

Exchange Bias and Bi-stable Magneto-Resistance States in Amorphous TbFeCo and TbSmFeCo Thin Films

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Outline

- Background

Why are we interested in Tb(Sm)FeCo thin films and exchange bias?

- Experimental Results

Magnetic and structural properties of exchange biased Tb(Sm)FeCo

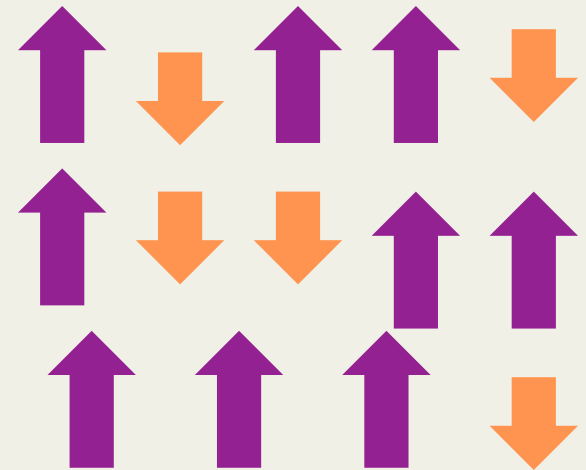
- Micromagnetic Simulations

Two-sublattice, two-phase model

Background

Amorphous TbFeCo films

- Ferrimagnetic (FiM)
- Tb and FeCo sublattices
- Compensation Temperature (T_{comp})



Background

Amorphous TbFeCo films

- Perpendicular magnetic anisotropy (PMA)
- Structural anisotropy gives rise to PMA in sputtered amorphous TbFe films

Harris, V. G., et al. Phys. Rev. Lett. **69**.13 (1992): 1939.

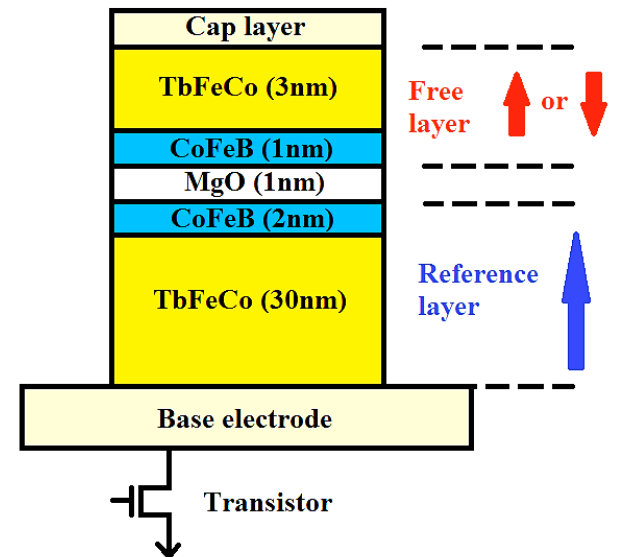
Yan, X., et al, Phys. Rev. B **43**.11 (1991): 9300

- Magnetic random access memory (MRAM)

Nakayama et al, J. Appl. Phys. **103**, 07A710 (2008).

- Ultrafast switching (picoseconds)

Hassdenteufel et al, Adv. Mater. **25**, 3122 (2013)



Background

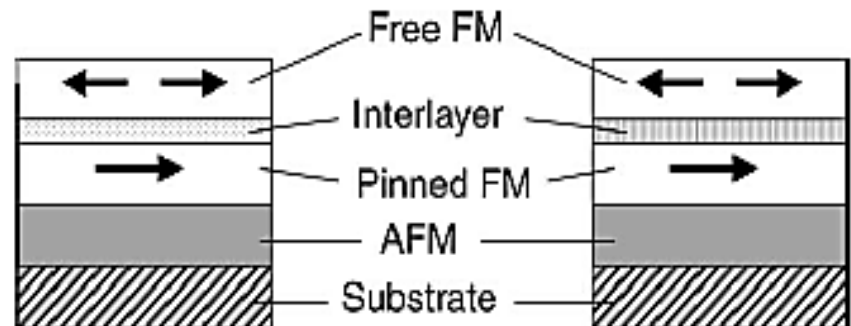
Exchange bias

- Ferromagnetic(FM)/Antiferromagnetic(AFM) bilayer act as a pinned layer in spintronics devices

Nogués et al. / Phys. Rep. **422** (2005) 65 –117

- Stabilize the magnetization in FM layer

Liu et al. Appl. Phys. Lett. **81**, 4434 (2002)



