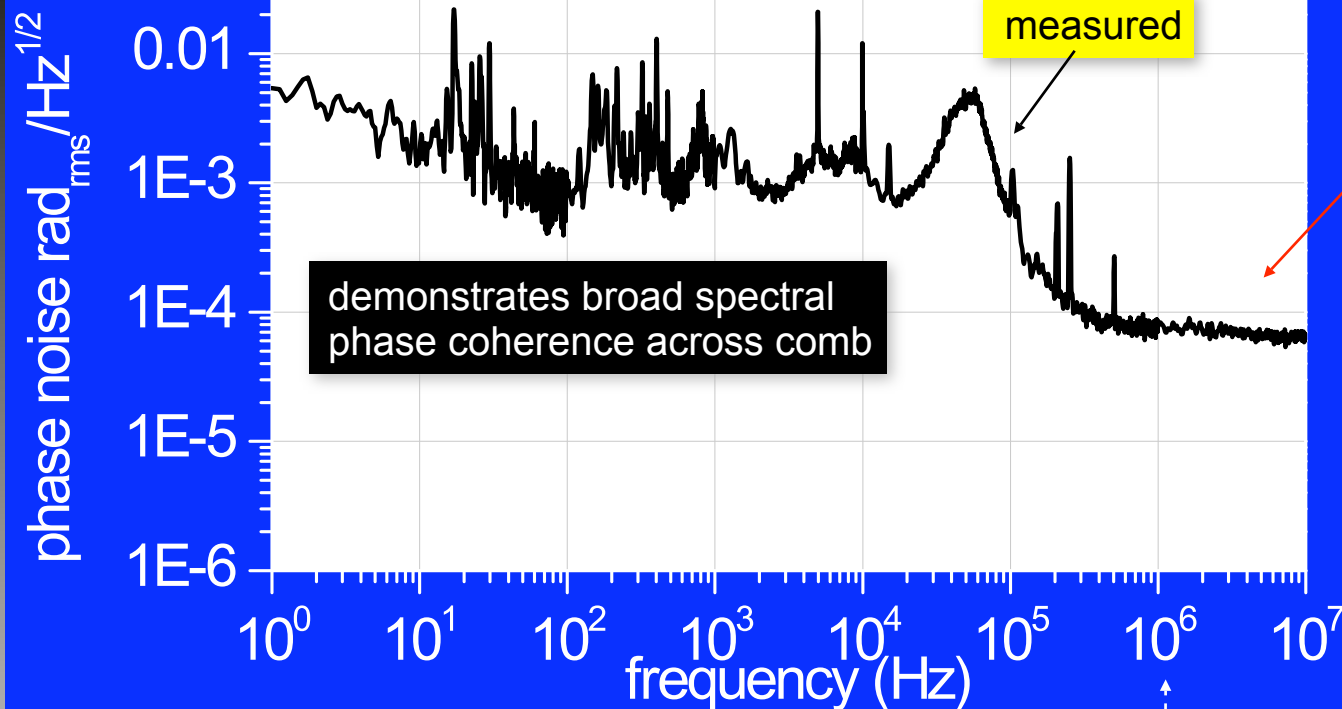
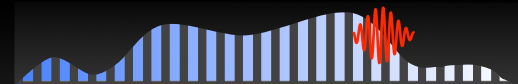
relative noise between lock point and region 230 nm away



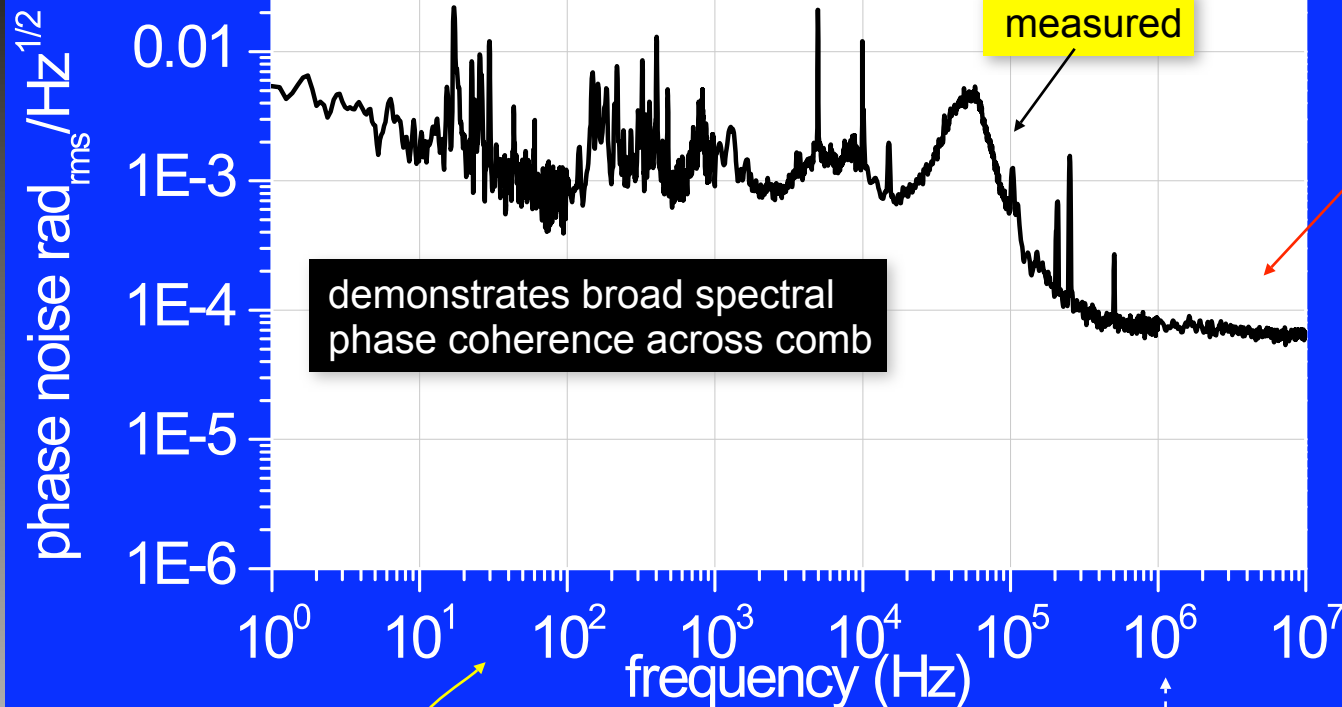
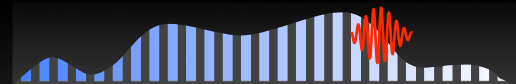
240 nm away from lock point!



relative noise between lock point and region 230 nm away

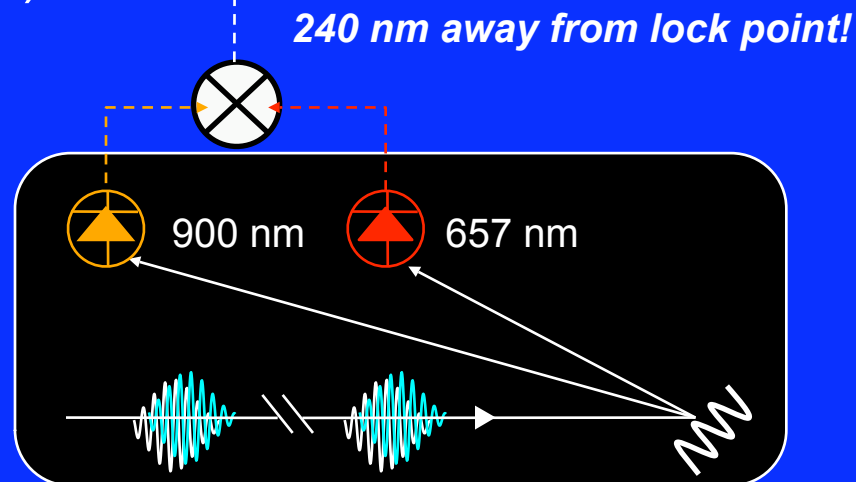


relative noise between lock point and region 230 nm away

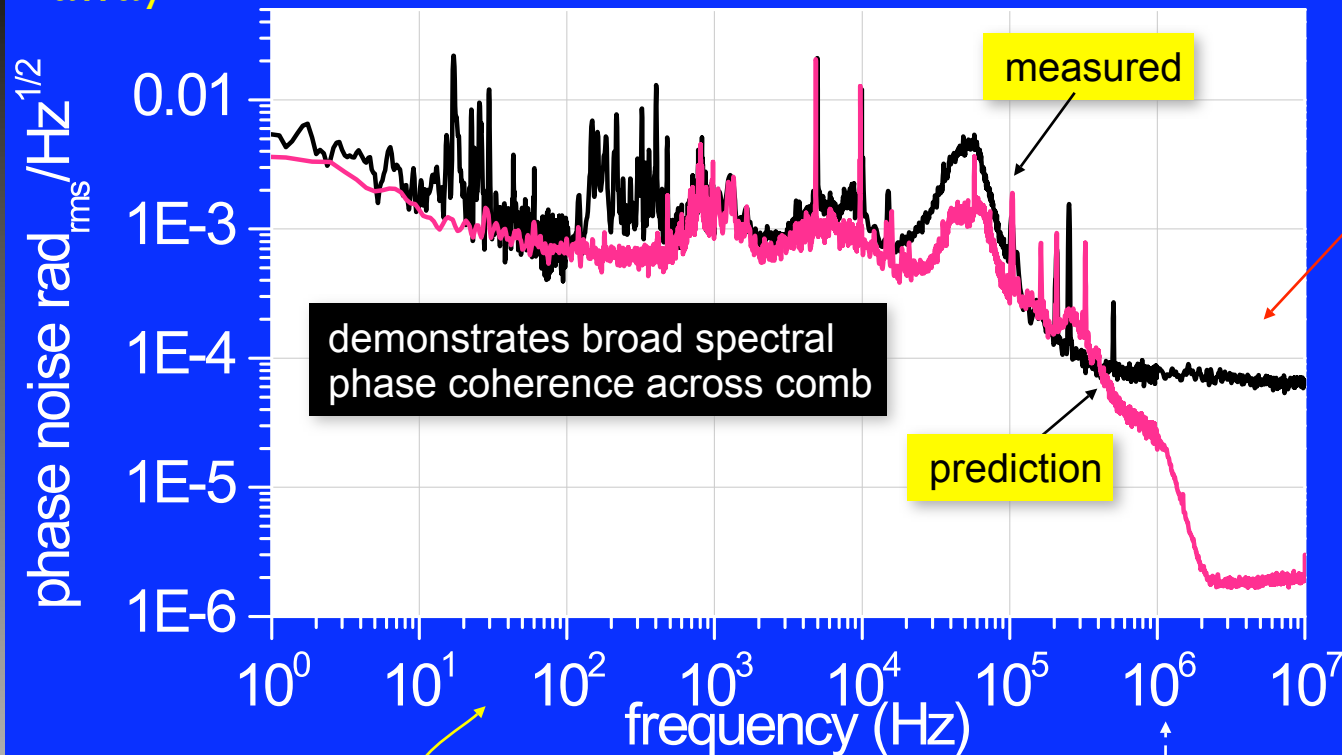
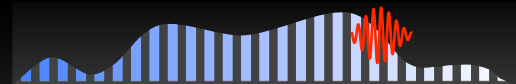


low level noise
milliradian/Hz^{1/2}
on optical signal

sub-fs timing jitter

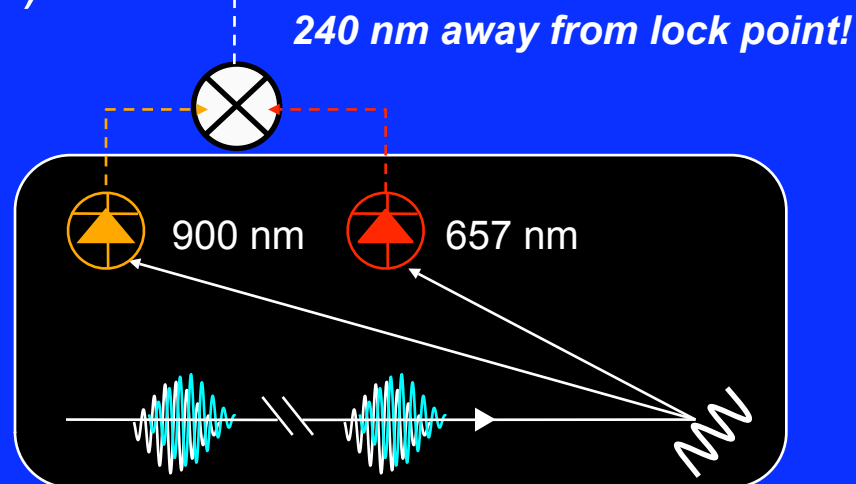


relative noise between lock point and region 230 nm away

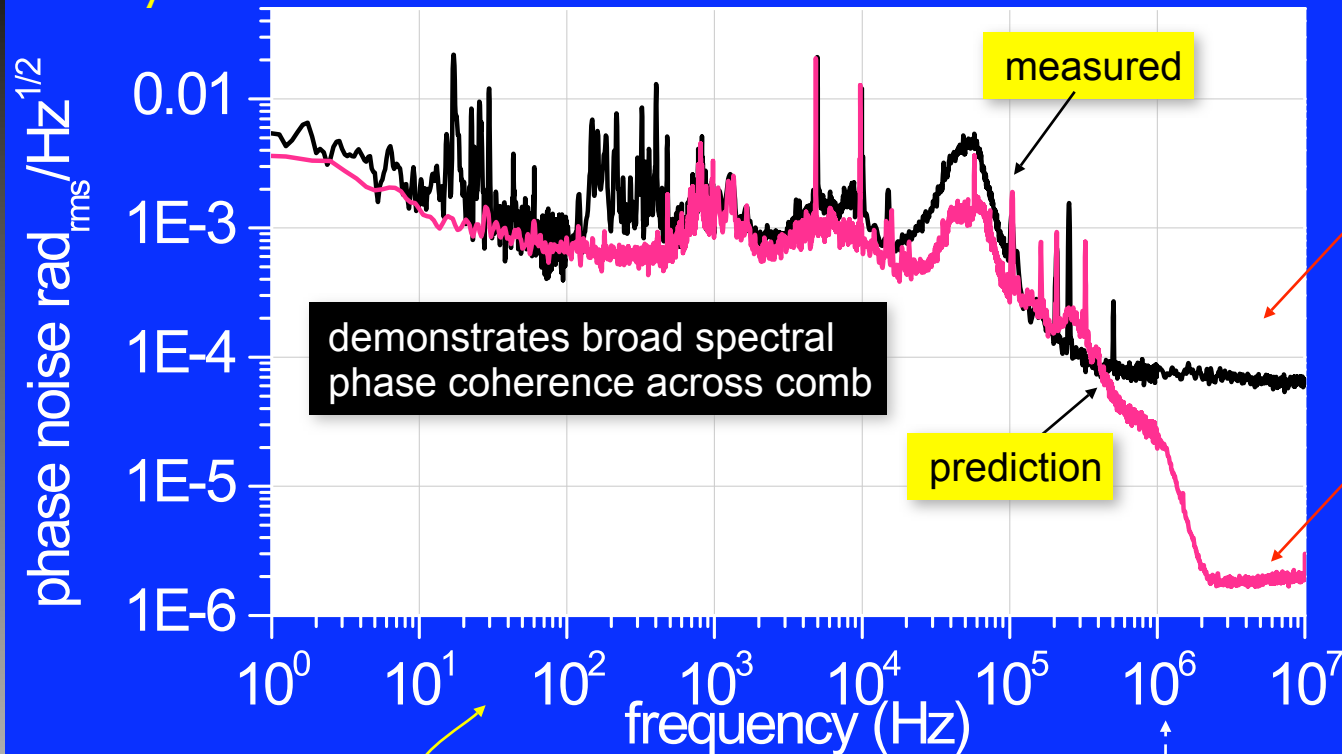
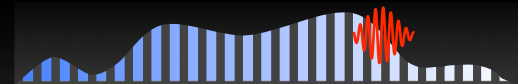


**low level noise
milliradian/Hz^{1/2}
on optical signal**

sub-fs timing jitter



relative noise between lock point and region 230 nm away



limited by
measurement
noise floor

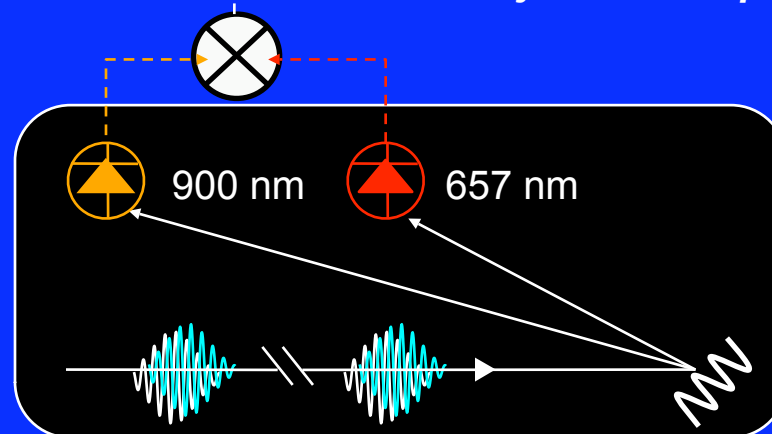
using comb equation,
we predict:

$$S_{\Phi,m,n}(f) = (r^m - r^n)^2 \sum S_i(f)$$

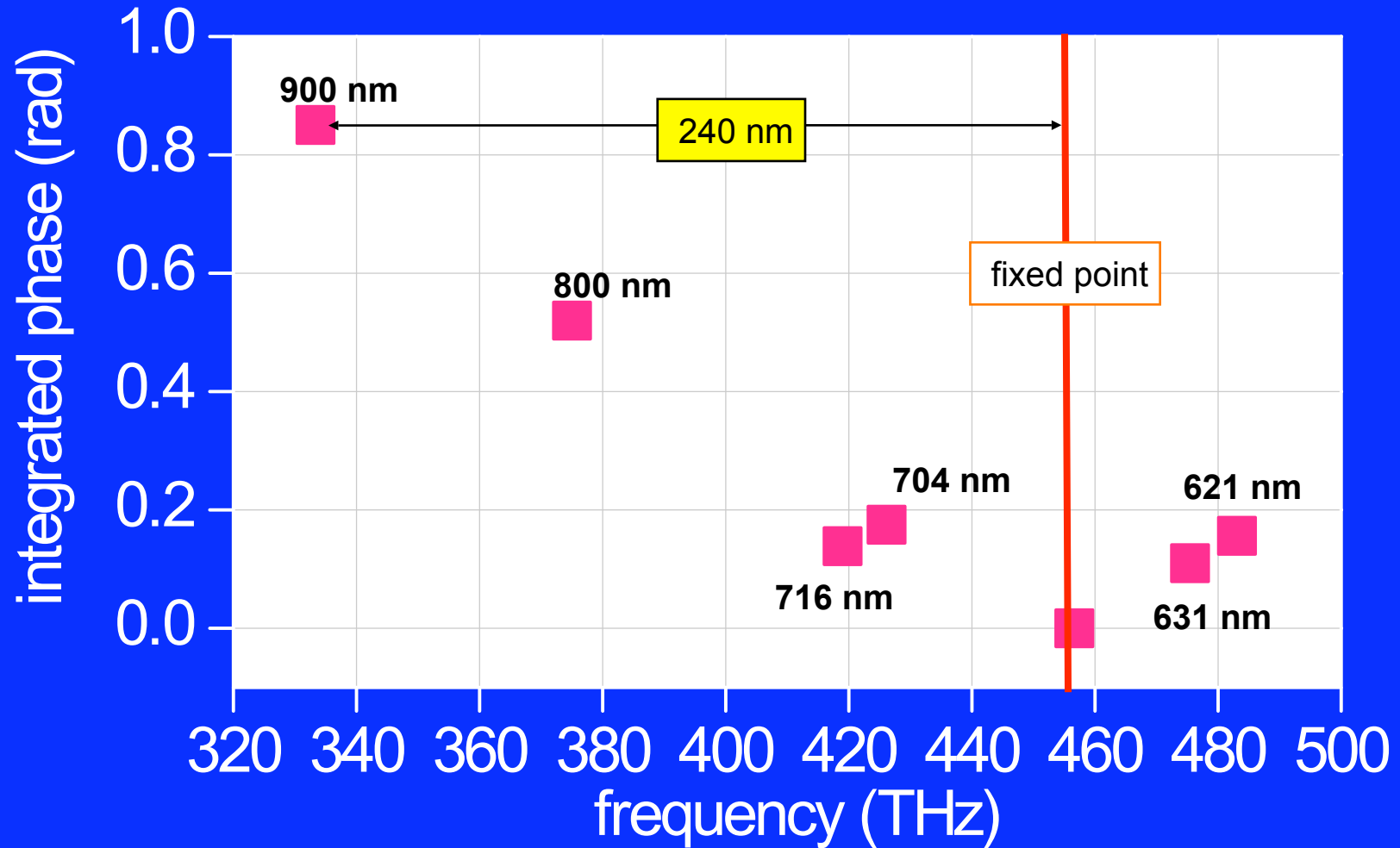
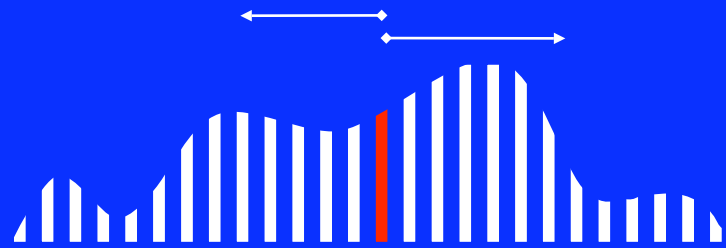
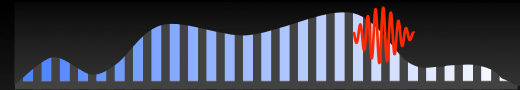
low level noise
milliradian/Hz^{1/2}
on optical signal