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- Micromagnetic Simulations

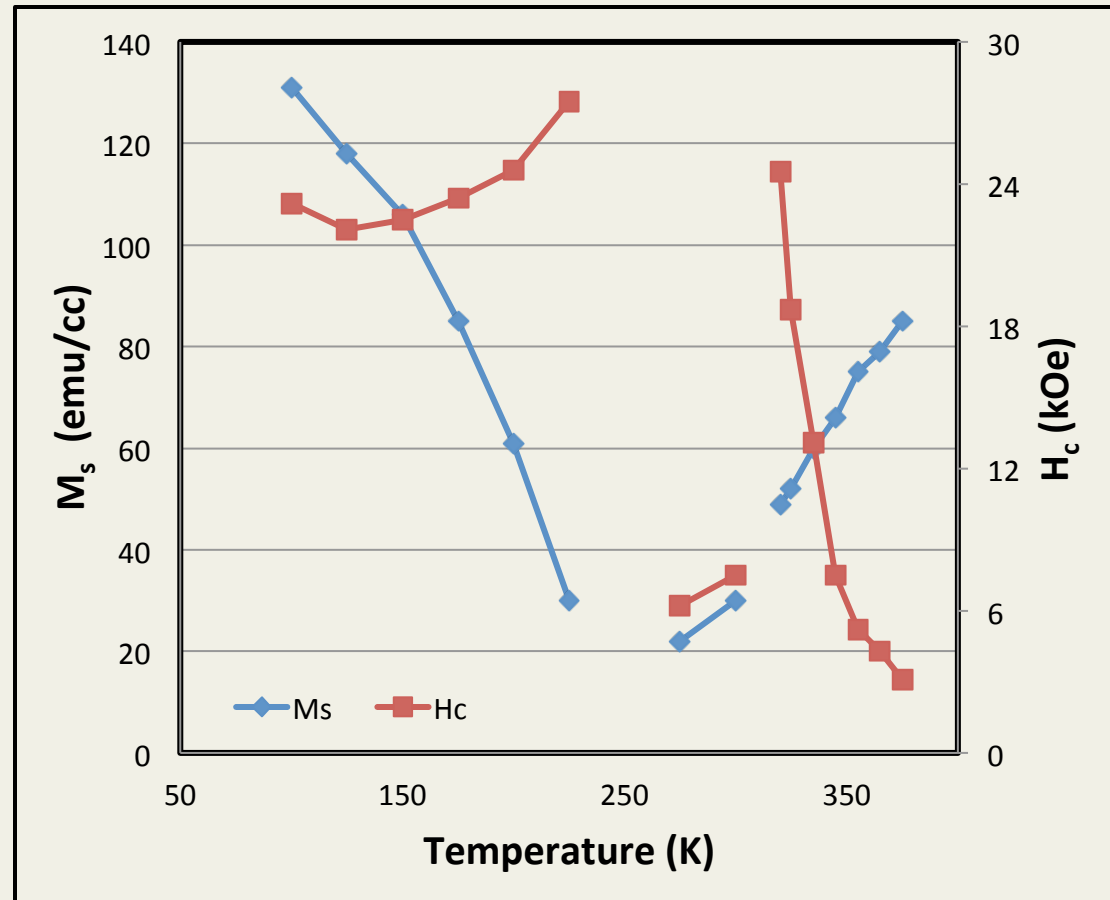
Interpenetrating two-phase, two-sublattice model

Experiment Methods

- Si/SiO₂ substrates
- Radio frequency (RF) magnetron sputtering at room temperature
- Magnetic Properties: Quantum Design Versa Lab system
- Thickness: Rigaku SmartLab system

Properties of Amorphous Tb₂₆Fe₆₄Co₁₀ Films

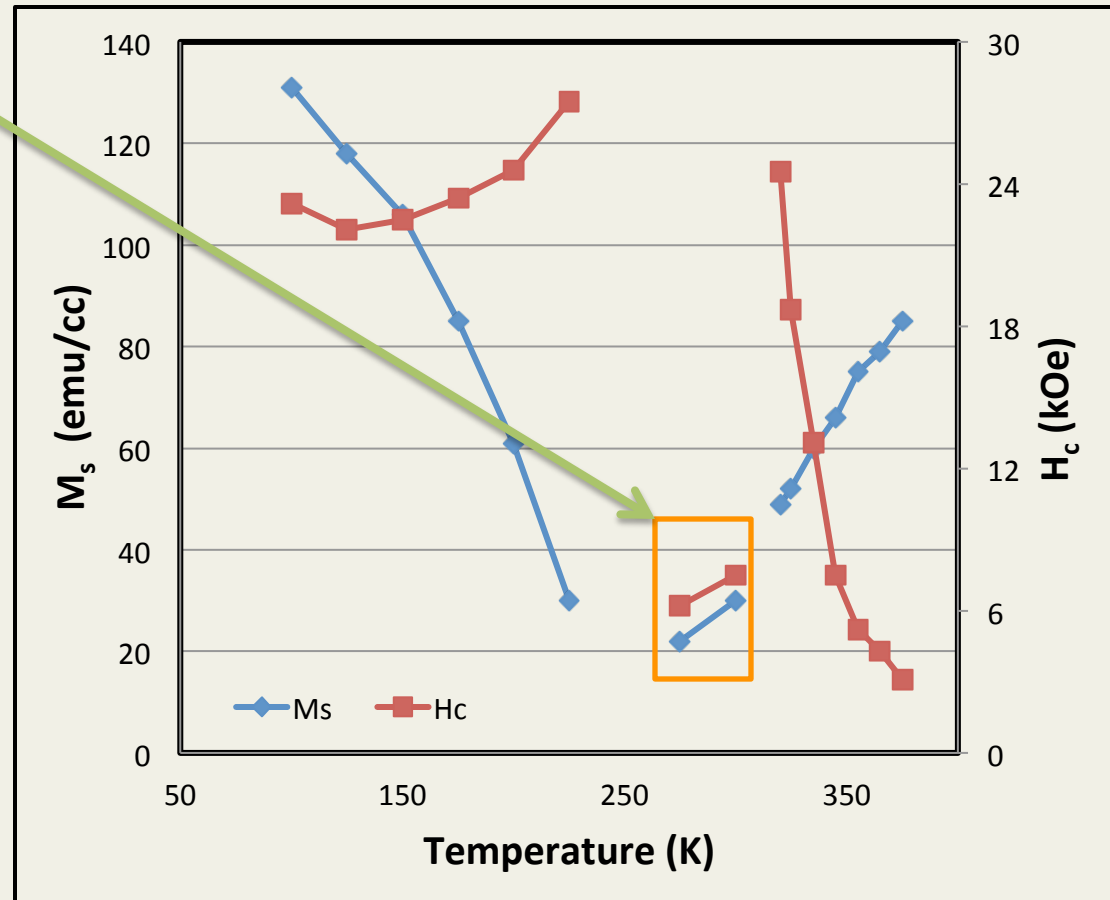
- 100 nm thick
- T_{comp} ~ 250K.
- PMA



Li et al, Appl. Phys. Lett. **108**, 012401 (2016)