sub-fs timing jitter

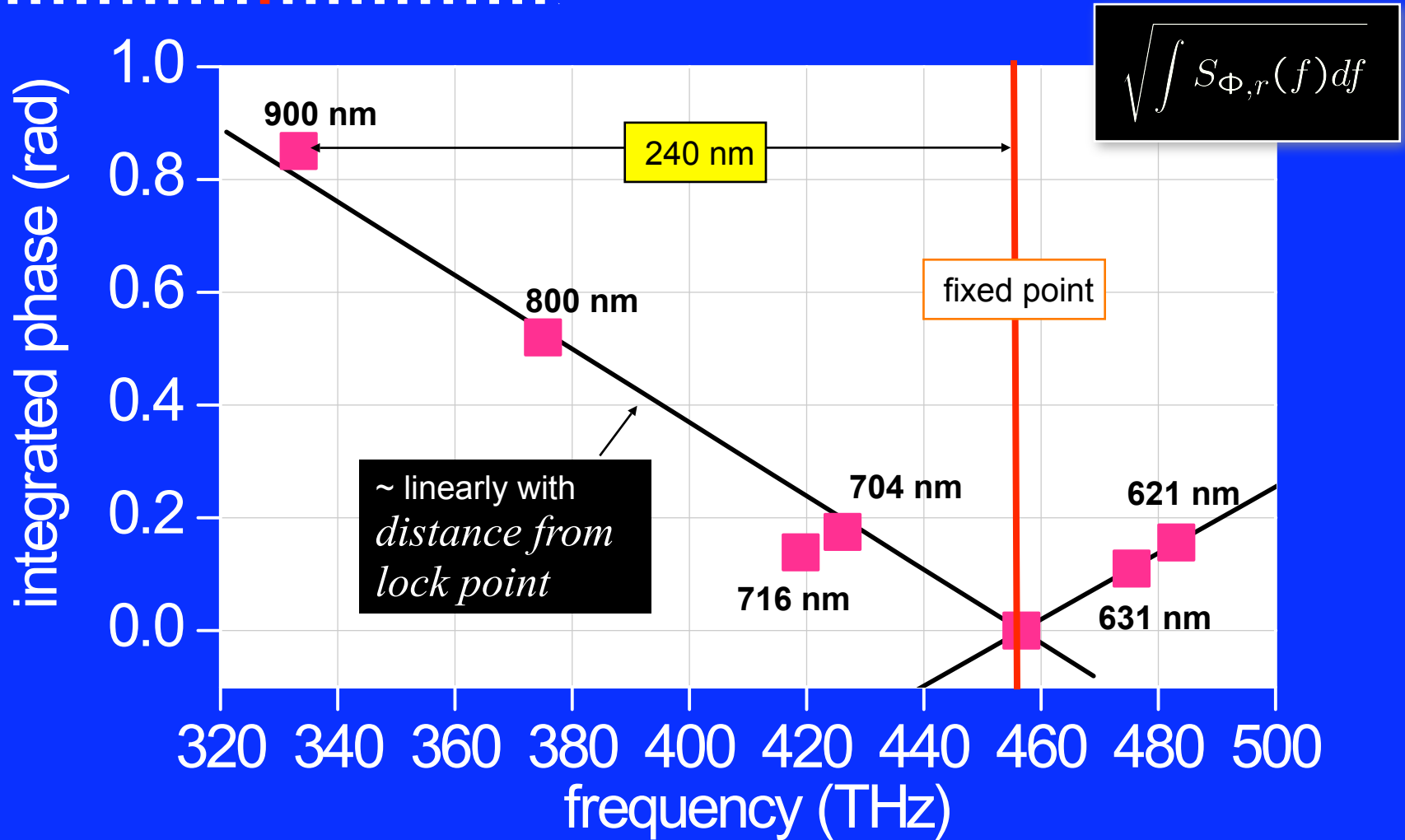
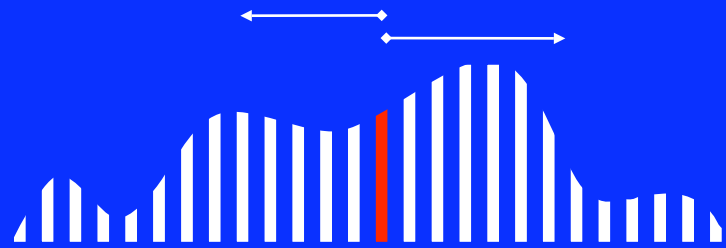
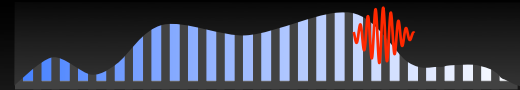
240 nm away from lock point!



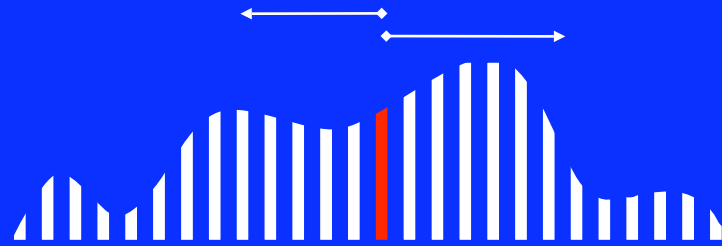
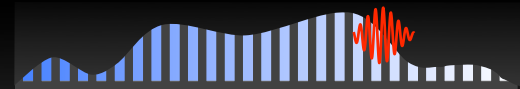
scaling of phase away from locked point



scaling of phase away from locked point



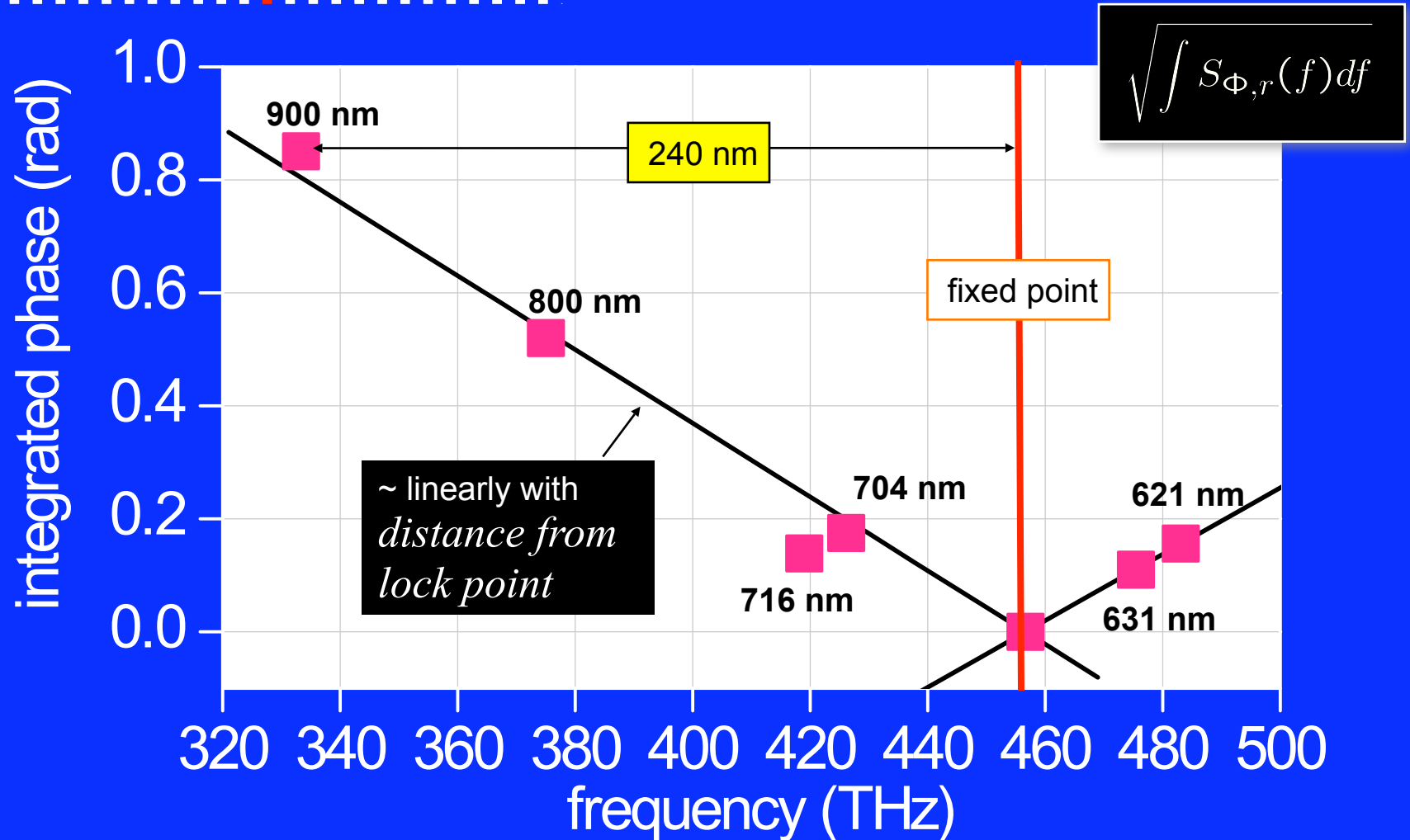
scaling of phase away from locked point



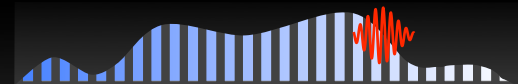
§ first demonstration scaling of phase noise across comb

§ comb equation can predict phase dynamics

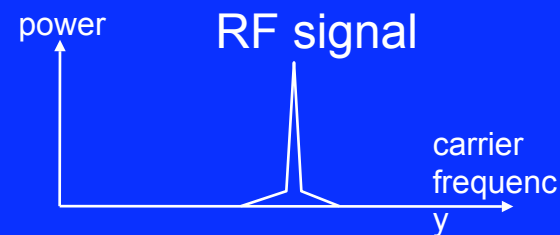
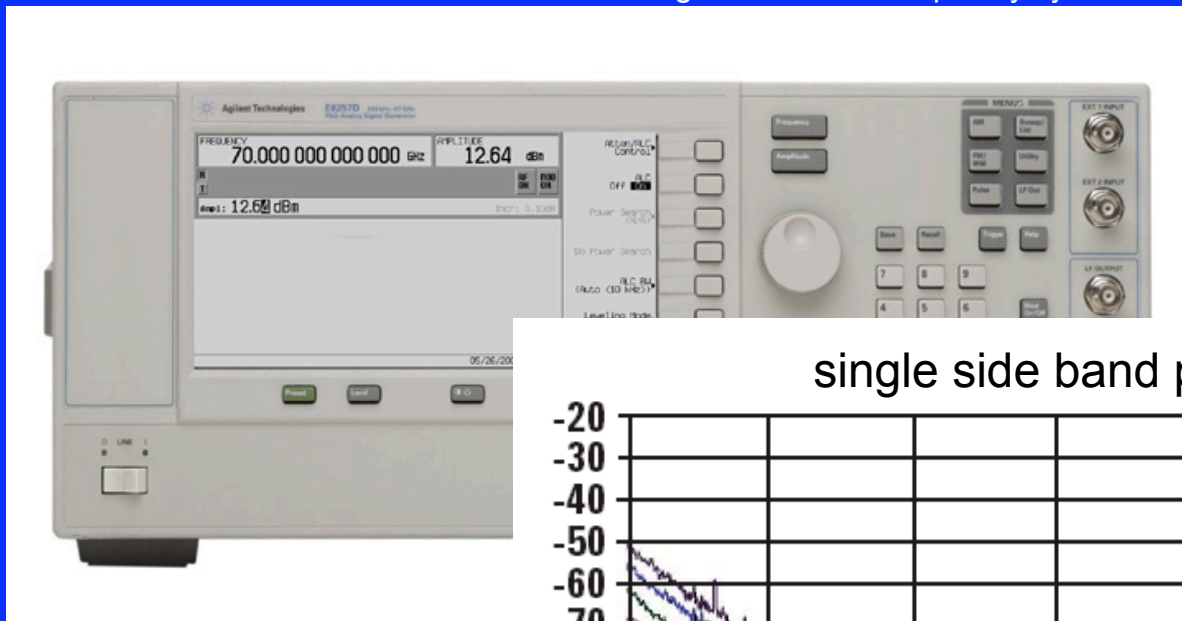
§ shows substantial coherence across comb



microwave frequency synthesizers



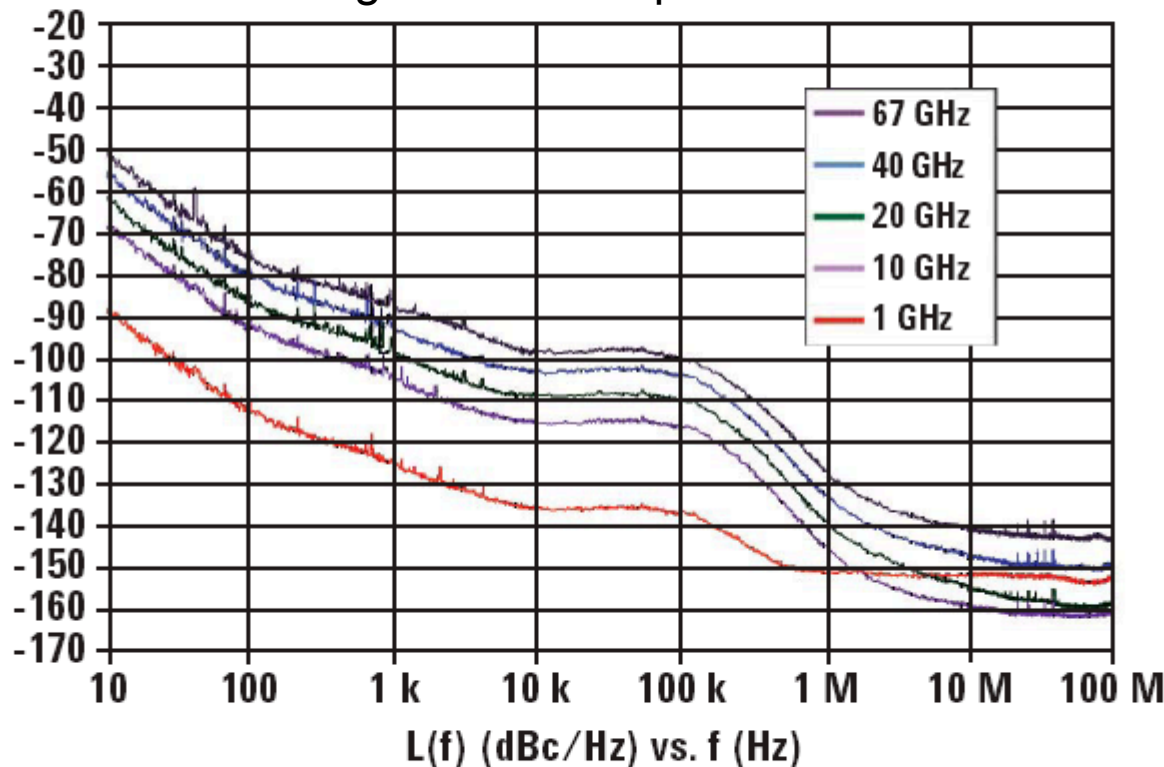
Agilent E8257D frequency synthesizer

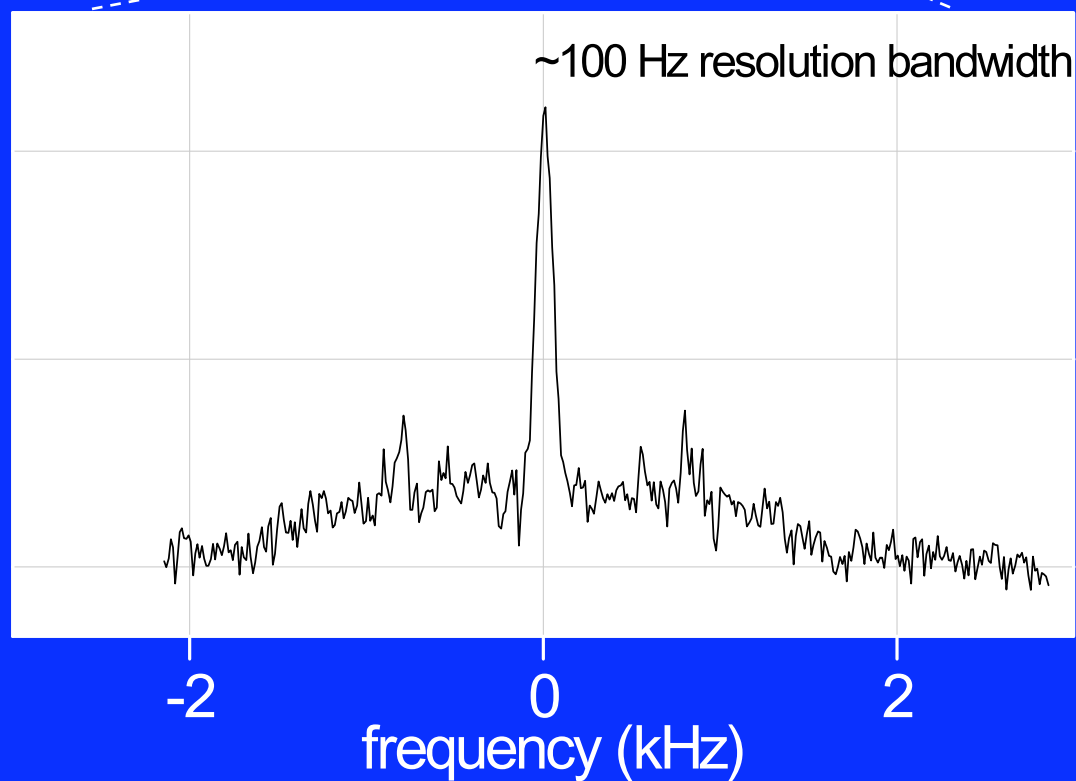
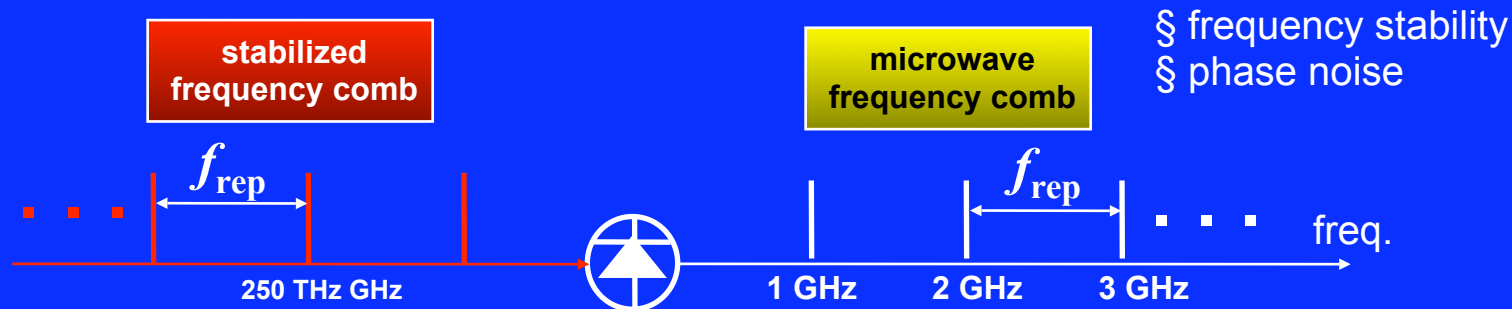
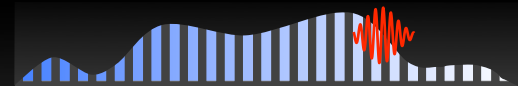


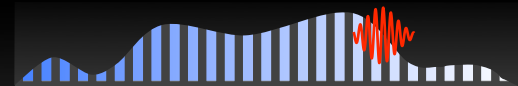
specifications

250 kHz – 20 GHz +
low phase noise

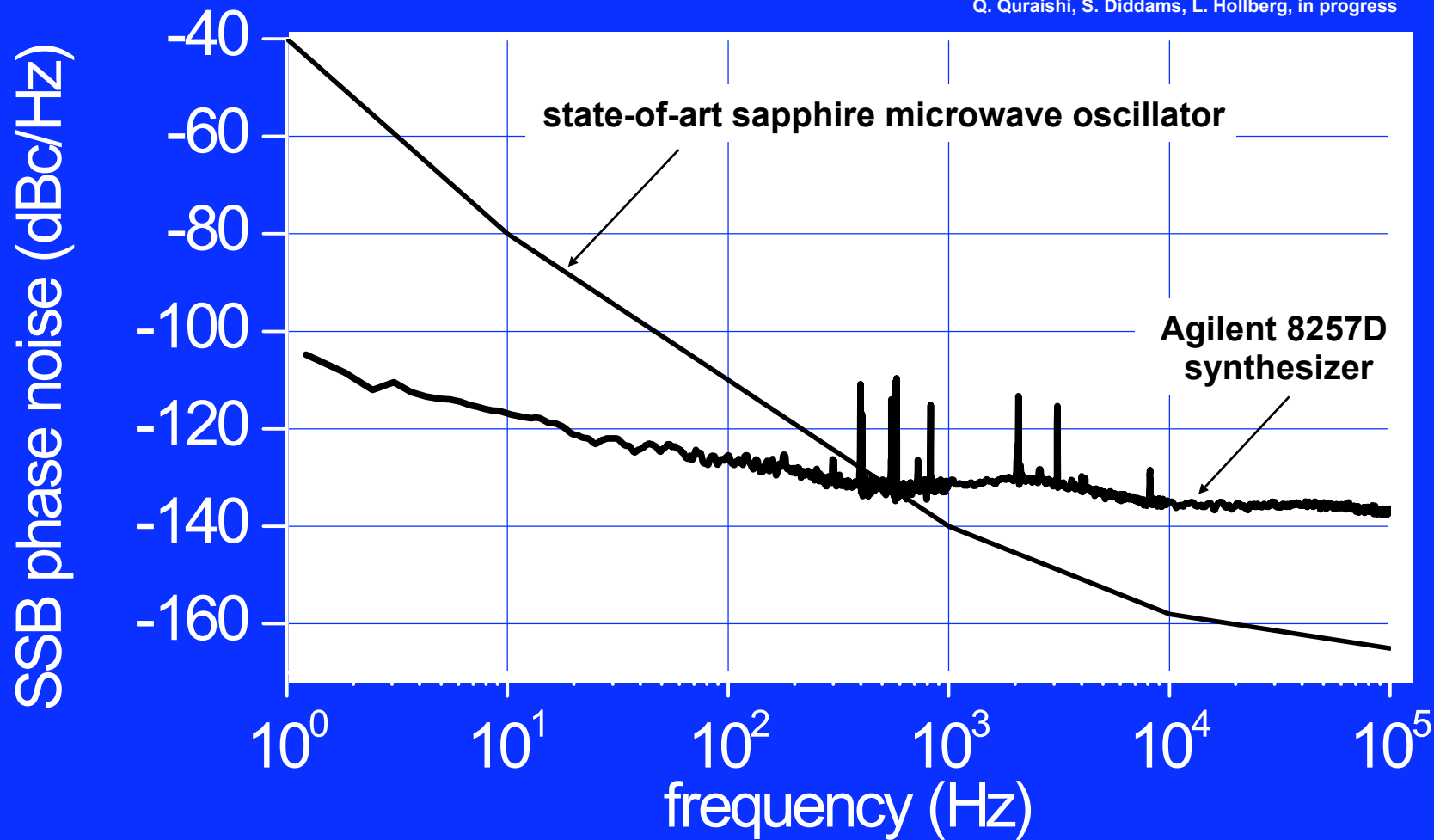
single side band phase noise

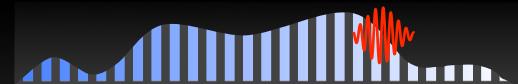




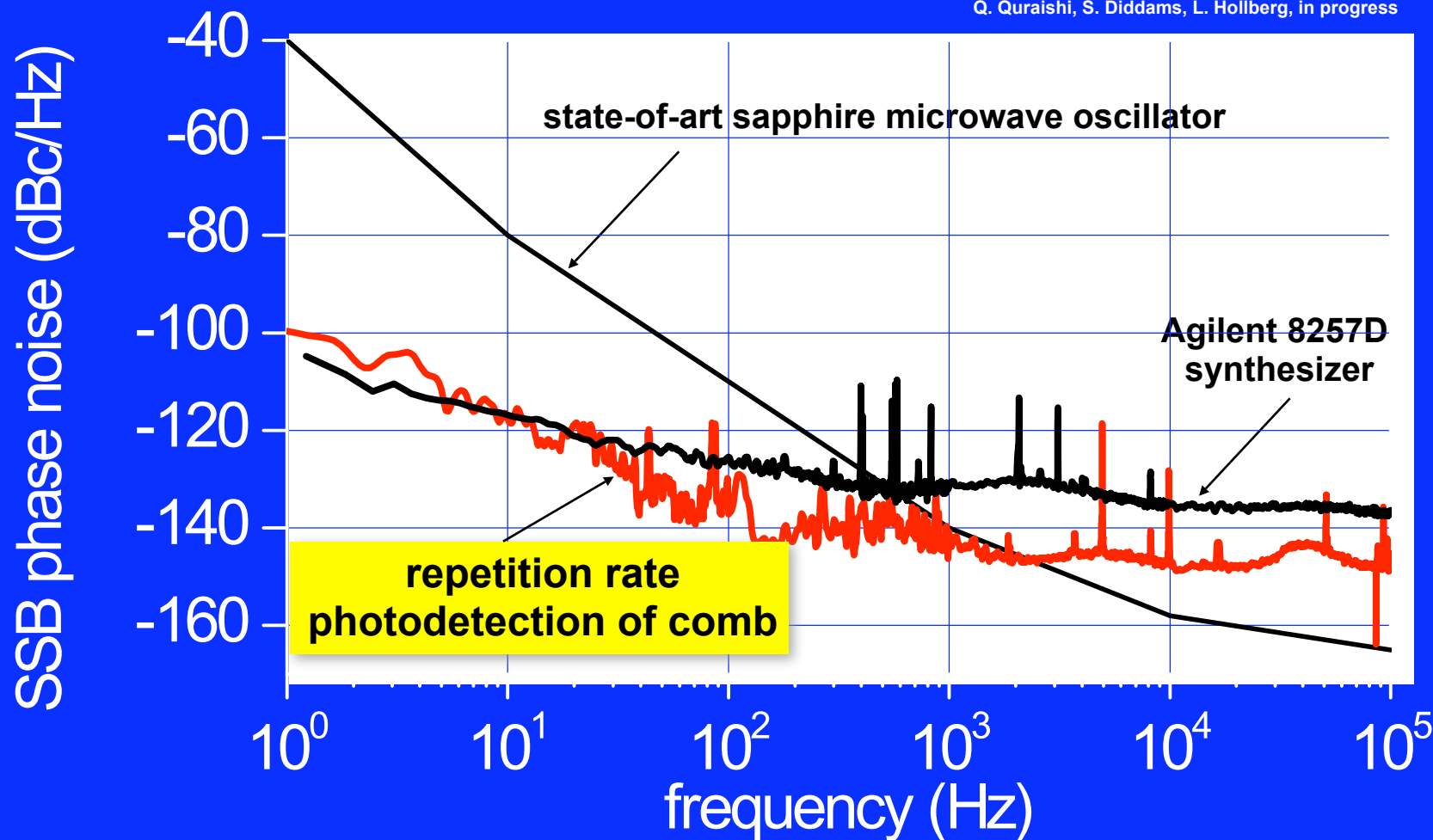


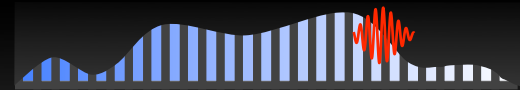
Q. Quraishi, S. Diddams, L. Hollberg, in progress



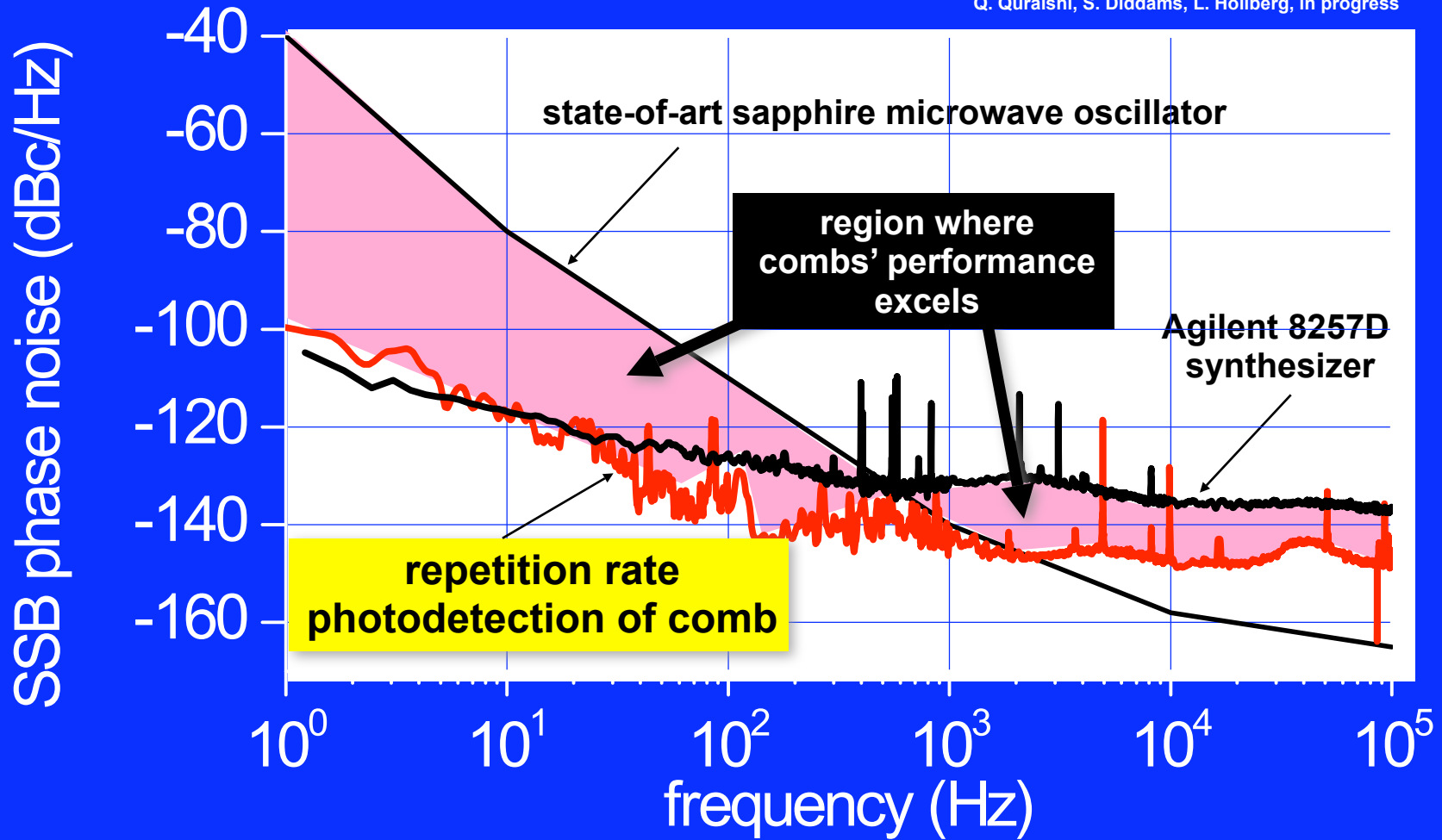


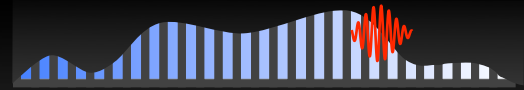
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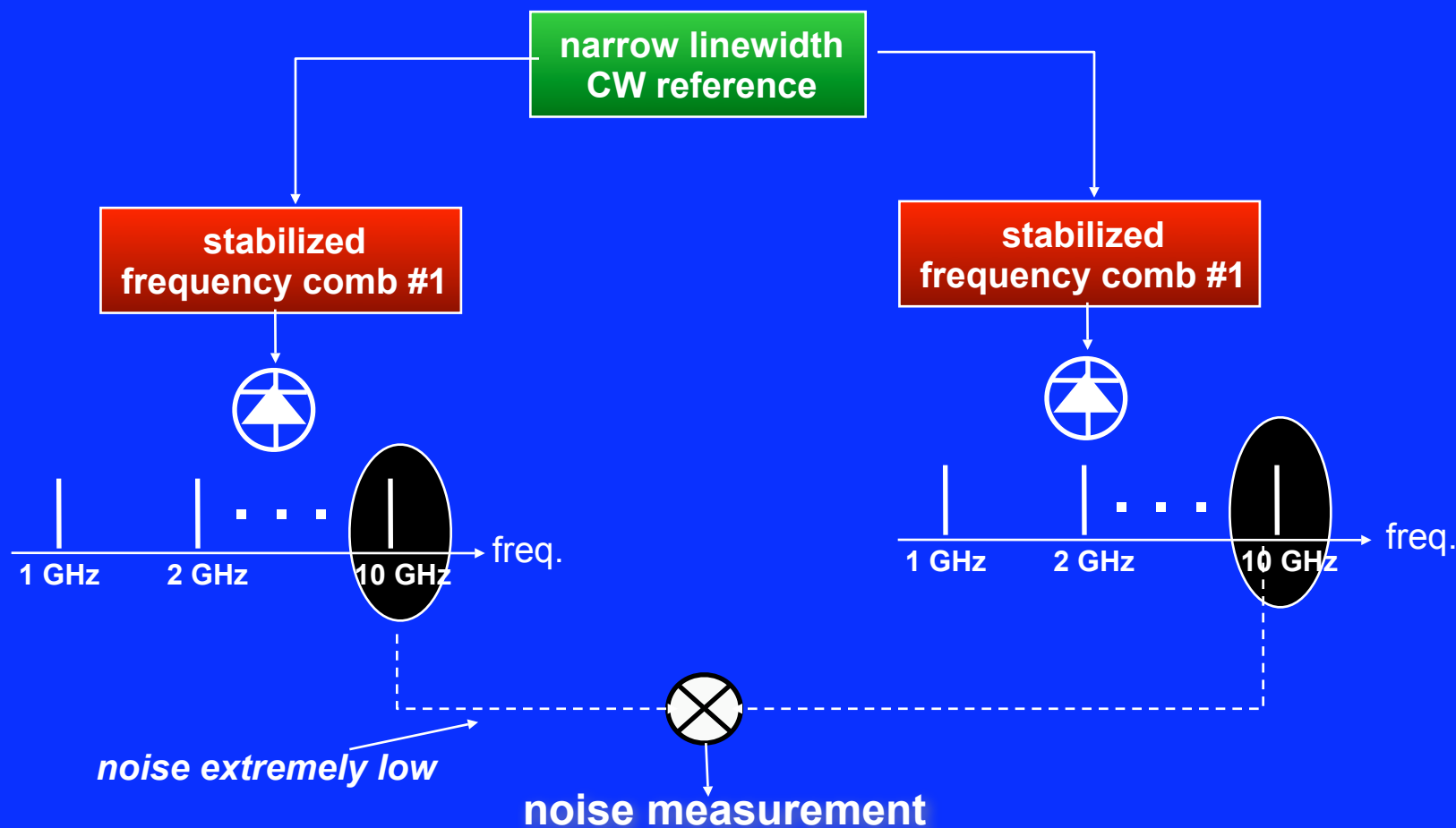
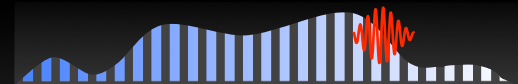
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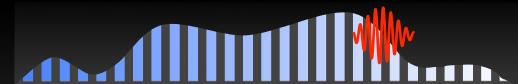


if noise is low than other microwave sources...

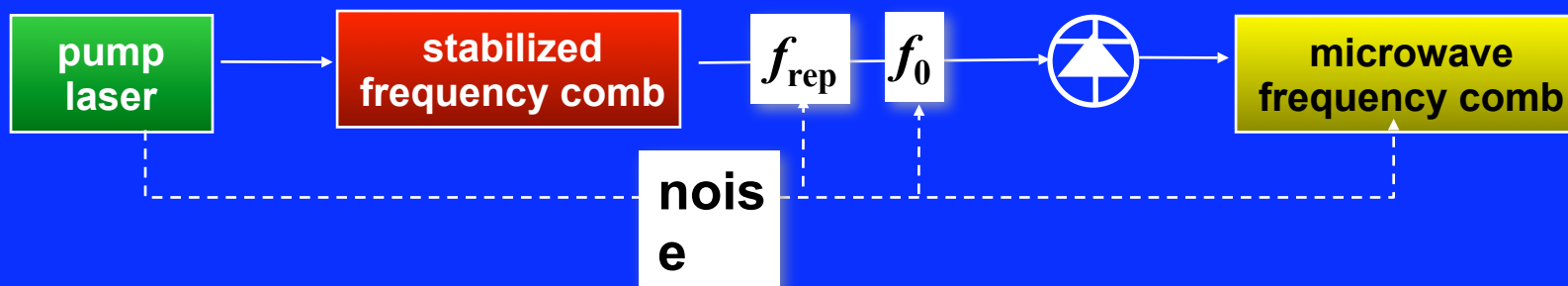
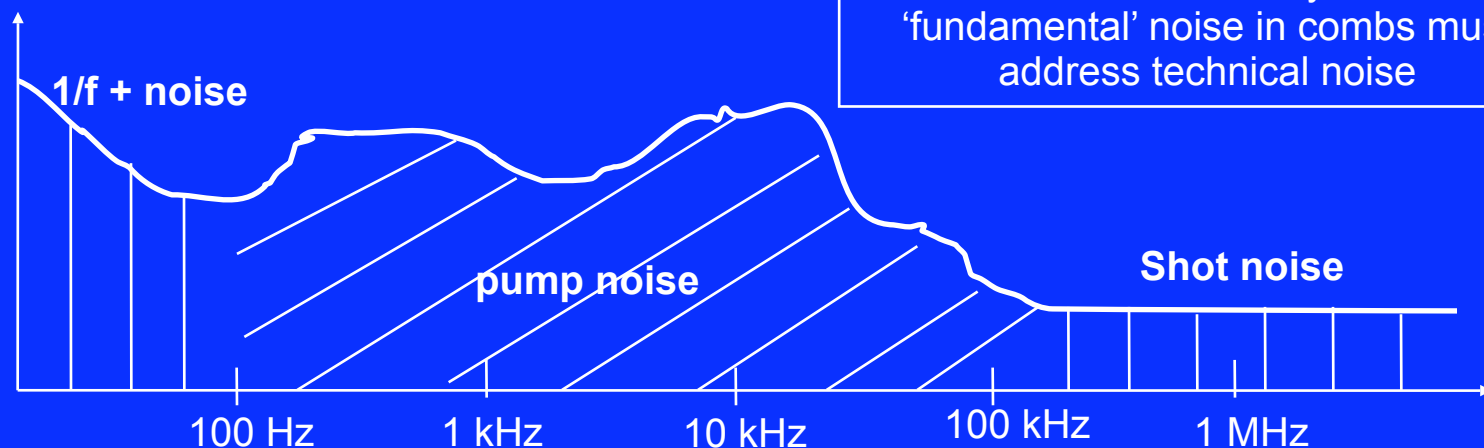
how was the measurement done?