Exchange Bias in Amorphous $\text{Tb}_{26}\text{Fe}_{64}\text{Co}_{10}$ Films

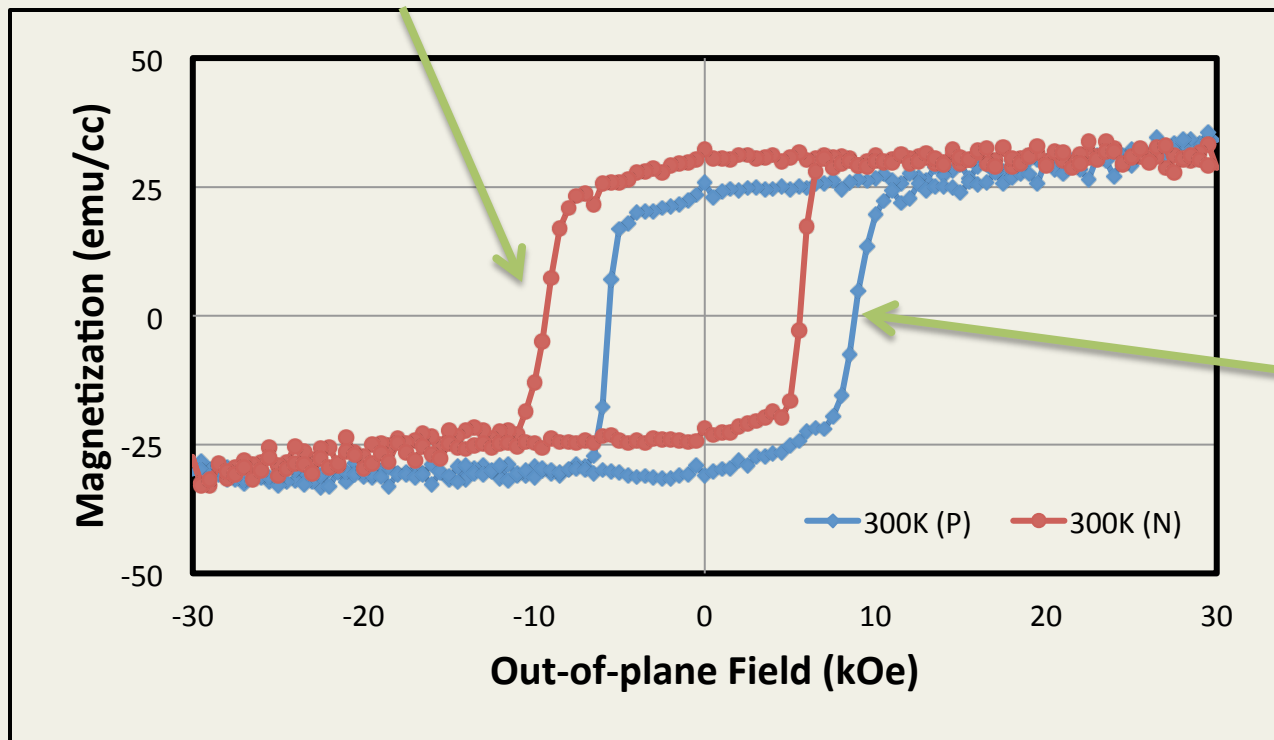
- Exchange bias effect is observed near T_{comp}



Exchange Bias in Amorphous $\text{Tb}_{26}\text{Fe}_{64}\text{Co}_{10}$ Films

- At 300K, both positive (P) and negative (N) exchange bias minor loops are observed, with different initialization procedures

(N) Initialized at 355K and 30kOe

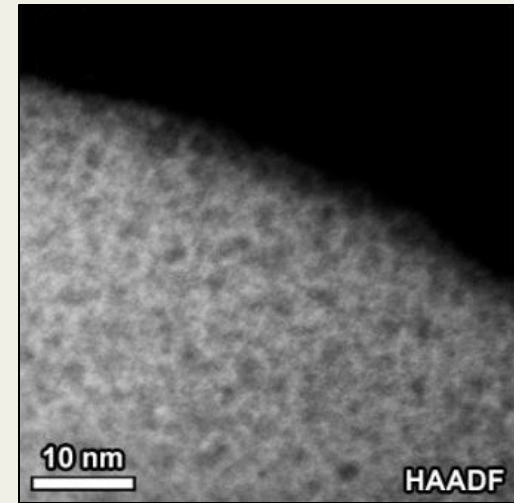


(P) Initialized at 175K and 30kOe

Origin of Exchange Bias in Tb₂₆Fe₆₄Co₁₀ Films

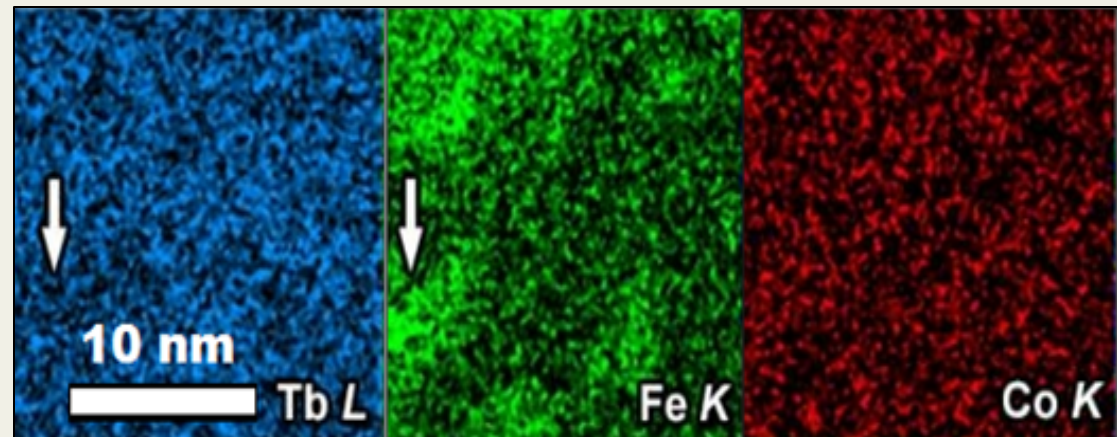
High-angle annular dark field imaging (STEM-HAADF)

- Non-uniform contrast indicates local compositional fluctuations



Energy-dispersive X-ray spectroscopy (STEM-EDS)