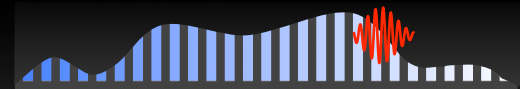


***microwave noise from each comb
so low that we can only measure
it by comparing to another comb.***

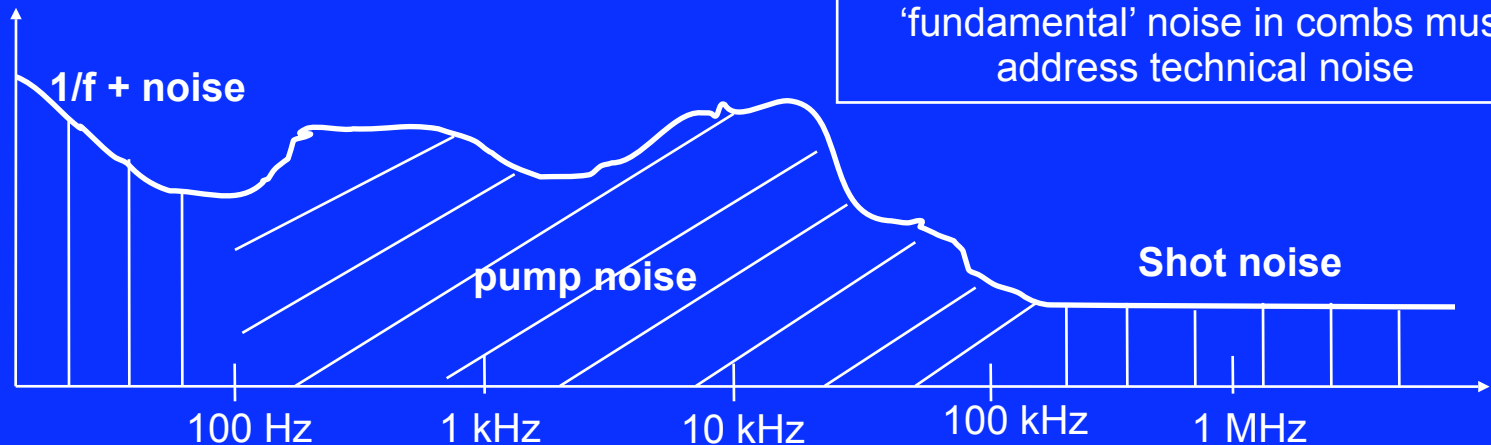


TiS phase noise
at 10 GHz



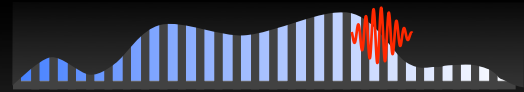


TiS phase noise
at 10 GHz



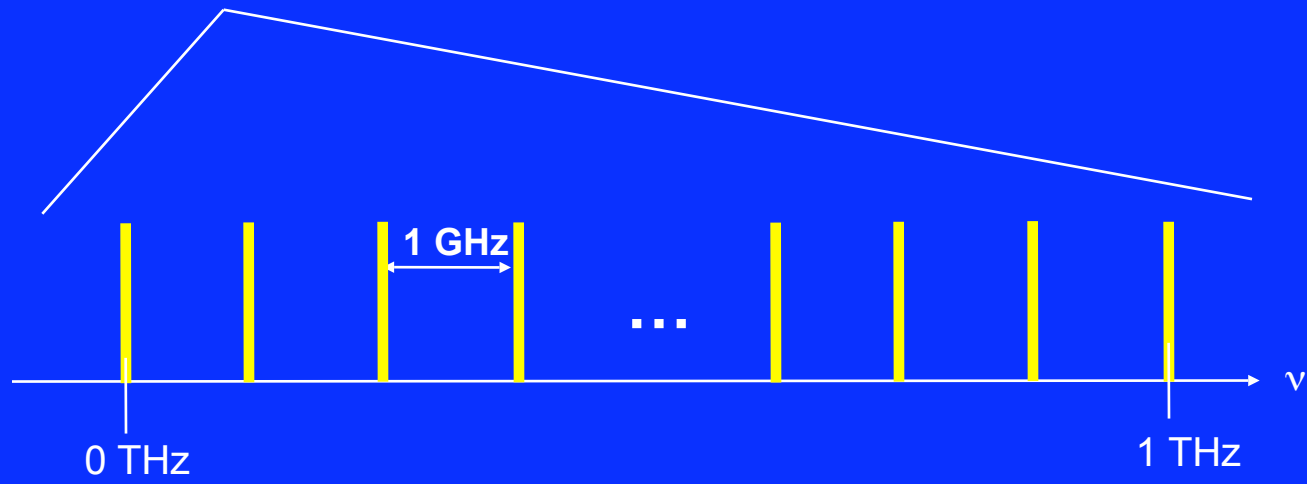
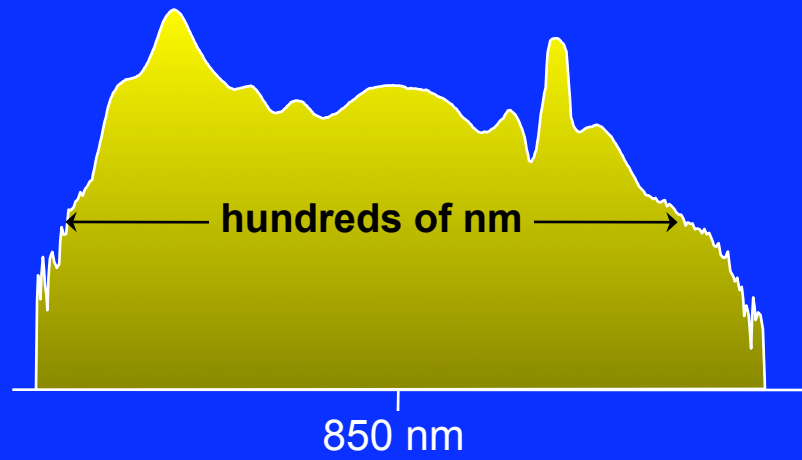
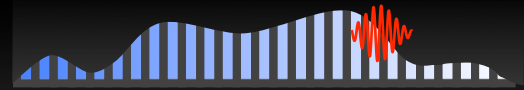
bottom line: before we try to measure
'fundamental' noise in combs must
address technical noise

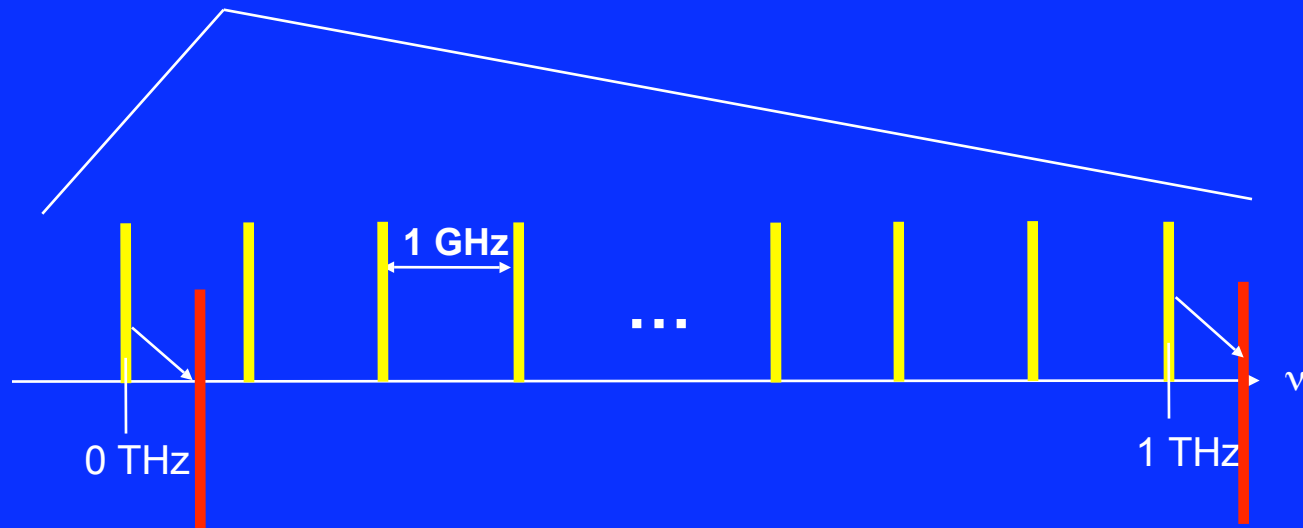
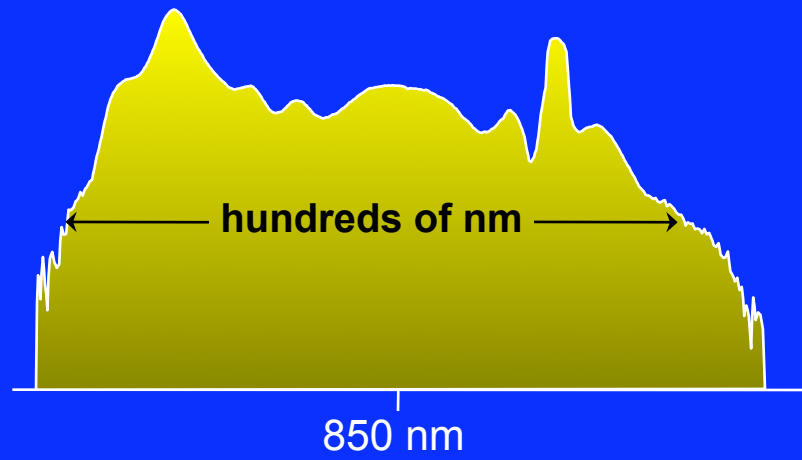
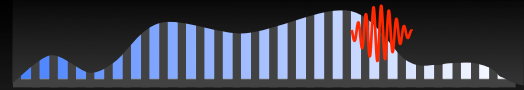
so far, technical noise
constitutes our most immediate challenge

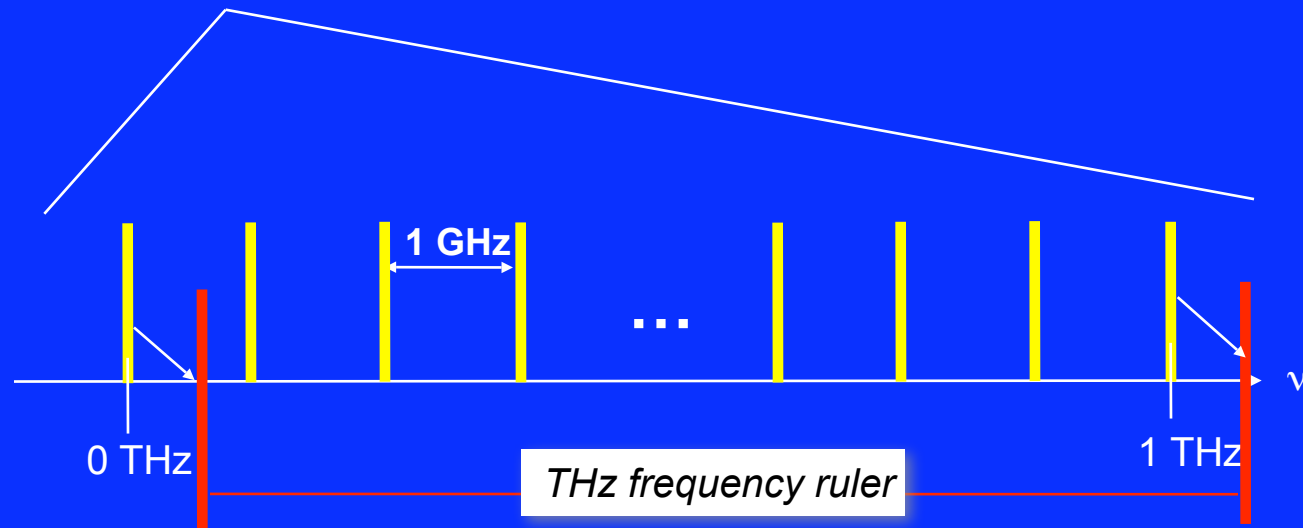
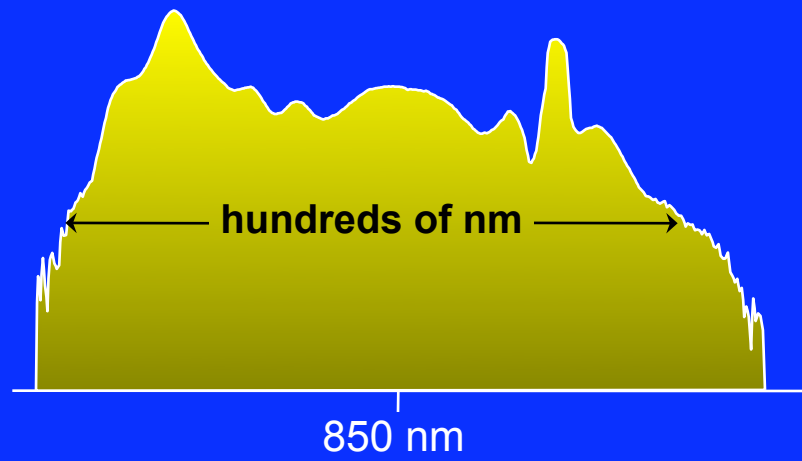
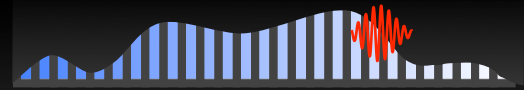


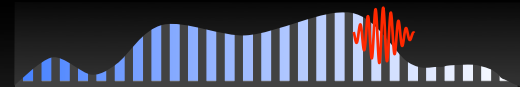
final example of comb application:

transfer the coherence of comb to terahertz domain



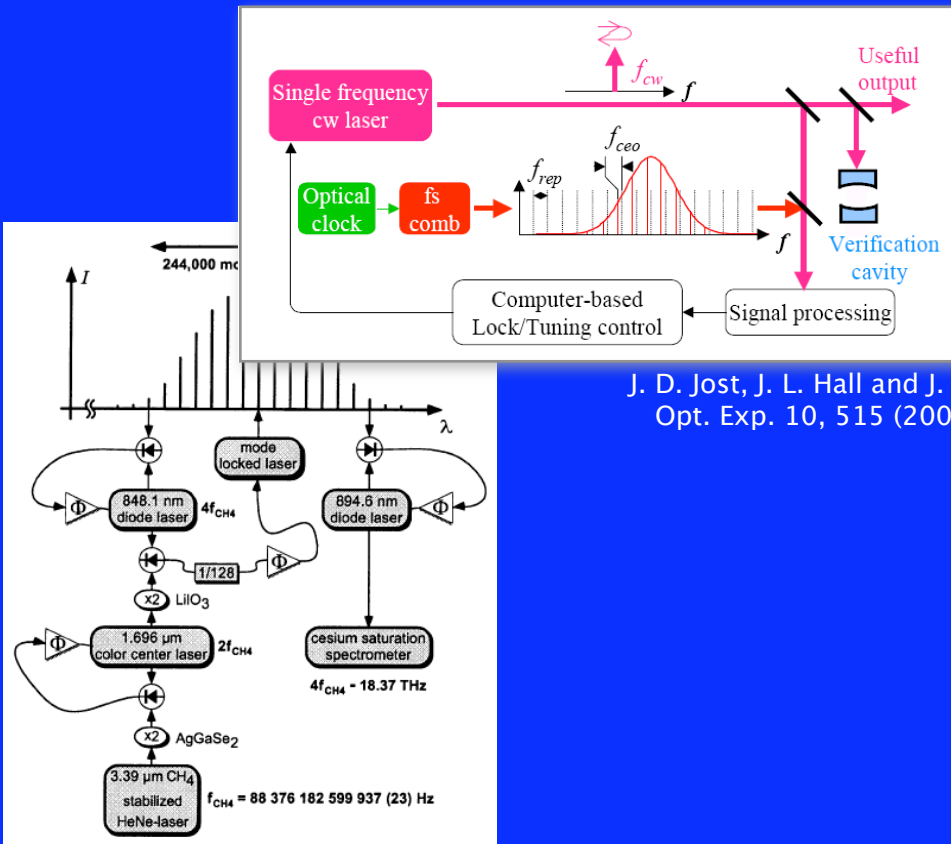






§ diode lasers referenced to optical frequency combs

1 THz \sim 0.3 μ m

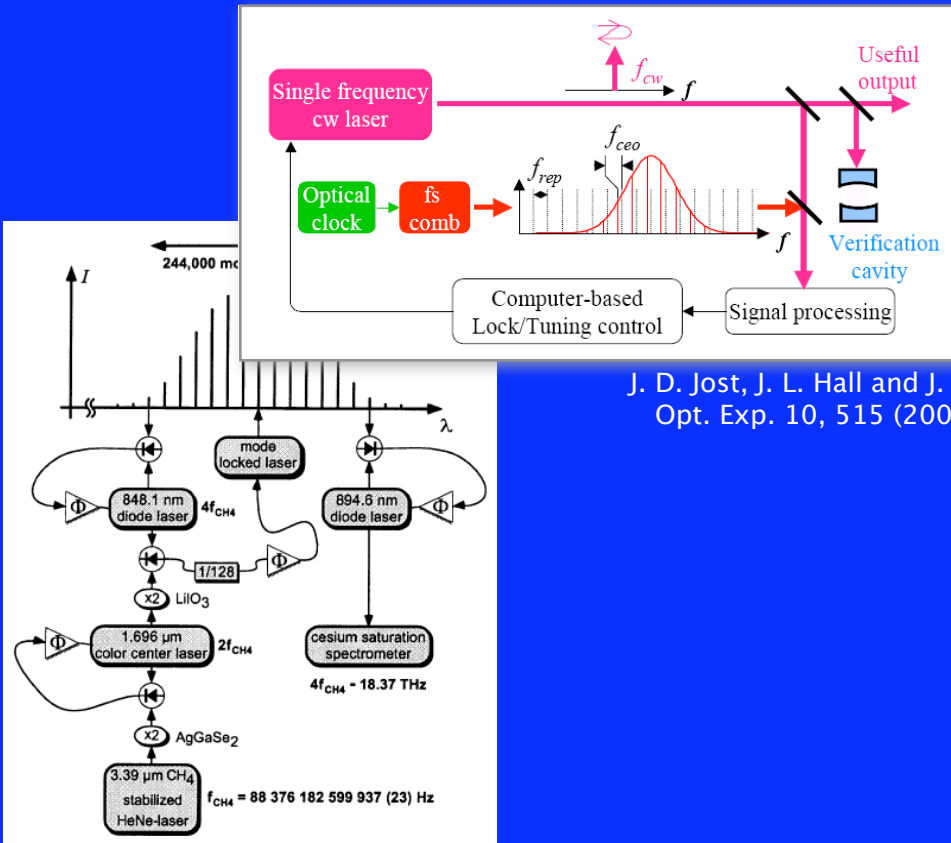


J. D. Jost, J. L. Hall and J. Ye
Opt. Exp. 10, 515 (2002).

Th. Udem, J. Reichert, R. Holzworth and
T. W. Hänsch, Phys. Rev. Lett. 82, 3568 (1999)

combs for referenced terahertz radiation

§ diode lasers referenced to optical frequency combs



J. D. Jost, J. L. Hall and J. Ye
Opt. Exp. 10, 515 (2002).

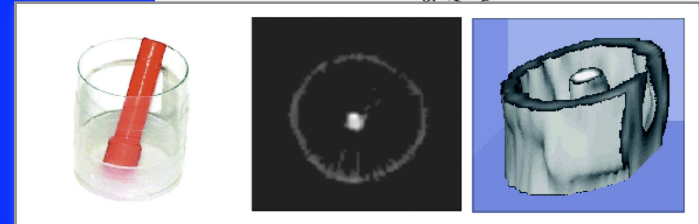
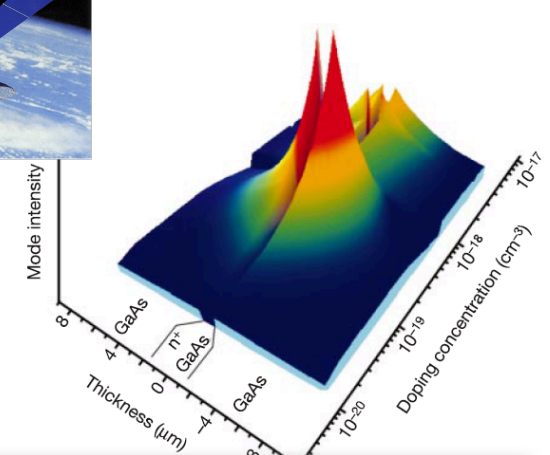
Th. Udem, J. Reichert, R. Holzworth and
T. W. Hänsch, Phys. Rev. Lett. 82, 3568 (1999)

§ THz generation and spectroscopy

0.1 – 10 THz

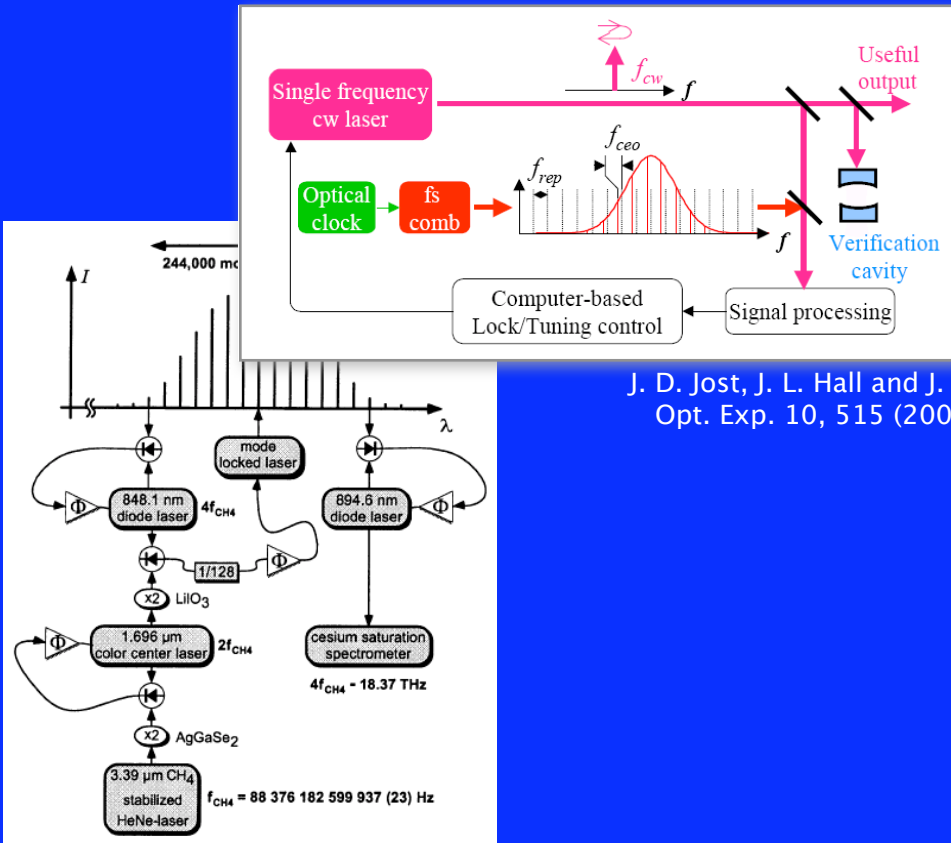
1 THz ~ 0.3 μm

R. Köhler, A. Tredicucci, F. Beltram,
et al., Nature 417, 156 (2002).



B. Ferguson and X. Zhang Nature Mat. 1, 26 (2002)

§ diode lasers referenced to optical frequency combs



J. D. Jost, J. L. Hall and J. Ye
Opt. Exp. 10, 515 (2002).

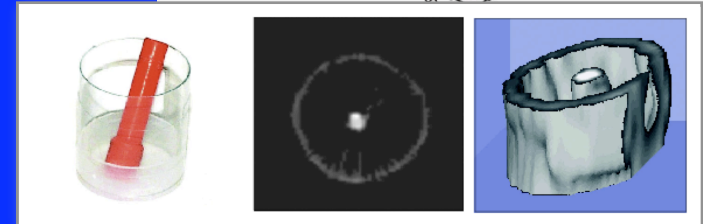
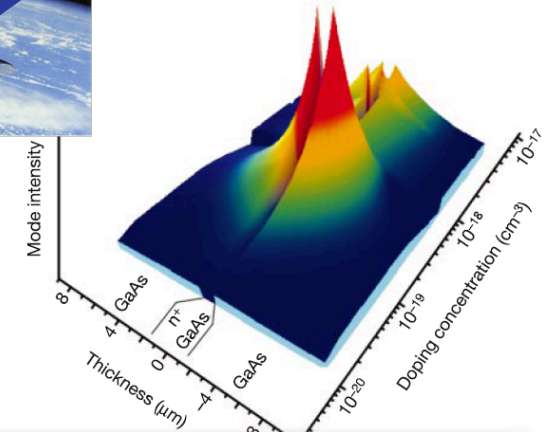
Th. Udem, J. Reichert, R. Holzworth and
T. W. Hänsch, Phys. Rev. Lett. 82, 3568 (1999)

§ THz generation and spectroscopy

0.1 – 10 THz

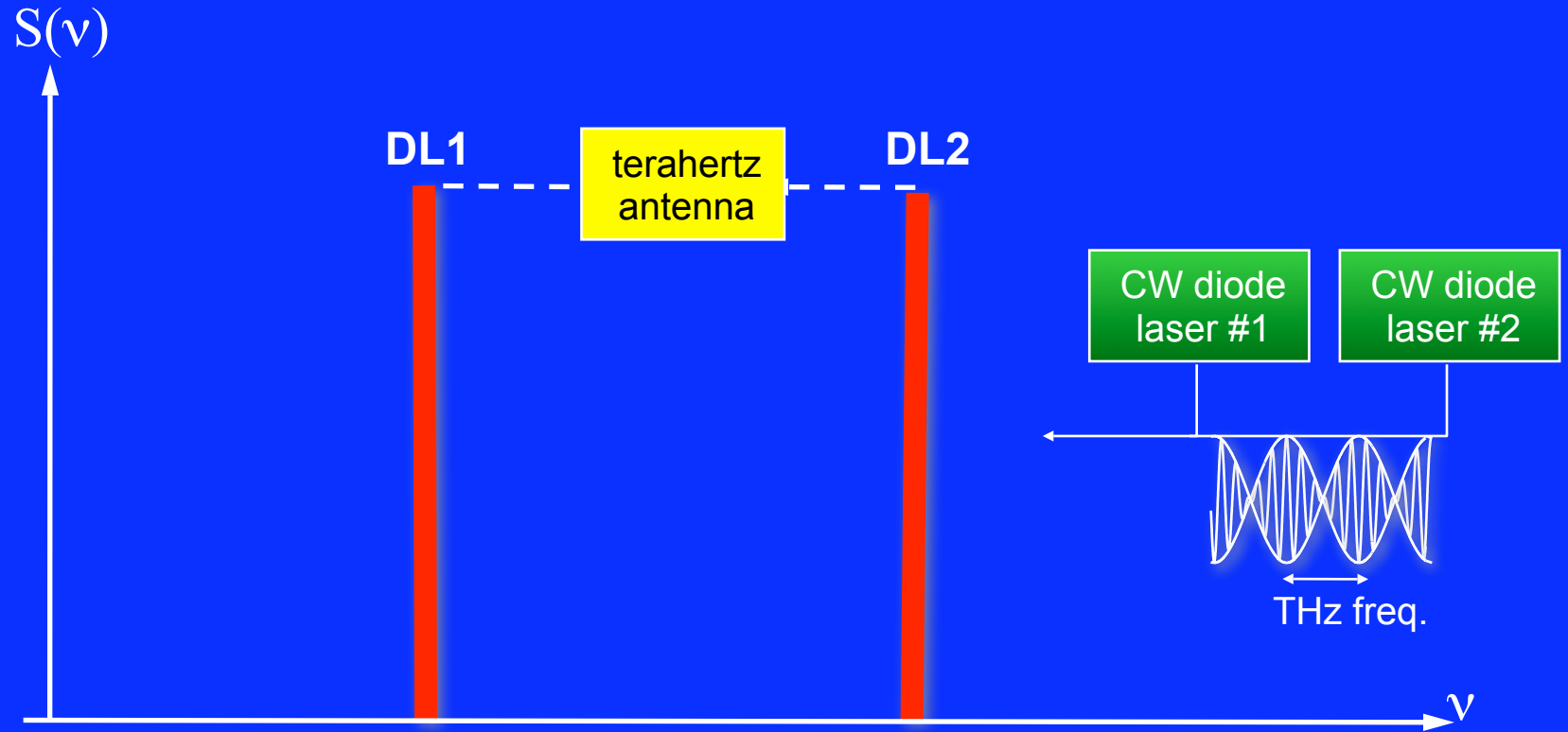
1 THz \sim 0.3 μm

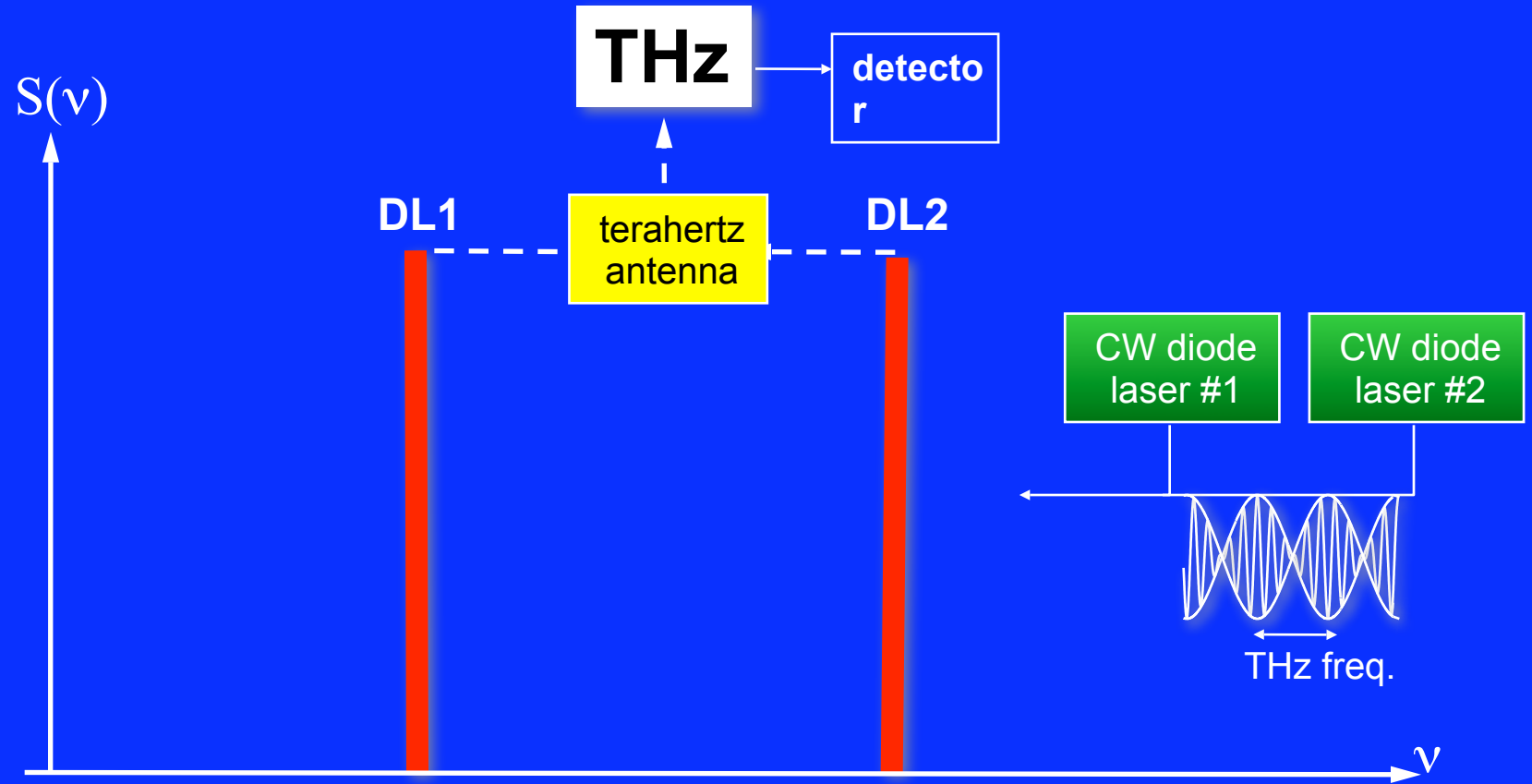
R. Köhler, A. Tredicucci, F. Beltram,
et al., Nature 417, 156 (2002).



B. Ferguson and X. Zhang Nature Mat. 1, 26 (2002)

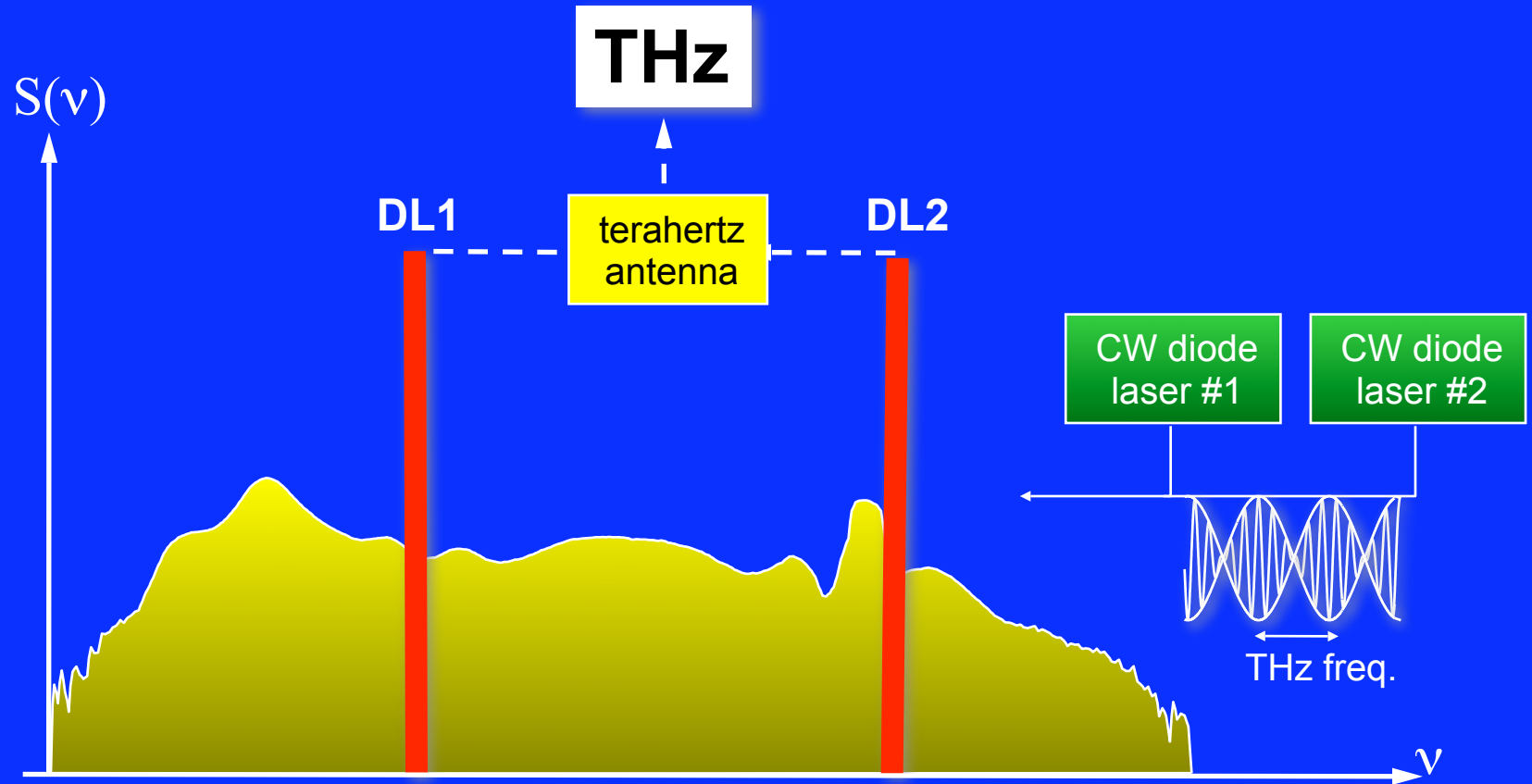
combine powerful ideas of
stabilized optical frequency combs
with THz domain





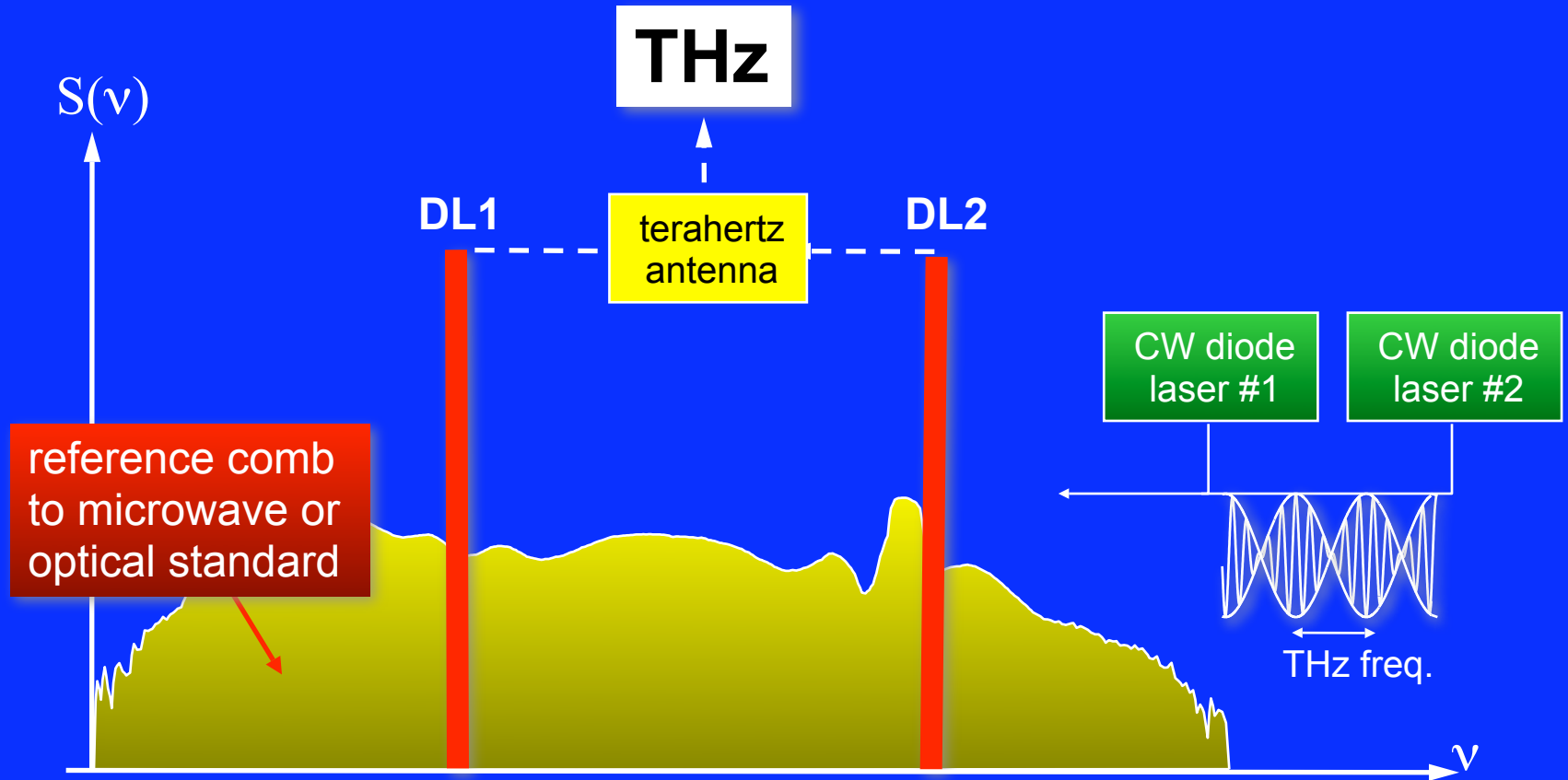
comb allows us to:

- § broad tune THz
- § know THz freq. precisely while tuning



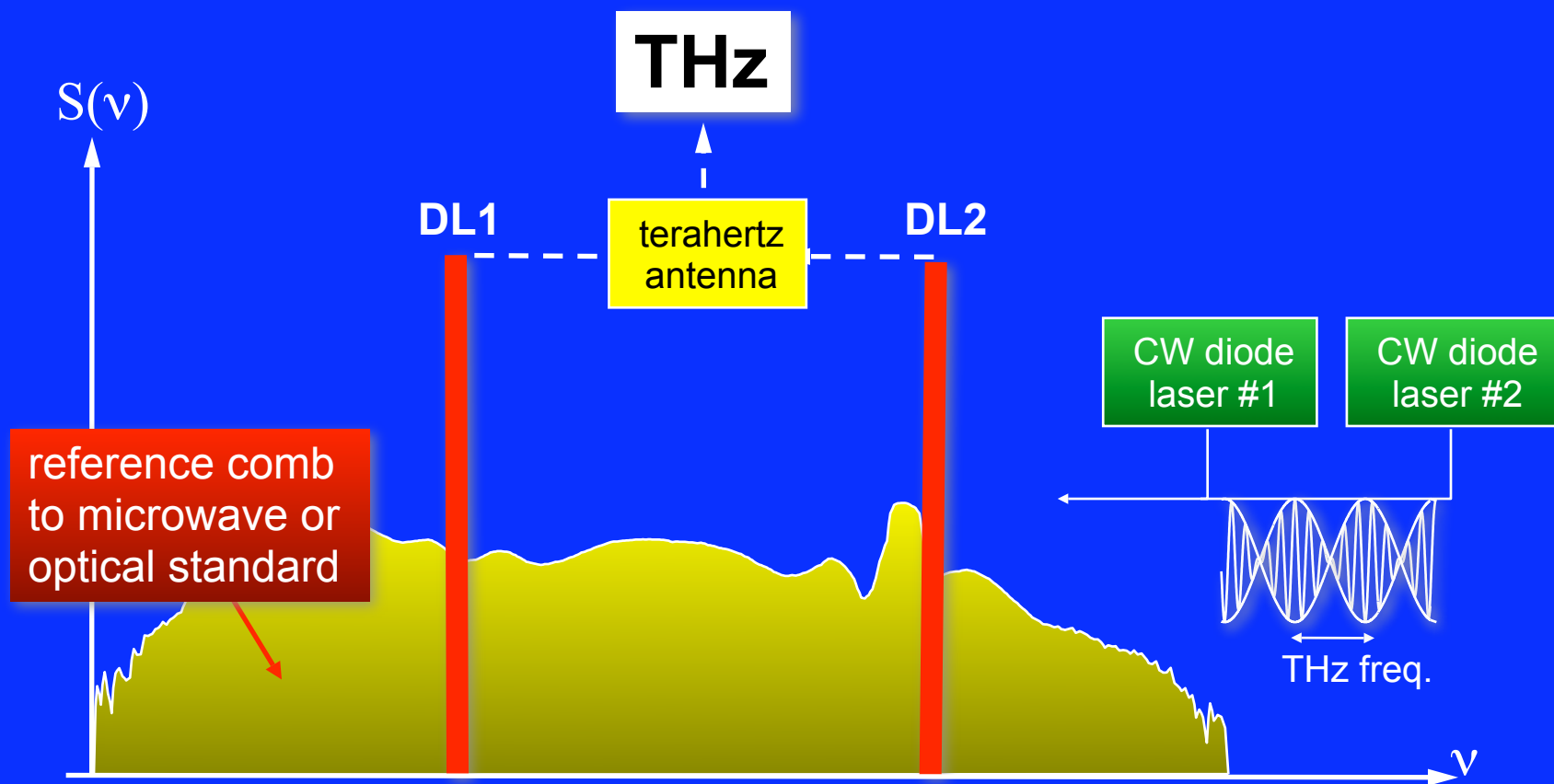
comb allows us to:

- § broad tune THz
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comb allows us to:

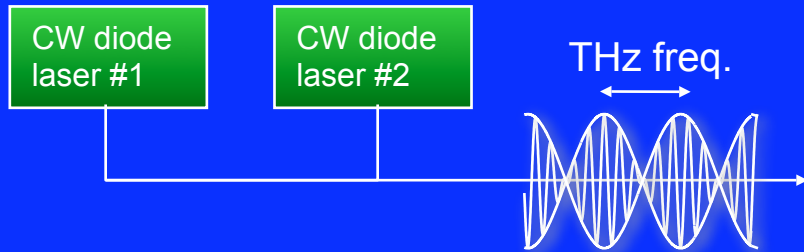
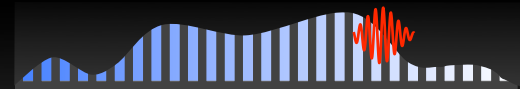
- § broad tune THz
- § know THz freq. precisely while tuning



potential applications:

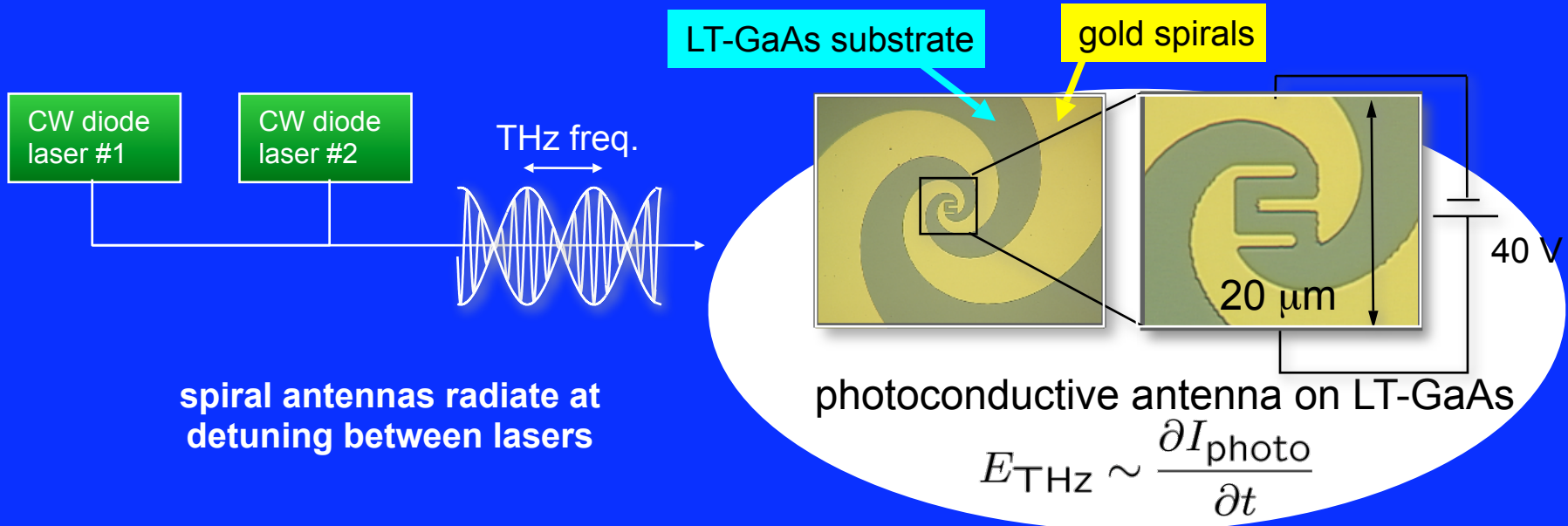
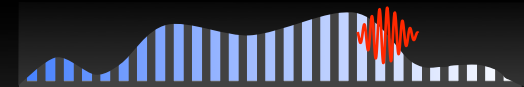
- § THz frequency standards
- § precision molecular spectroscopy
- § commercial applications in defense and space industries
- § studies of semiconductor dynamics

CW THz source: heterodyne photomixer



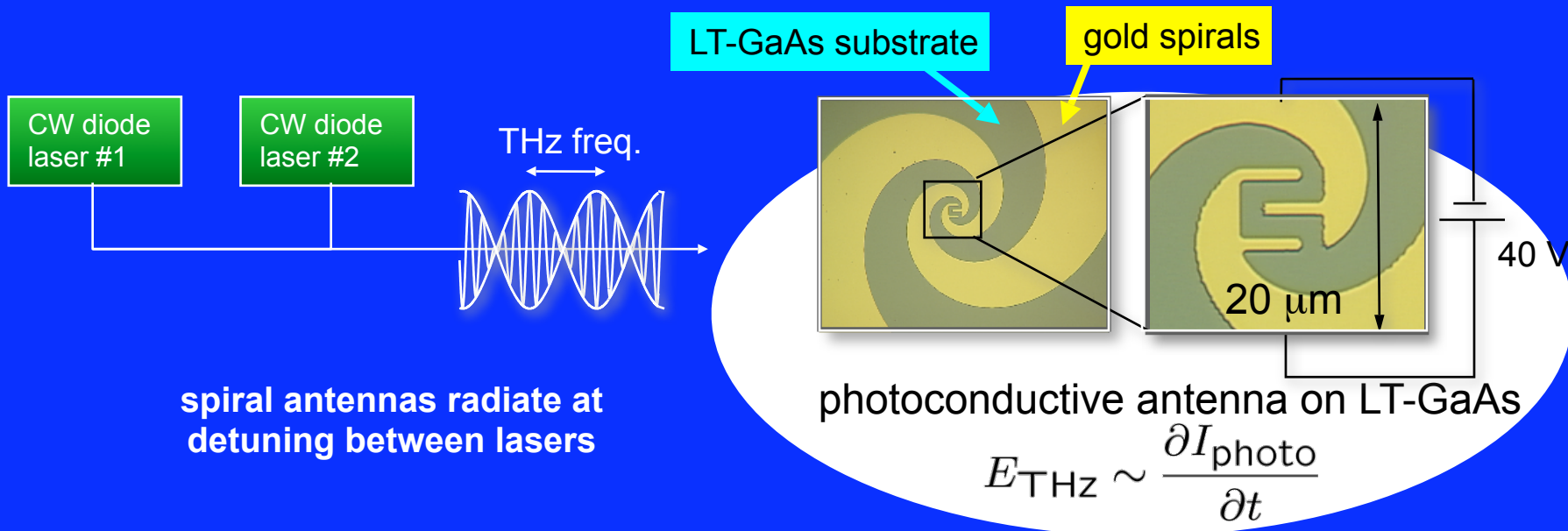
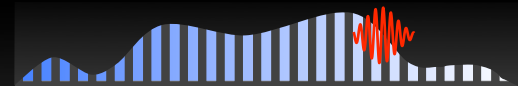
**spiral antennas radiate at
detuning between lasers**

CW THz source: heterodyne photomixer

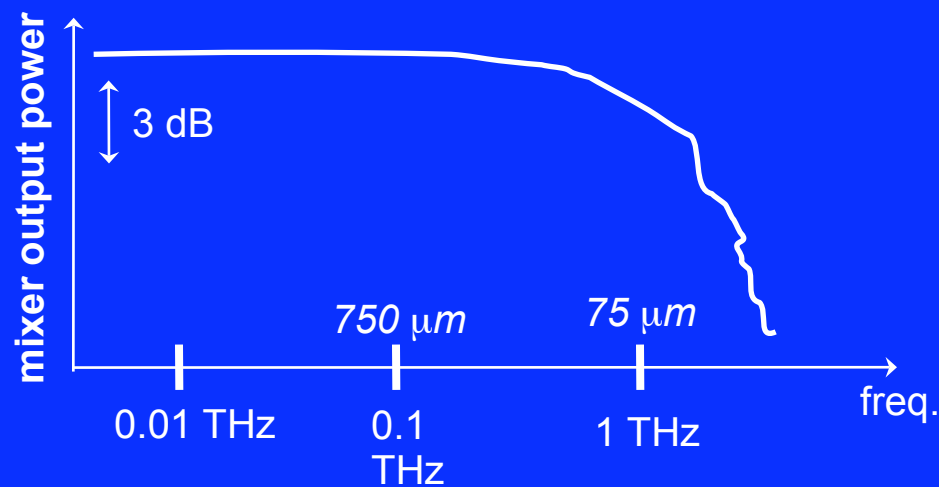


Vershese et al. IEEE Trans. on Micro. Theory and Tech. **45** 1307 (1997).
Smith et al. IEEE J. of Quantum Electron. **24** 255 (1988).

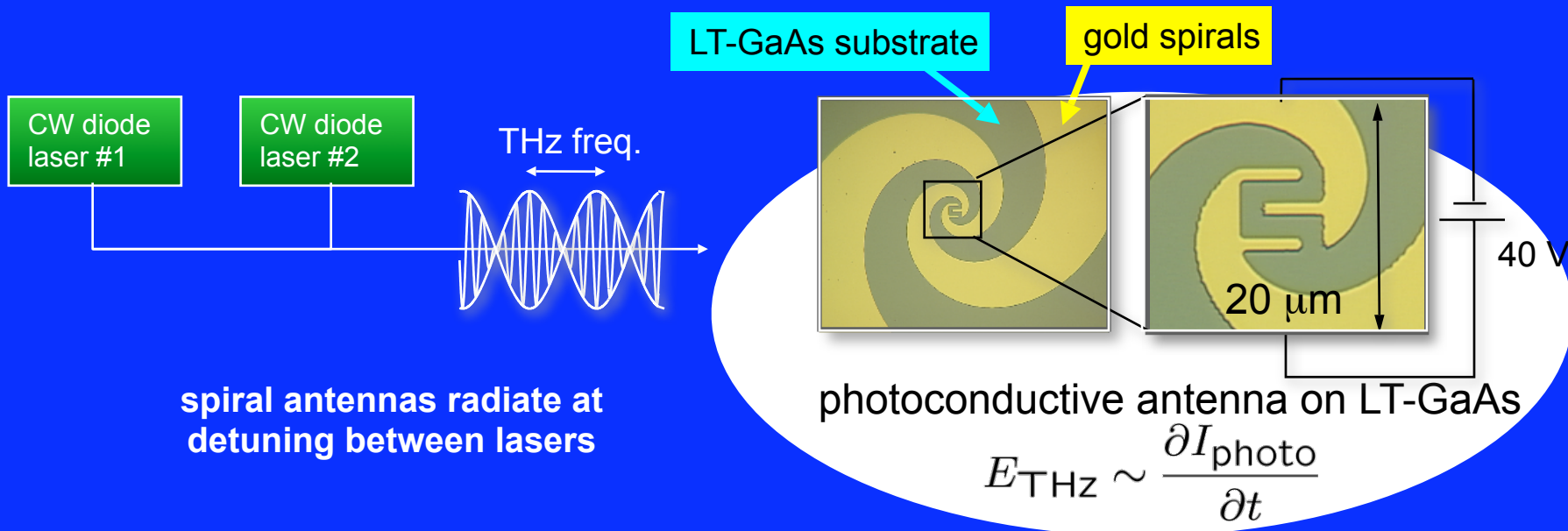
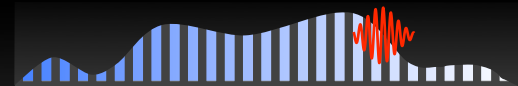
CW THz source: heterodyne photomixer



Vershesh et al. IEEE Trans. on Micro. Theory and Tech. **45** 1307 (1997).
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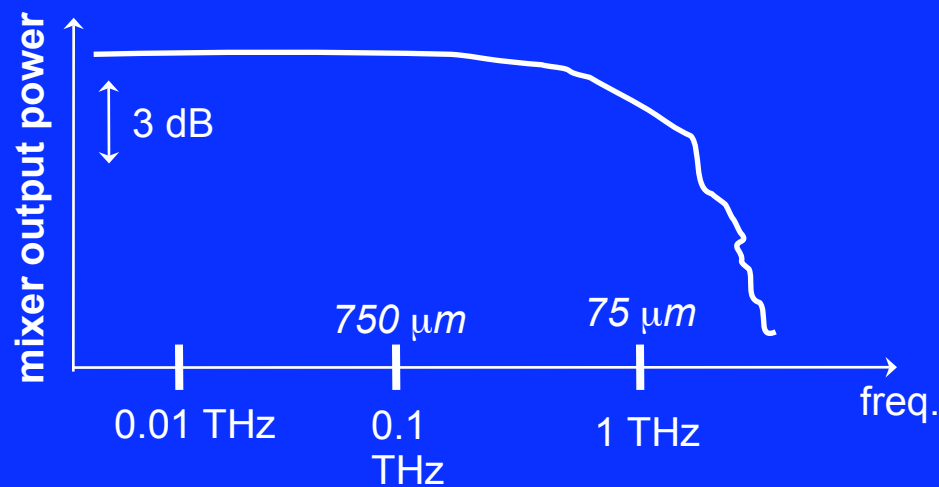
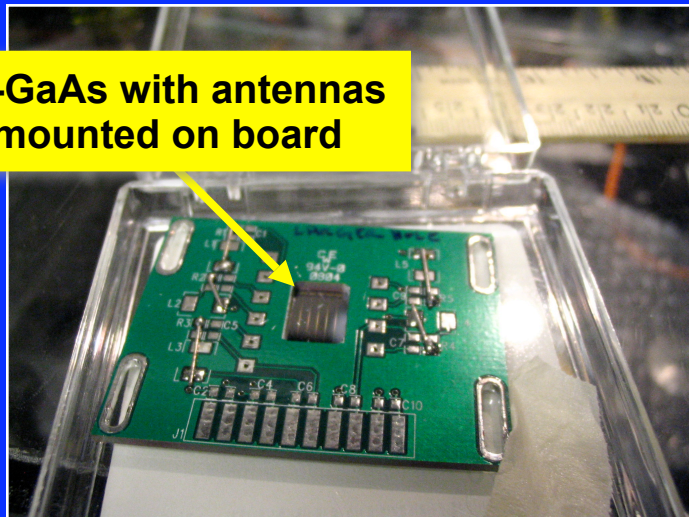


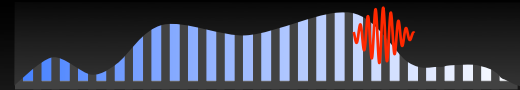
CW THz source: heterodyne photomixer



Vershese et al. IEEE Trans. on Micro. Theory and Tech. **45** 1307 (1997).
Smith et al. IEEE J. of Quantum Electron. **24** 255 (1988).

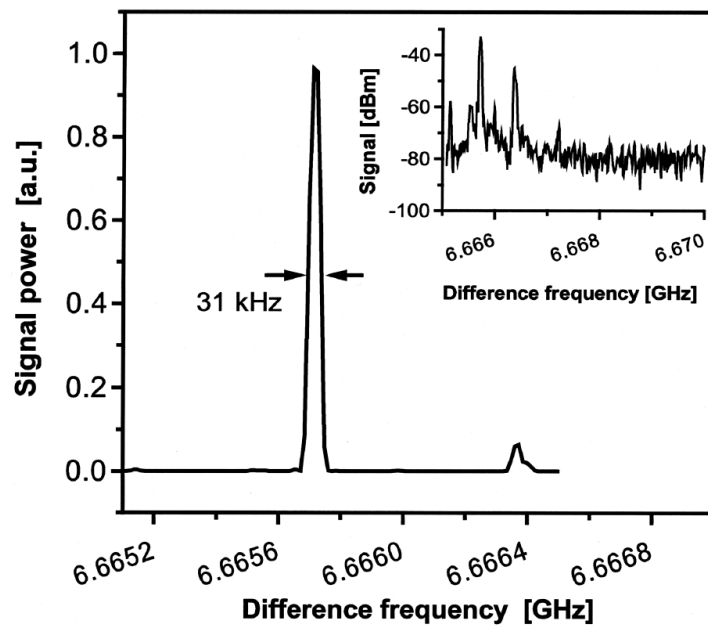
LT-GaAs with antennas mounted on board





quantum cascade laser

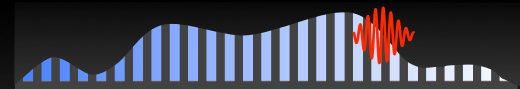
- § tunability: 10 GHz
- § cryogenic temperatures
- § linewidth ~ 30 kHz



A. Barkan *et al.*, Opt. Lett. **29** 575 (2004).

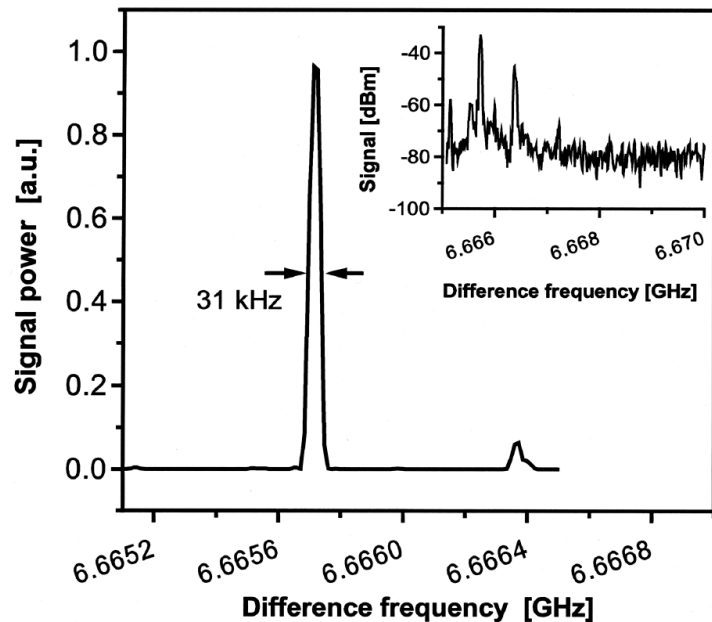
quantum
cascade laser

linewidth comparison of our results to others



quantum cascade laser

- § tunability: 10 GHz
- § cryogenic temperatures
- § linewidth ~30 kHz

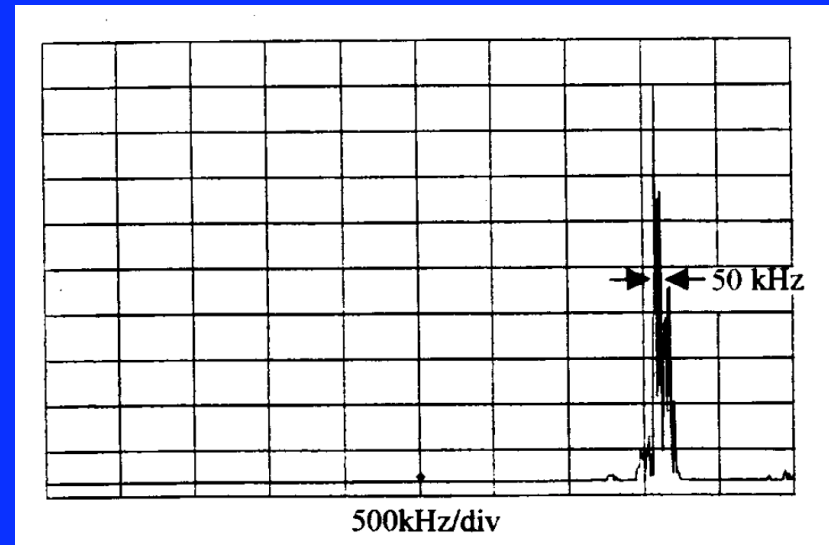


A. Barkan *et al.*, Opt. Lett. **29** 575 (2004).

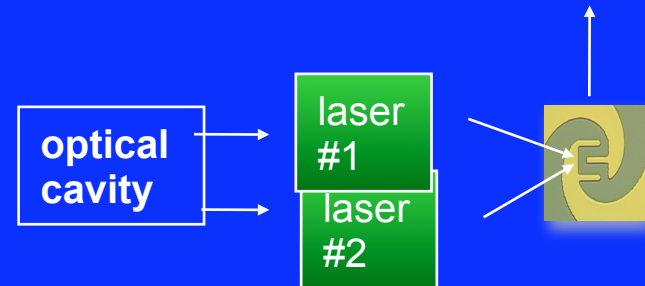


two CW lasers referenced to optical cavity

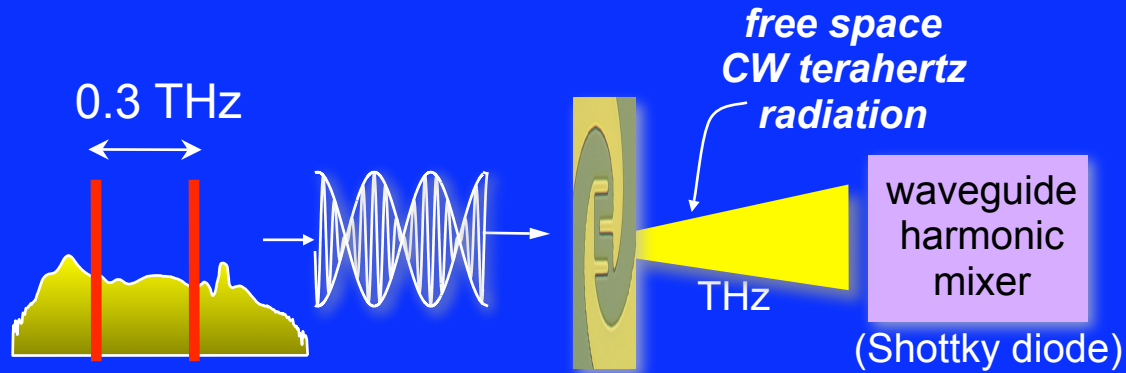
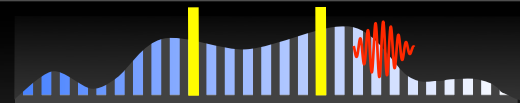
- § tunability: THz
- § more work required to know THz frequency
- § locked linewidth ~50 kHz, but can be made narrower



P. Chen *et al.*, App. Phys. Lett. **71** 1601 (1997).

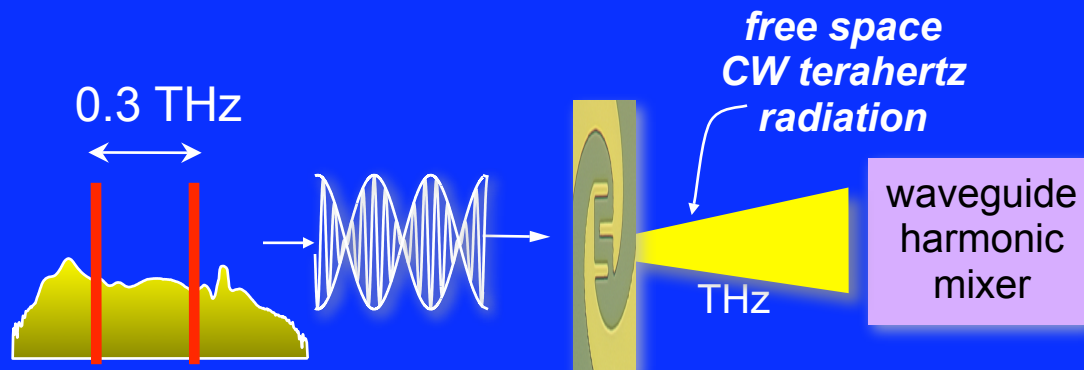
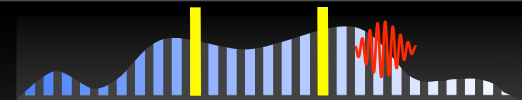


THz freq. down-conversion: waveguide harmonic mixer



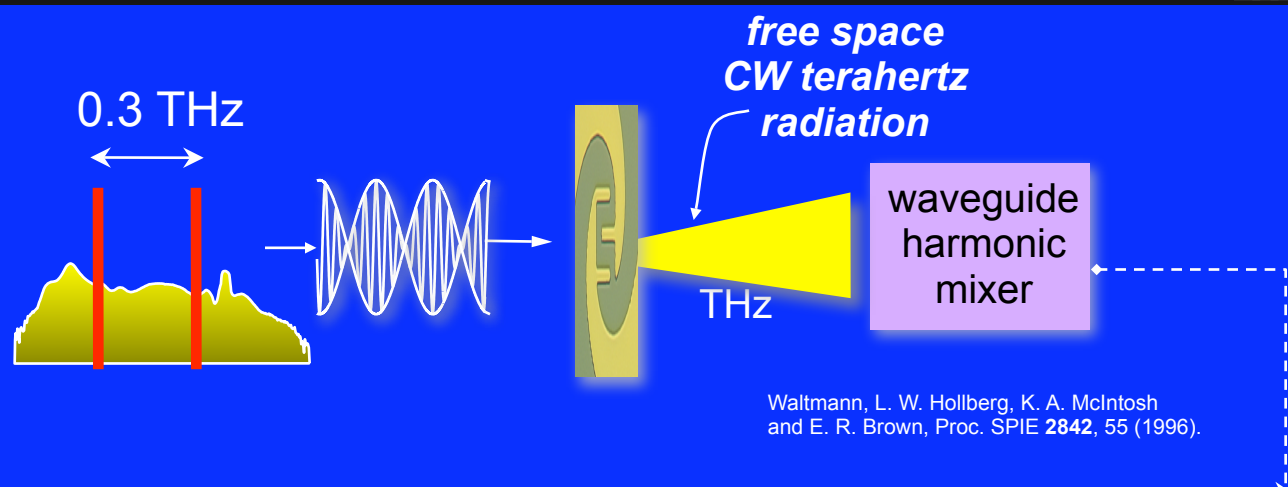
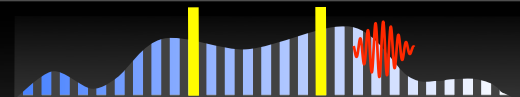
Waltmann, L. W. Hollberg, K. A. McIntosh
and E. R. Brown, Proc. SPIE **2842**, 55 (1996).