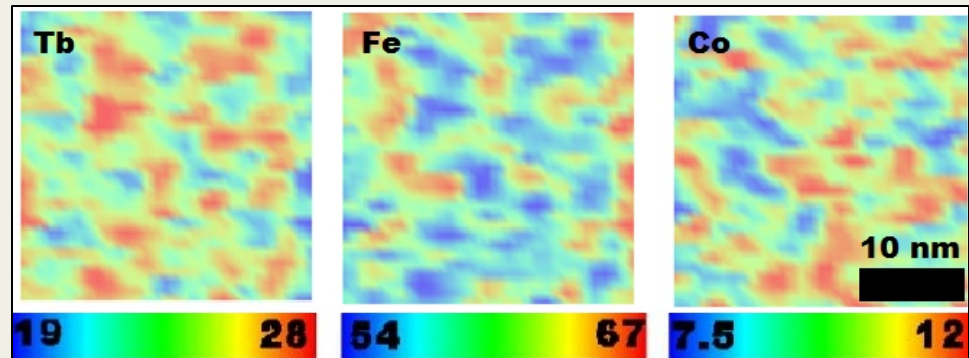
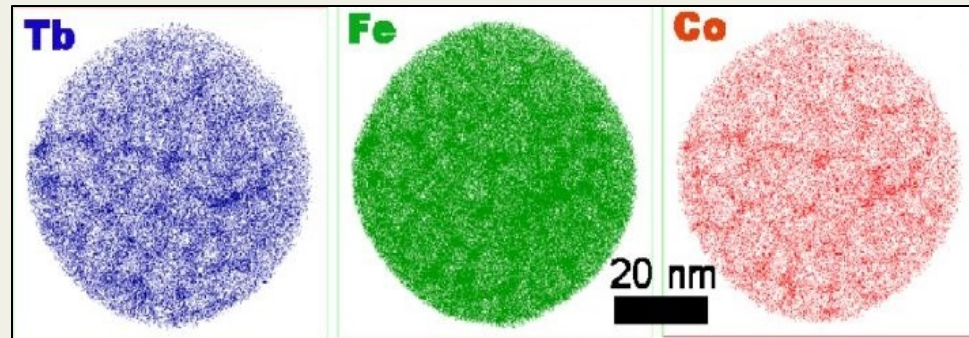
- Non-uniform distribution of all three elements.
- The regions marked with arrows indicate a local depletion in Tb, which directly coincides with an enrichment in Fe



Origin of Exchange Bias in Tb₂₆Fe₆₄Co₁₀ Films

Atomic probe tomography (APT)

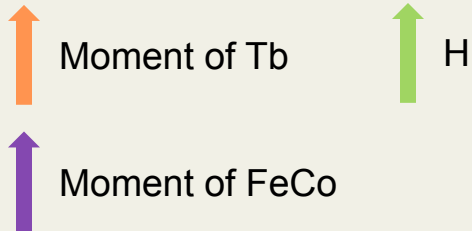
- Tb (blue), Fe (green) and Co (red) distribution along a slice parallel to the film plane
- A network-like segregation of all three elements
- Existence of two compositional phases in amorphous Tb₂₆Fe₆₄Co₁₀ film



Origin of Exchange Bias in Tb₂₆Fe₆₄Co₁₀ Films

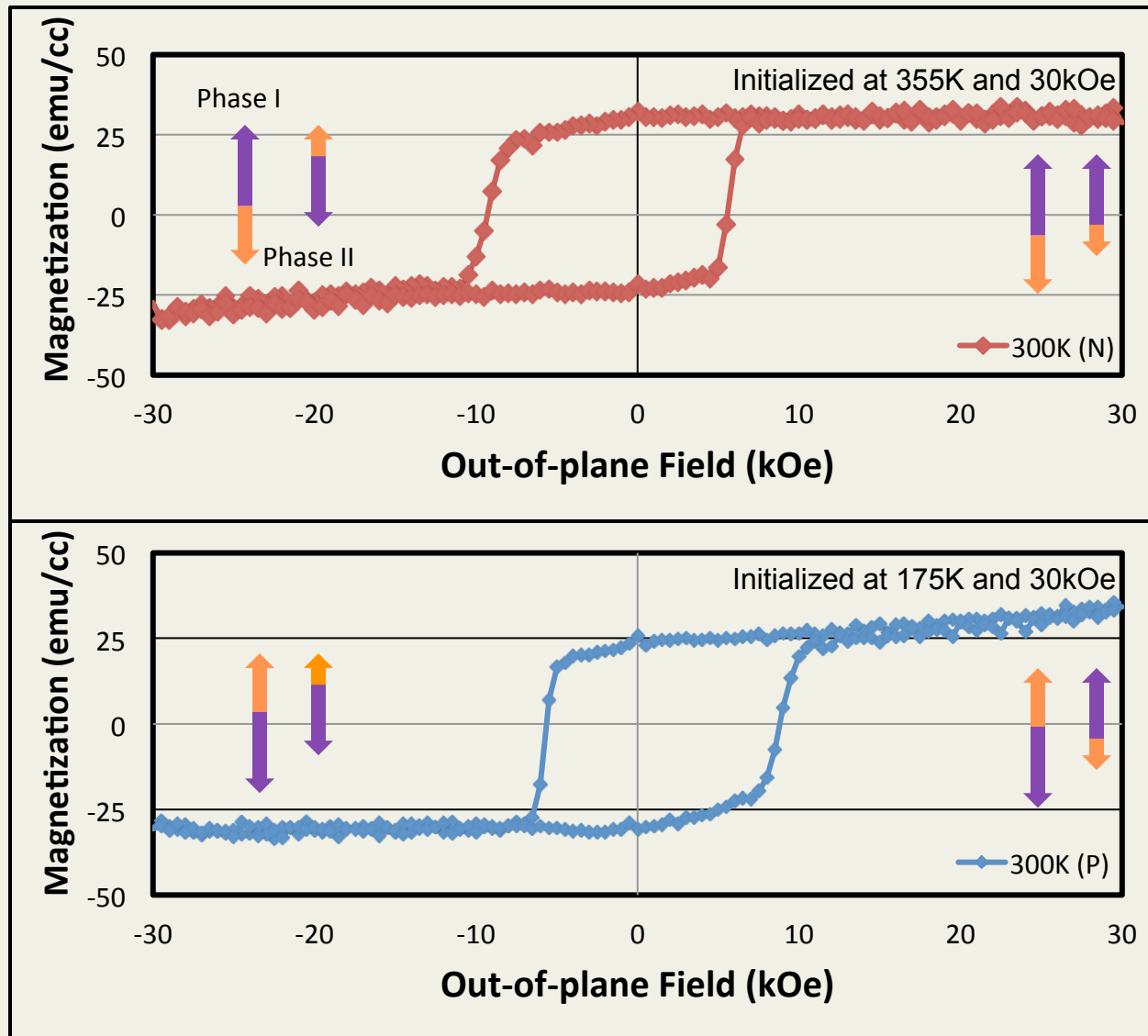
- Two nanoscale amorphous phases on the length scale of 2-5nm are revealed from STEM and APT.
- A Tb-enriched phase (Phase I) is nearly compensated and acts as a fixed layer
- A Tb-depleted phase (Phase II) is far away from compensation and acts as a free layer
- Exchange bias in Tb₂₆Fe₆₄Co₁₀ film originates from the exchange interaction between these two nanoscale amorphous phases

Origin of Exchange Bias in Tb₂₆Fe₆₄Co₁₀ Films



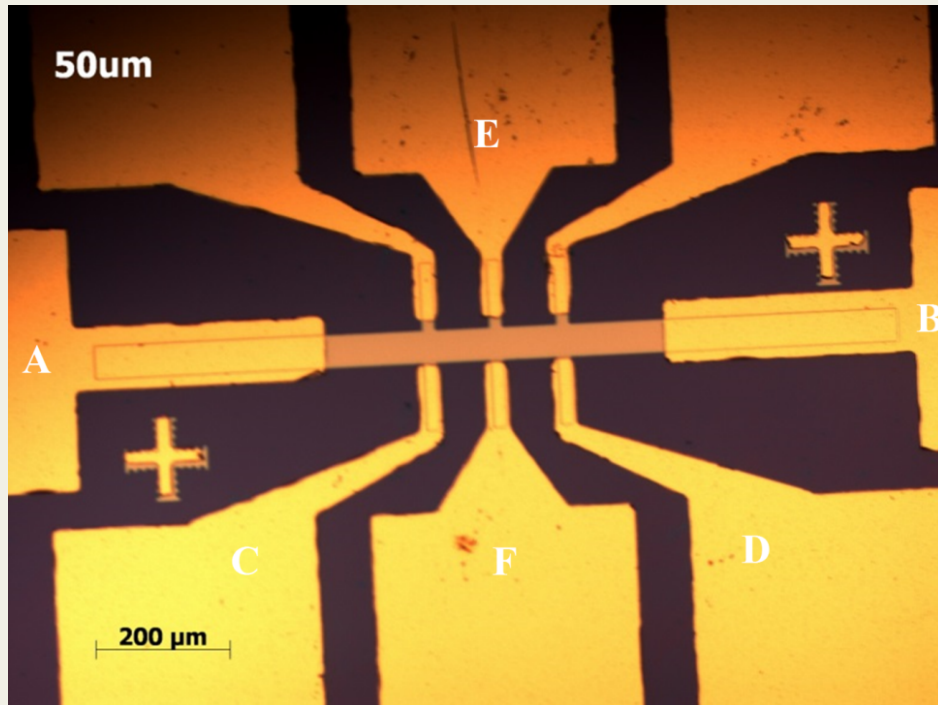
$$M = \phi(M_{\downarrow Tb\uparrow I} + M_{\downarrow FeCo\uparrow I}) + (1-\phi)(M_{\downarrow Tb\uparrow II} + M_{\downarrow FeCo\uparrow II})$$

ϕ is the volume concentration of Phase I



Exchange Bias effect in magneto-transport measurements

Anomalous Hall Effect (AHE) and Magneto-resistance (MR) of $\text{Tb}_{26}\text{Fe}_{64}\text{Co}_{10}$



Current is injected through A and B

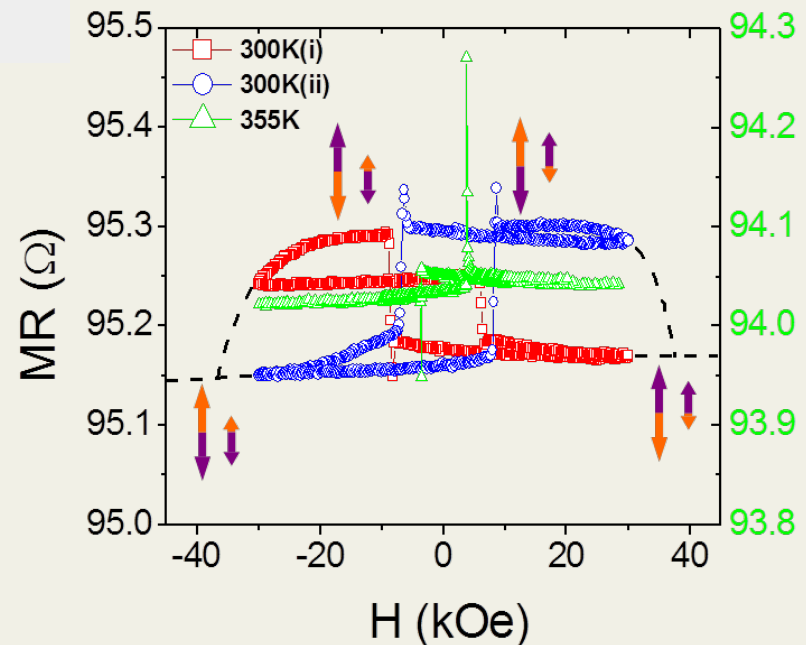
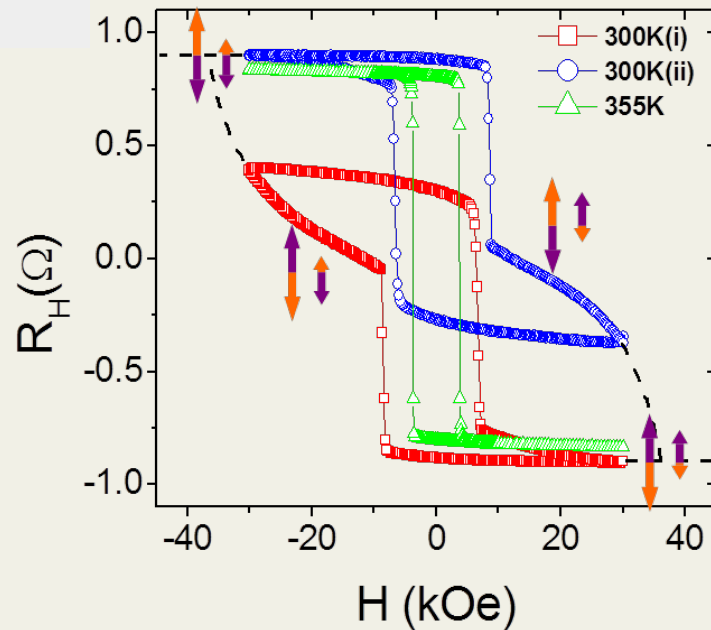
Voltage difference is measured between