THz freq. down-conversion: waveguide harmonic mixer

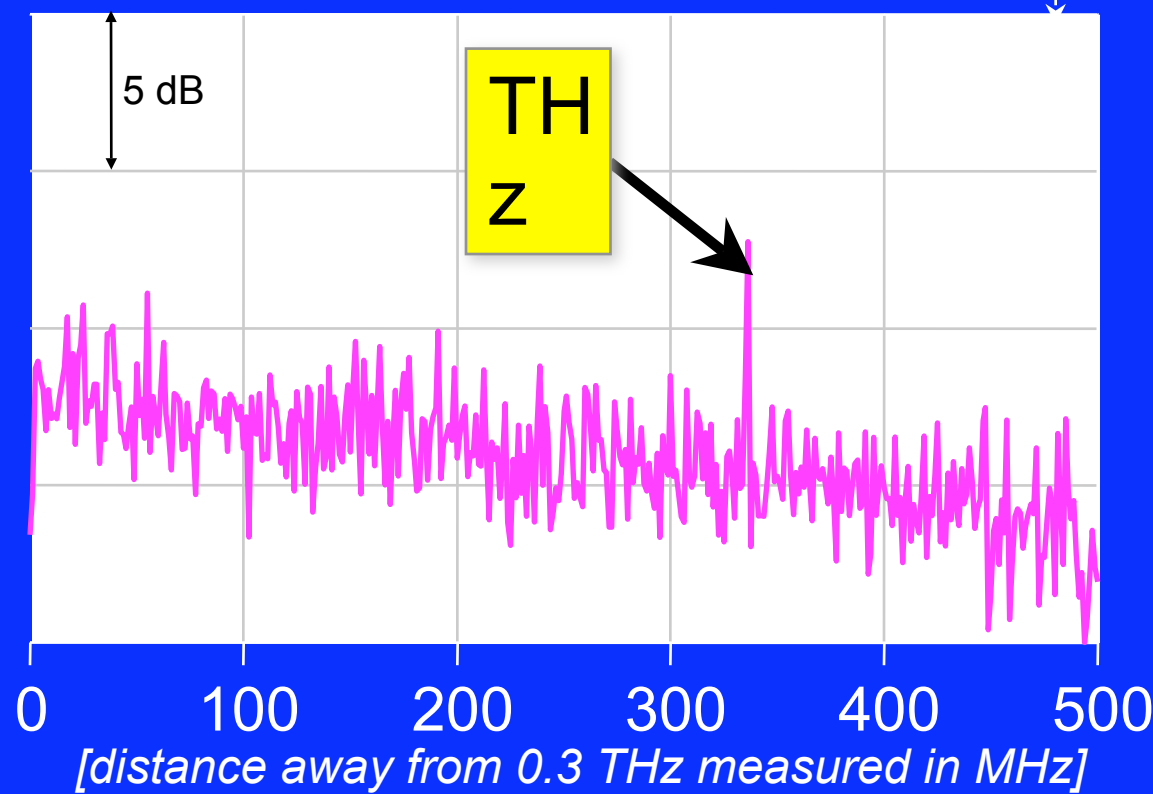


Waltmann, L. W. Hollberg, K. A. McIntosh
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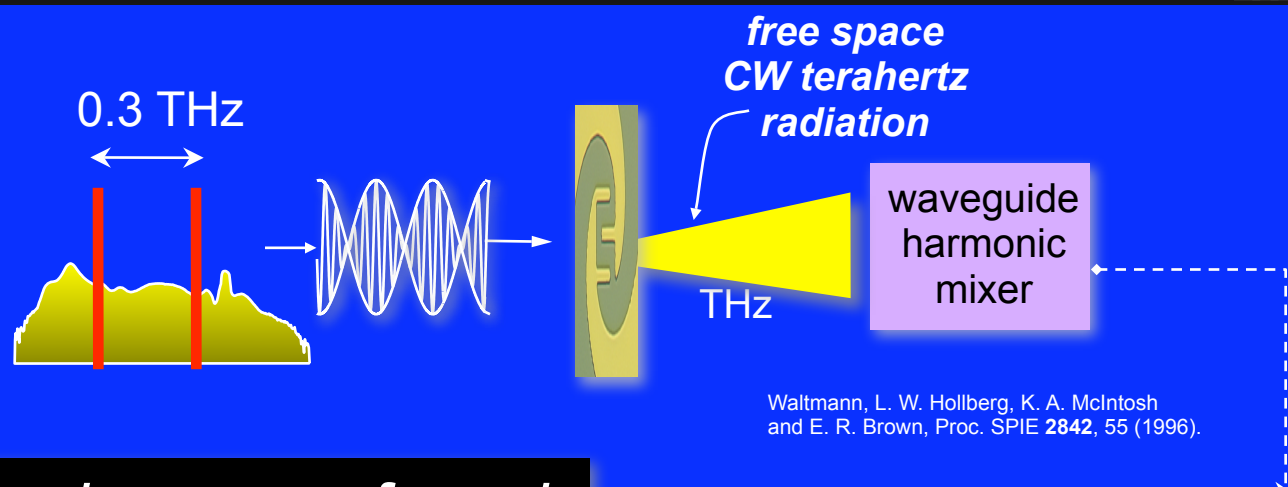
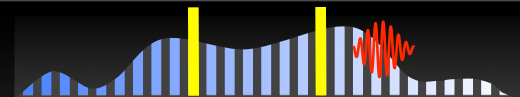
THz freq. down-conversion: waveguide harmonic mixer



Waltmann, L. W. Hollberg, K. A. McIntosh and E. R. Brown, Proc. SPIE **2842**, 55 (1996).

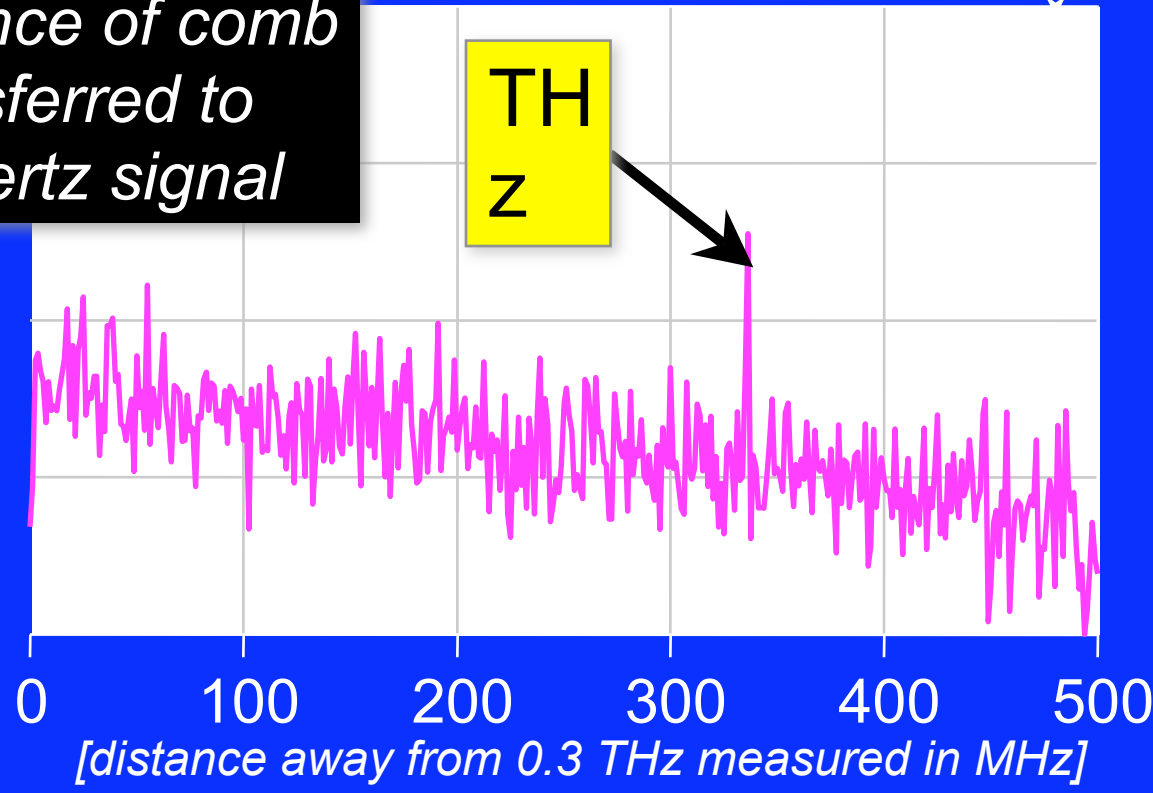


THz freq. down-conversion: waveguide harmonic mixer

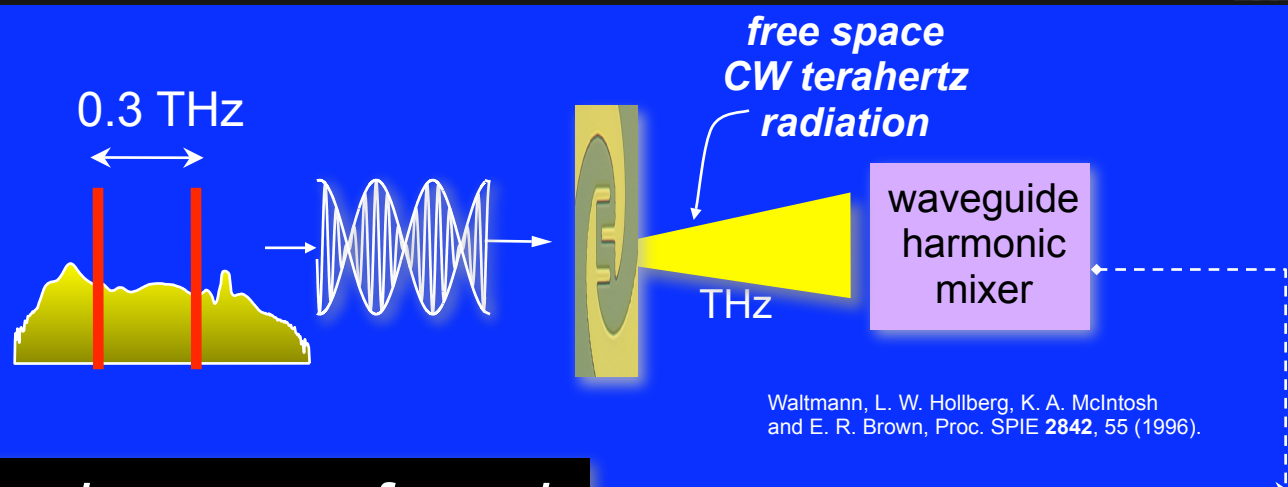
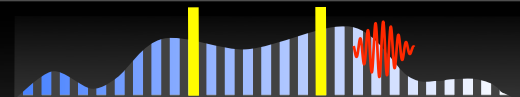


Waltmann, L. W. Hollberg, K. A. McIntosh and E. R. Brown, Proc. SPIE 2842, 55 (1996).

coherence of comb transferred to terahertz signal

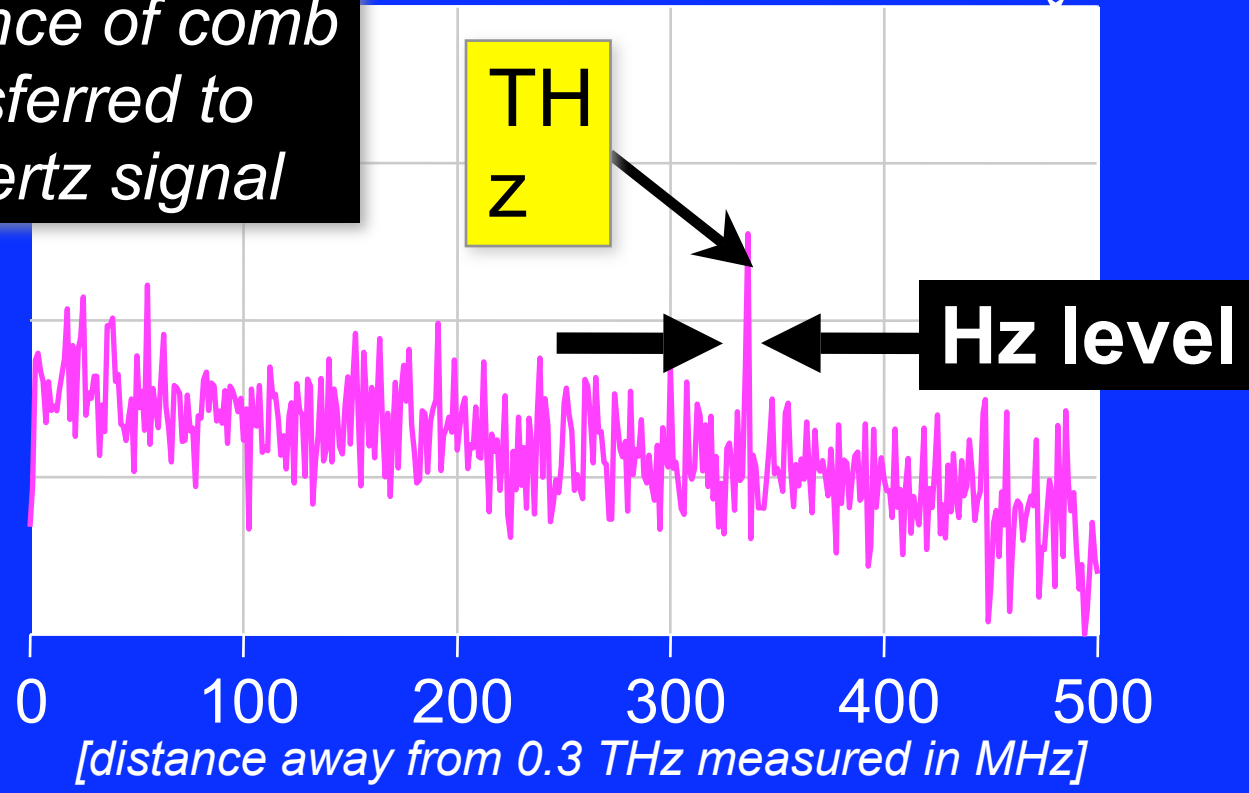


THz freq. down-conversion: waveguide harmonic mixer

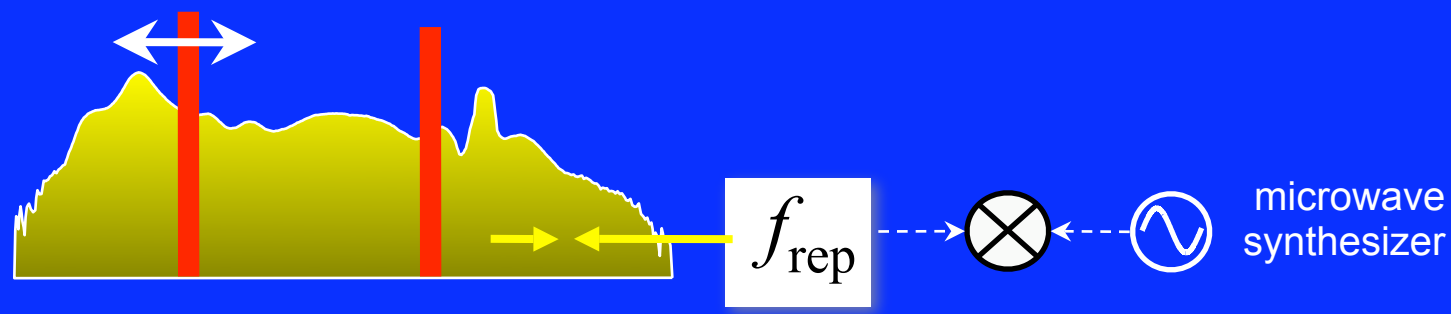
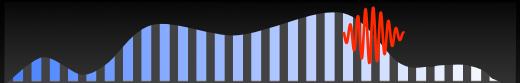