EF for AHE

CD for MR

Exchange Bias effect in magneto-transport measurements

Anomalous Hall Effect (AHE) and Magneto-resistance (MR) of $\text{Tb}_{26}\text{Fe}_{64}\text{Co}_{10}$

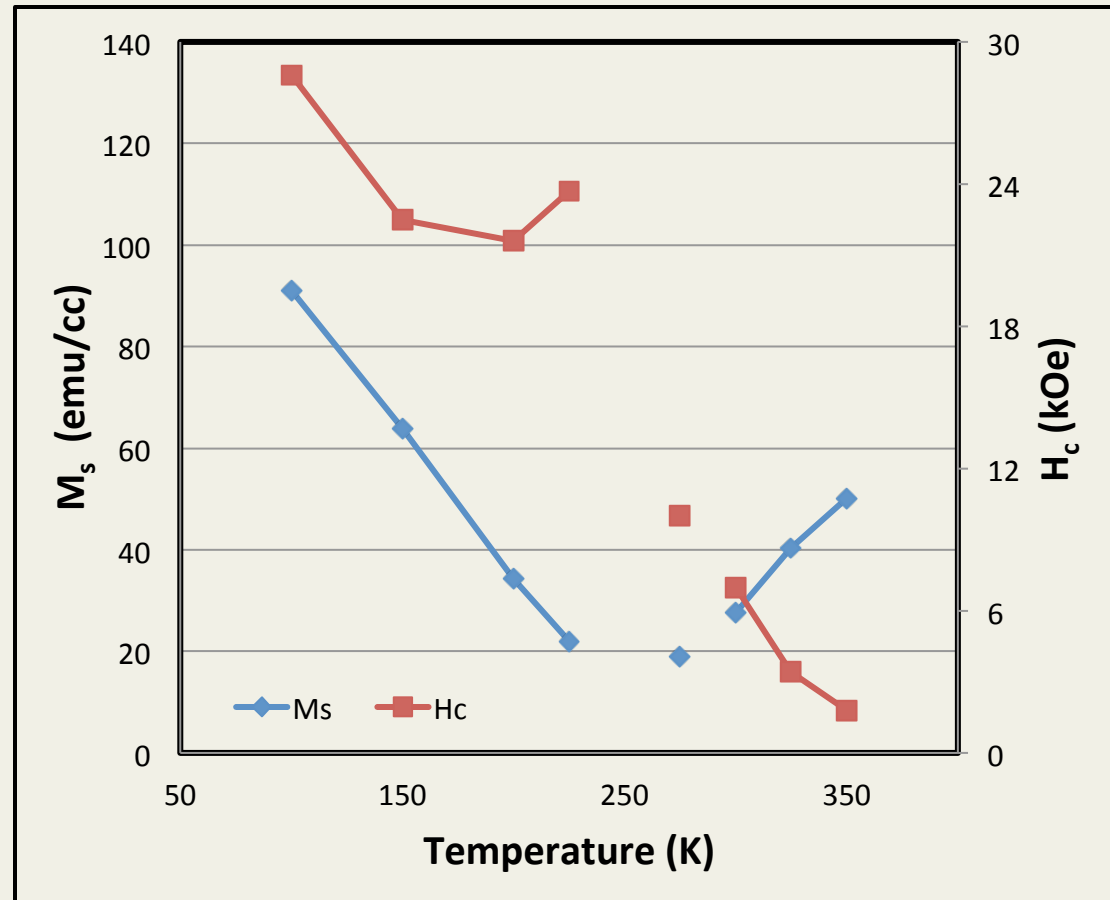


$$R \downarrow H \propto C \uparrow I (R \downarrow Tb \uparrow I M \downarrow Tb \uparrow I + R \downarrow FeCo \uparrow I M \downarrow FeCo \uparrow I) + C \uparrow II (R \downarrow Tb \uparrow II M \downarrow Tb \uparrow II + R \downarrow FeCo \uparrow II M \downarrow FeCo \uparrow II)$$

Bi-stable MR states are revealed at 300K, corresponds to the exchange bias observed in AHE loops.

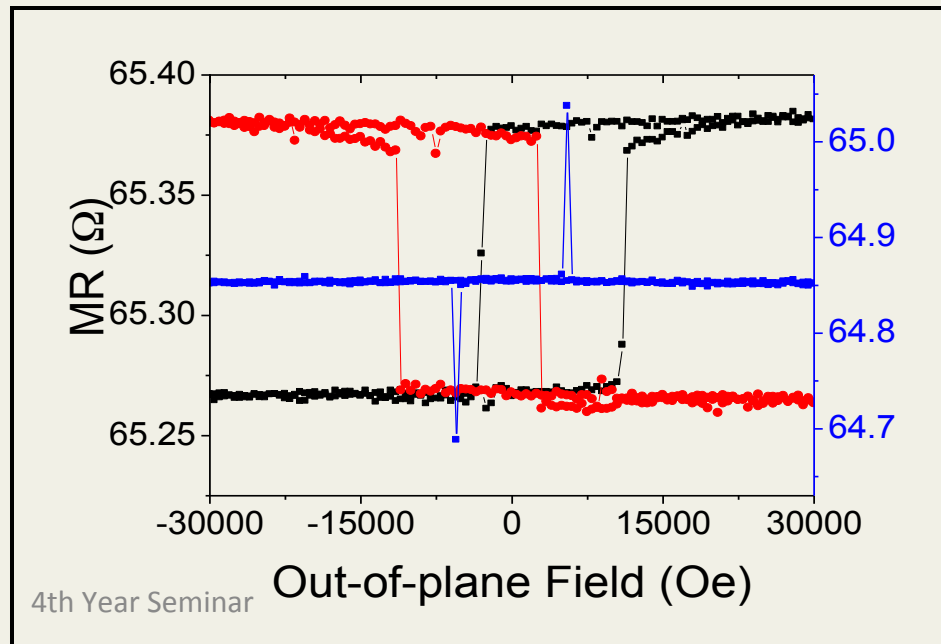
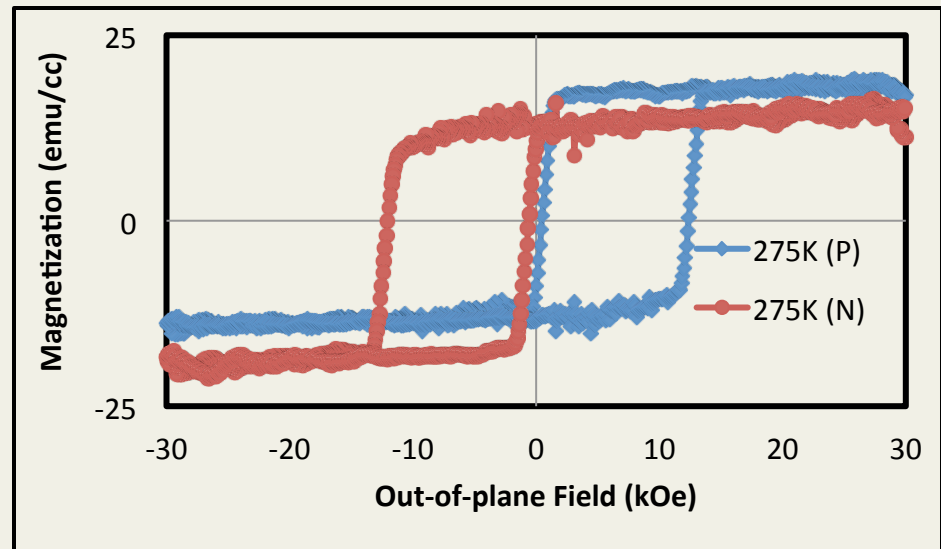
Exchange Bias in Amorphous $\text{Tb}_{20}\text{Sm}_{15}\text{Fe}_{55}\text{Co}_{10}$ Films

- 100nm thick
- $T_{\text{comp}} \sim 250\text{K}$
- PMA



Exchange Bias in Amorphous $\text{Tb}_{20}\text{Sm}_{15}\text{Fe}_{55}\text{Co}_{10}$ Films

- Exchange bias at 275K
- Bistable MR states



Experimental Summary

- Exchange bias and bi-stable magneto-resistance states are uncovered in amorphous TbFeCo and TbSmFeCo films with perpendicular magnetic anisotropy
- Structural analysis revealed two nanoscale amorphous phases with different Tb atomic percentages distributed within the films.
- Exchange anisotropy originates from the exchange interaction between the two amorphous phases

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Magnetic and structural properties of exchange biased TbFeCo

- Micromagnetic Simulations

Two-sublattice, two-phase model.

Landau-Lifshitz-Gilbert Equation

Dynamic of Magnetization M

Landau-Lifshitz-Gilbert (LLG) Equation

$$\frac{dM}{dt} = -\gamma(M \times H_{\text{eff}}) + \alpha/M_s (M \times \frac{dM}{dt})$$

Where γ is the gyromagnetic ratio, and α is the damping factor

Landau-Lifshitz-Gilbert Equation

The Effective Field

$$\mathbf{H}_{\text{eff}} = \mathbf{H}_{\text{Ext}} + \mathbf{H}_{\text{Demag}} + \mathbf{H}_{\text{Ani}} + \mathbf{H}_{\text{Exch}}$$

- External field
- Demagnetization field
- Anisotropy field
- Exchange field

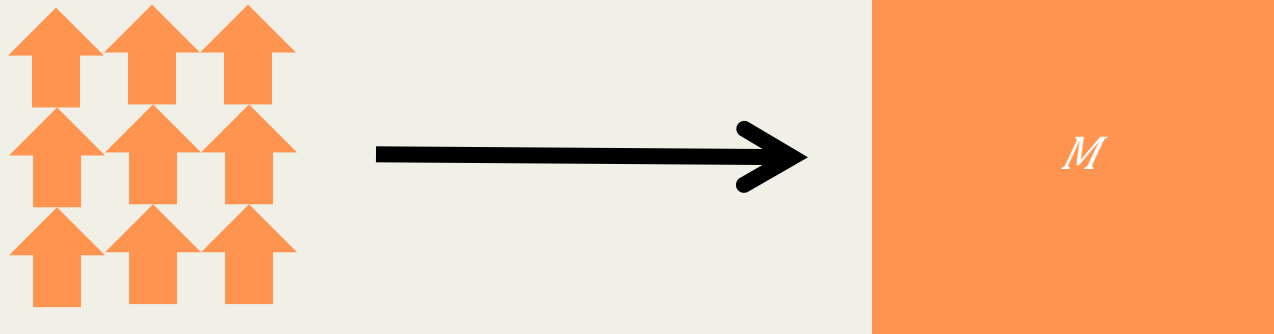
Methods

- Atomistic model
- Micromagnetic model

The Micromagnetic Model

The Continuum Approximation

Multiple spins are grouped together to form a single cell of magnetization.