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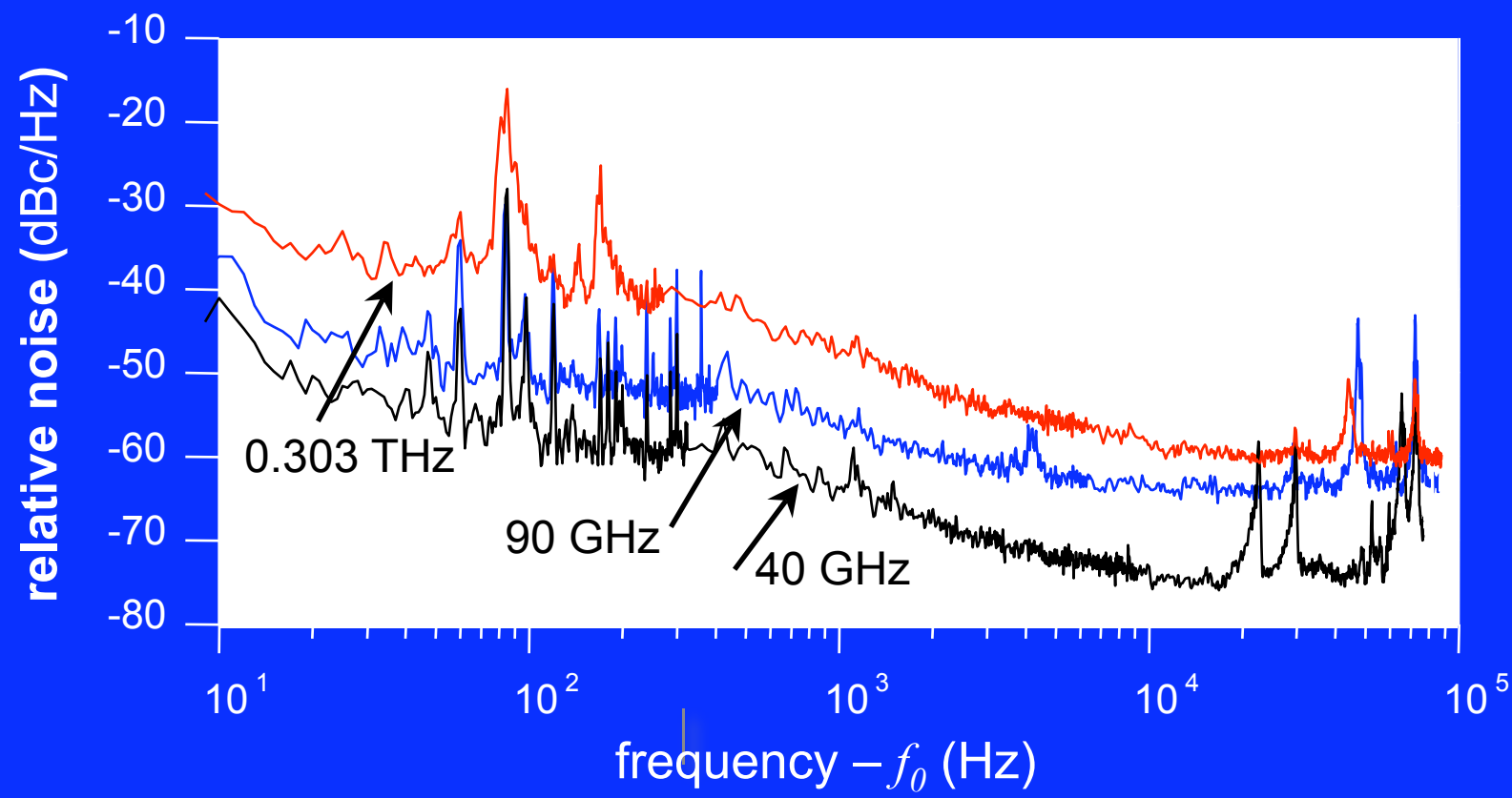
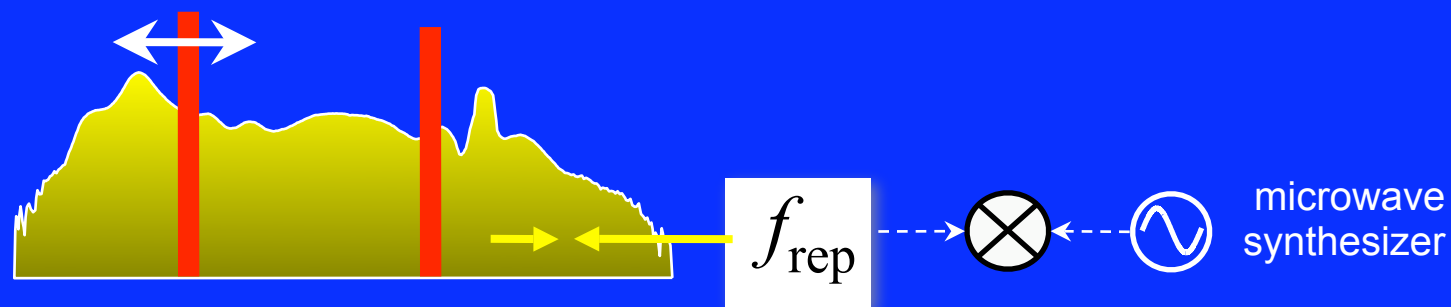
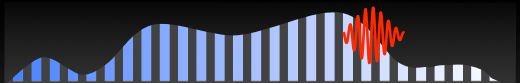
coherence of comb transferred to terahertz signal



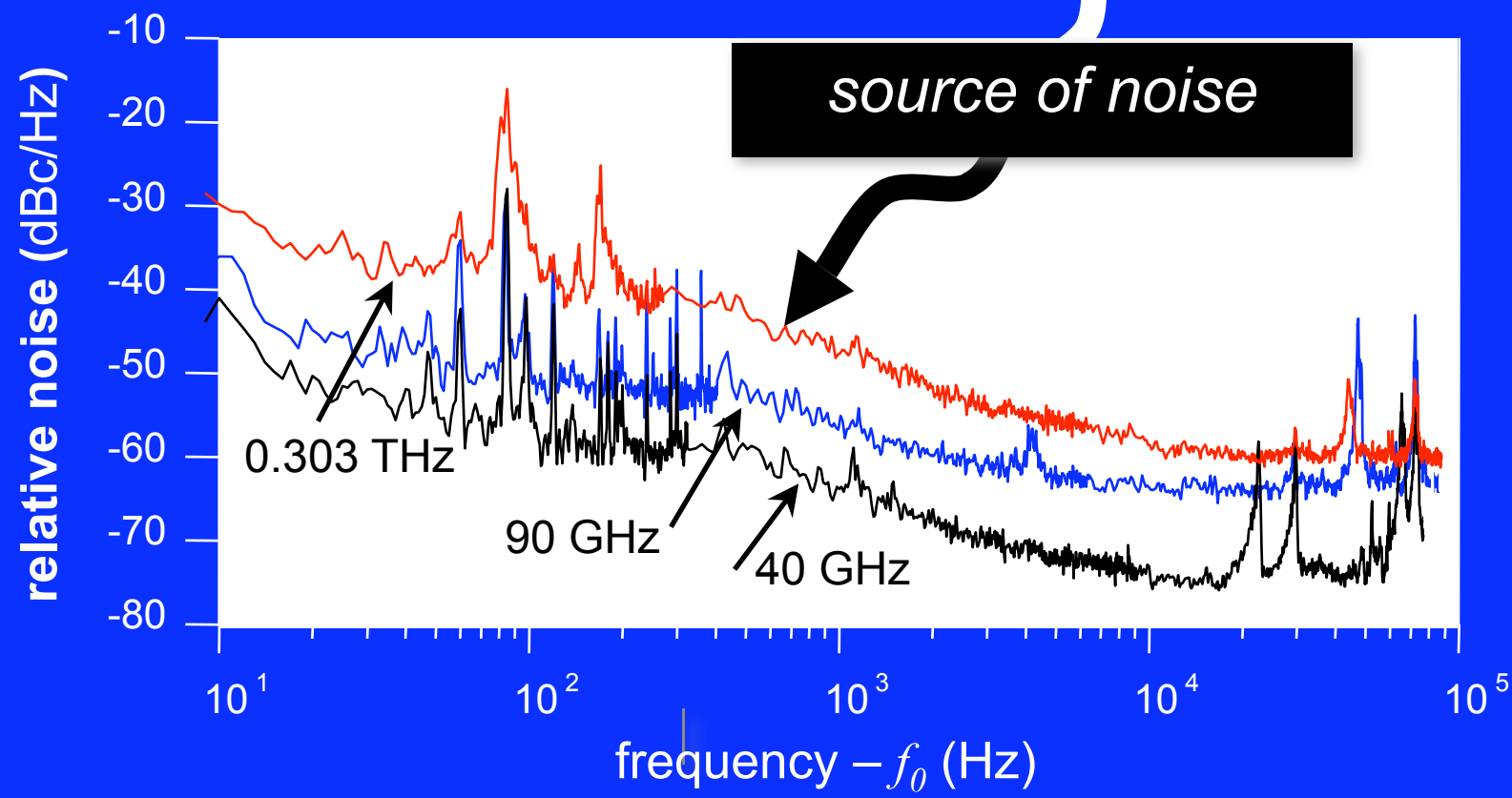
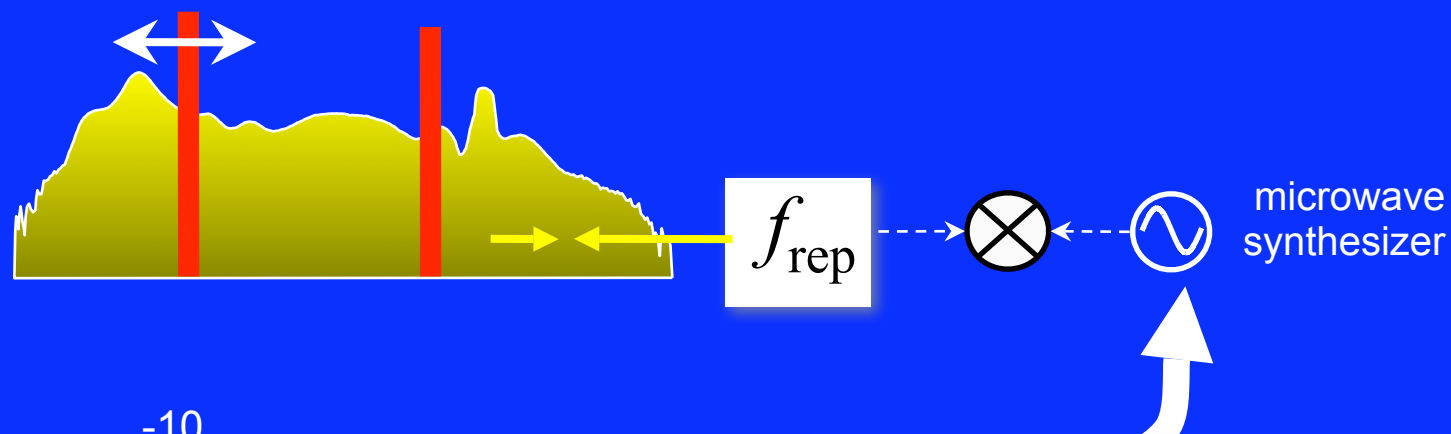
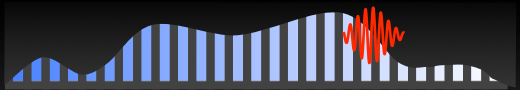
coherence of comb transferred to terahertz

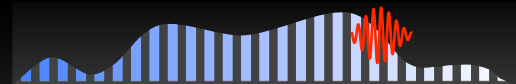


coherence of comb transferred to terahertz



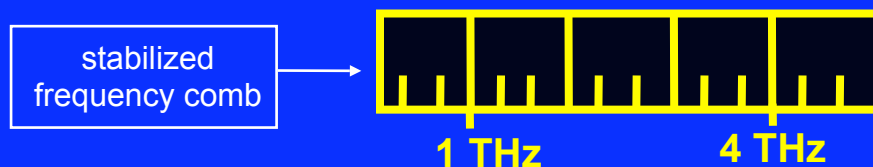
coherence of comb transferred to terahertz





- (a) demonstrated that stabilized optical frequency combs may be successfully integrated into THz spectrometers.

resulting in: excellent linewidth and broad tunability



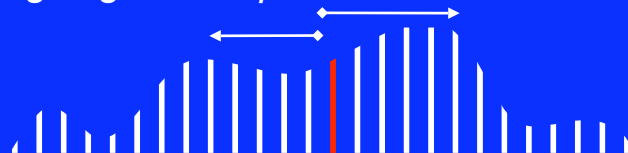
- (b) demonstrated improved optical phase noise performance of TiS

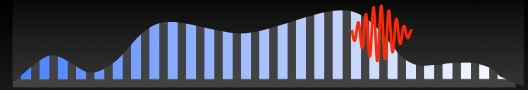
resulting in: potential for enhance microwave phase noise performance

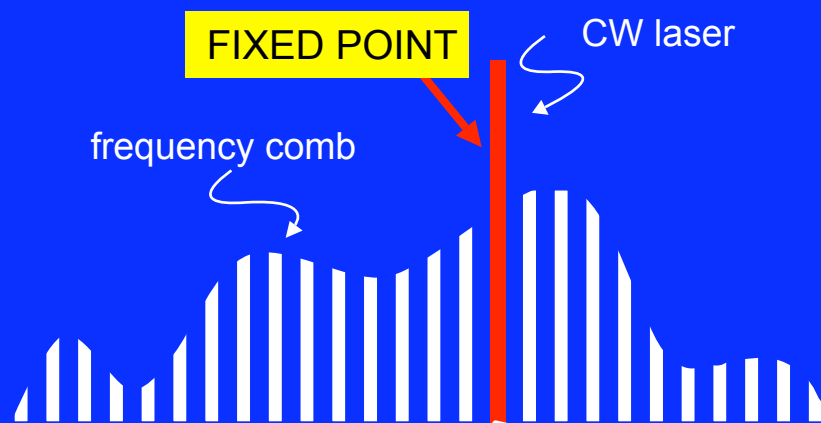
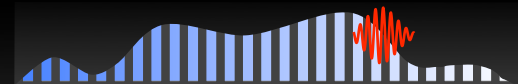


- (c) showed optical coherence properties of comb

demonstrating: significant phase coherence across 100s of nm across





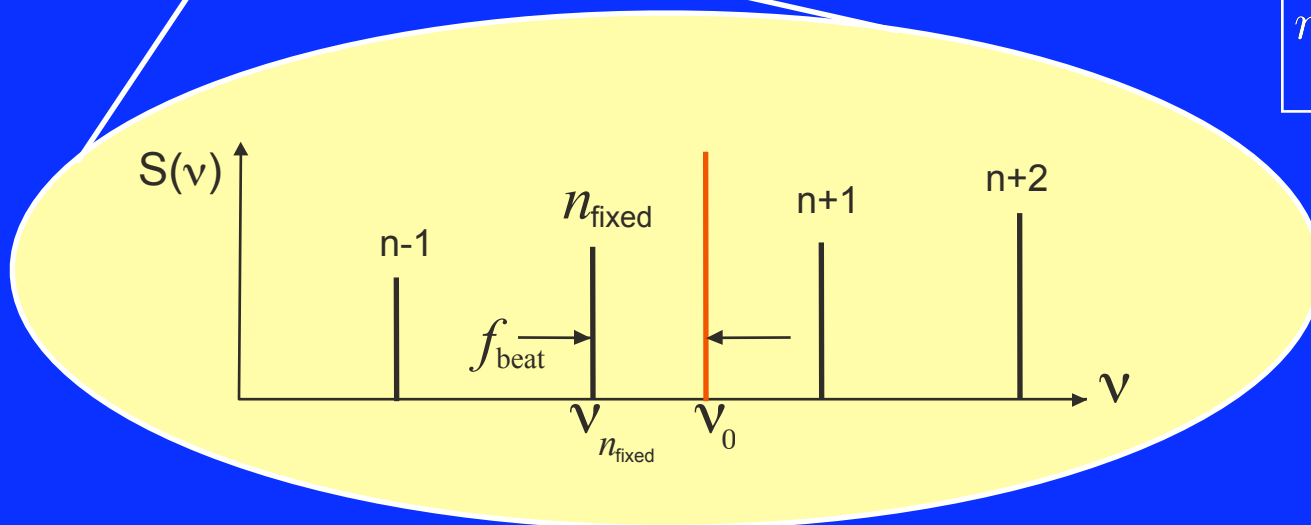


$$f_{\text{rep}} = \frac{\nu_0 + f_{\text{beat}} - f_0}{n_{\text{fixed}}}$$

OFC modes redefined in terms of fixed point

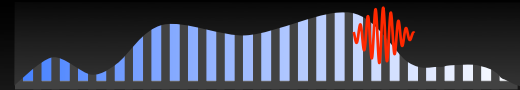
$$\begin{aligned} \nu_n &= n f_{\text{rep}} + f_0 \\ &= n \frac{\nu_0 + f_{\text{beat}} - f_0}{n_{\text{fixed}}} + f_0 \\ &= r(\nu_0 + f_{\text{beat}}) + (1 - r)f_0 \end{aligned}$$

$$r = \frac{n}{n_{\text{fixed}}}$$

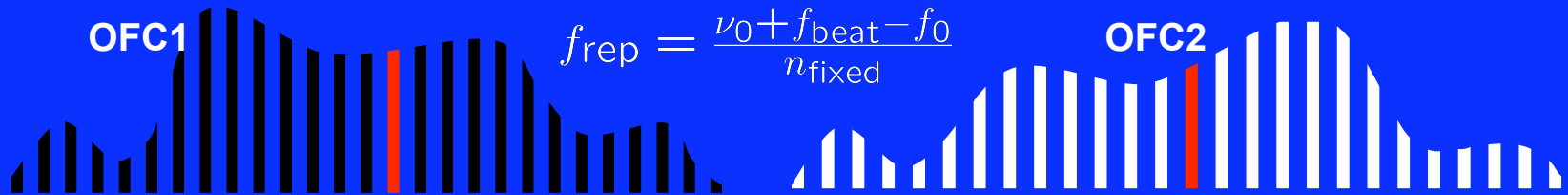


§ f_0 independently stabilized

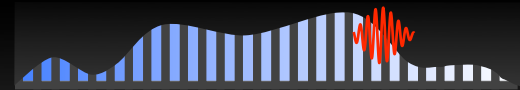
deriving prediction for phase noise across comb



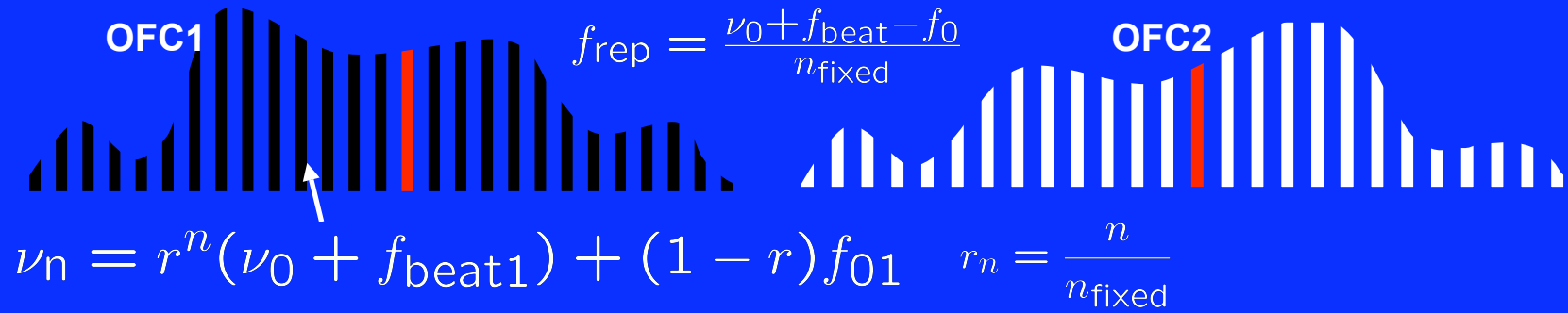
§ rewrite comb equation in terms of phase-locked parameters



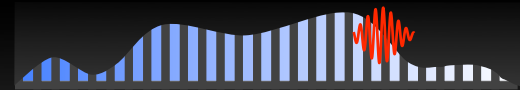
deriving prediction for phase noise across comb



§ rewrite comb equation in terms of phase-locked parameters



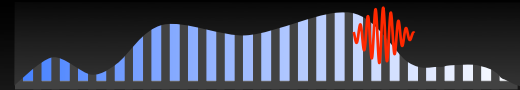
deriving prediction for phase noise across comb



§ rewrite comb equation in terms of phase-locked parameters



deriving prediction for phase noise across comb



§ rewrite comb equation in terms of phase-locked parameters



§ relative noise between these two, using ν_n equation is:

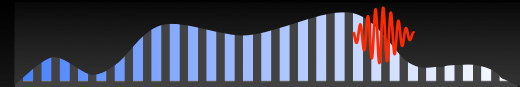
projected phase noise

$$S_{\Phi, m, n}(f) = (r^m - r^n)^2 \sum_i S_{\phi, i}(f) \frac{\text{rad}^2}{\text{Hz}}$$

phase noise of each locked parameter

(we neglect cross terms)

deriving prediction for phase noise across comb



§ rewrite comb equation in terms of phase-locked parameters

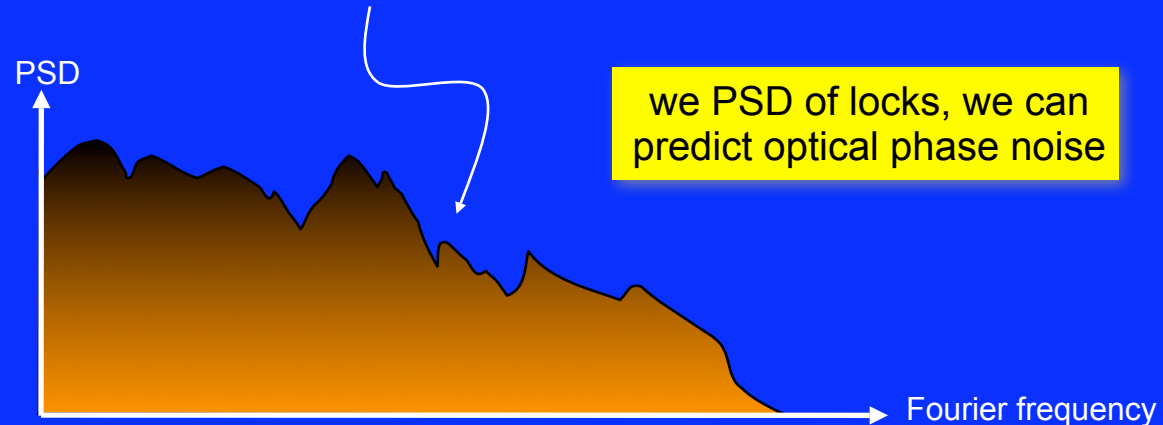


§ relative noise between these two, using ν_n equation is:

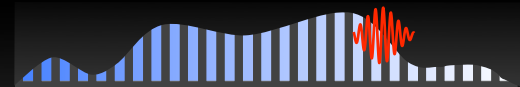
projected phase noise

$$S_{\Phi, m, n}(f) = (r^m - r^n)^2 \sum_i S_{\phi, i}(f) \frac{\text{rad}^2}{\text{Hz}} \quad (\text{we neglect cross terms})$$

phase noise of each locked parameter



deriving prediction for phase noise across comb



§ rewrite comb equation in terms of phase-locked parameters



§ relative noise between these two, using ν_n equation is:

projected phase noise

$$S_{\Phi, m, n}(f) = (r^m - r^n)^2 \sum_i S_{\phi, i}(f) \frac{\text{rad}^2}{\text{Hz}}$$

phase noise of each locked parameter

(we neglect cross terms)