The Two-Sublattice Model

- Ferrimagnetic
- Tb and FeCo Sublattices
- Two LLG equations for each sublattice

$$\frac{d\mathbf{M}_{\downarrow Tb}}{dt} = -\gamma(\mathbf{M}_{\downarrow Tb} \times \mathbf{H}_{eff\downarrow Tb}) + \alpha/M_{\downarrow s\downarrow Tb} (\mathbf{M}_{\downarrow Tb} \times \frac{d\mathbf{M}_{\downarrow Tb}}{dt})$$

$$\frac{d\mathbf{M}_{\downarrow Fe}}{dt} = -\gamma(\mathbf{M}_{\downarrow Fe} \times \mathbf{H}_{eff\downarrow Fe}) + \alpha/M_{\downarrow s\downarrow Fe} (\mathbf{M}_{\downarrow Fe} \times \frac{d\mathbf{M}_{\downarrow Fe}}{dt})$$

The Two-Sublattice Model

The effective field due to the exchange interaction ($H_{\text{exch}}^{\uparrow}$)

$$H_{\text{exch}}^{\uparrow \text{Tb}} = 2A_{\text{Tb-Tb}} / \mu_0 M_{\text{Tb}} \nabla^2 \mathbf{m}_{\text{Tb}} + 2A_{\text{Tb-Fe}} / \mu_0 M_{\text{Tb}} \nabla^2 \mathbf{m}_{\text{Fe}} + B_{\text{Tb-Fe}} / \mu_0 M_{\text{Tb}} \mathbf{m}_{\text{Fe}}$$

$$H_{\text{exch}}^{\uparrow \text{Fe}} = 2A_{\text{Fe-Fe}} / \mu_0 M_{\text{Fe}} \nabla^2 \mathbf{m}_{\text{Fe}} + 2A_{\text{Fe-Tb}} / \mu_0 M_{\text{Fe}} \nabla^2 \mathbf{m}_{\text{Tb}} + B_{\text{Fe-Tb}} / \mu_0 M_{\text{Fe}} \mathbf{m}_{\text{Tb}}$$

- Neighbor cells from both sublattice
- Same cell from the other sublattice

The Two-Sublattice Model

The effective field due to the exchange interaction (H_{exch})

$$A_{\text{Tb-Tb}} = \frac{1}{4} \frac{J_{\text{Tb-Tb}} S_{\text{Tb}}}{r_{\text{nn}}^2 c_{\text{Tb}} / a^3}$$

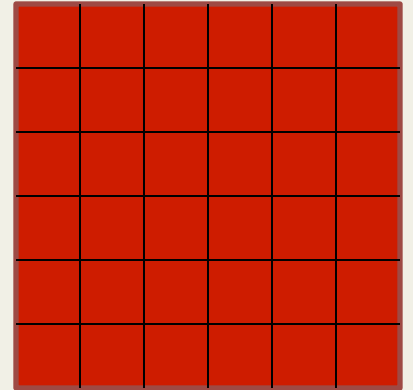
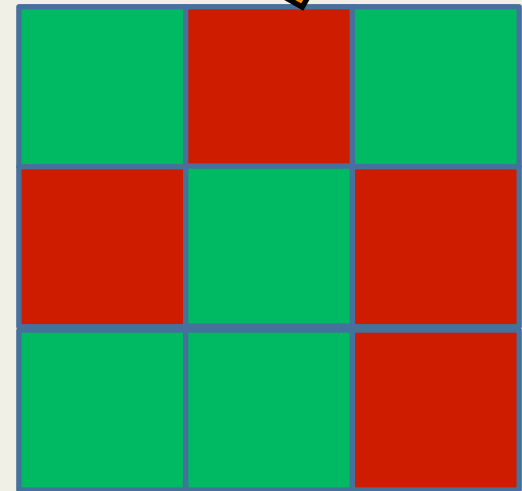
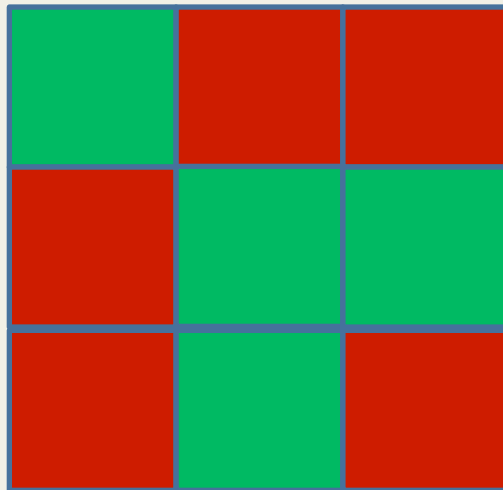
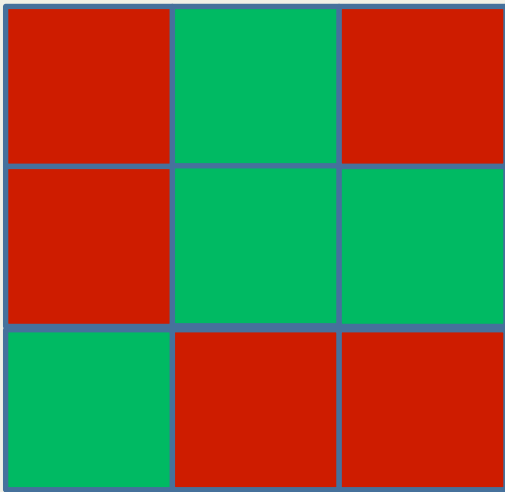
$$A_{\text{Fe-Fe}} = \frac{1}{4} \frac{J_{\text{Fe-Fe}} S_{\text{Fe}}}{r_{\text{nn}}^2 c_{\text{Fe}} / a^3}$$

$$A_{\text{Tb-Fe}} = \frac{1}{4} \frac{J_{\text{Tb-Fe}} S_{\text{Tb}} S_{\text{Fe}}}{r_{\text{nn}}^2 c_{\text{Tb}} / a^3}$$

	Phase I	Phase II
K_{Tb} (J/m ³)	3.4×10^5	1.9×10^5
$A_{\text{Tb-Tb}}$ (J/m)	1.90×10^{-12}	1.21×10^{-12}
$A_{\text{Tb-Fe}}$ (J/m)	-2.43×10^{-12}	-1.87×10^{-12}
$A_{\text{Fe-Fe}}$ (J/m)	1.40×10^{-11}	1.68×10^{-11}
$B_{\text{Tb-Fe}}$ (J/m ³)	-1.43×10^7	-1.09×10^7

The Two-Phase Model

- Two interpenetrating phase
- Phase I (Red) and Phase II (Green) blocks
- 6x6x6 cells in each block
- Distributed throughout the modeling space



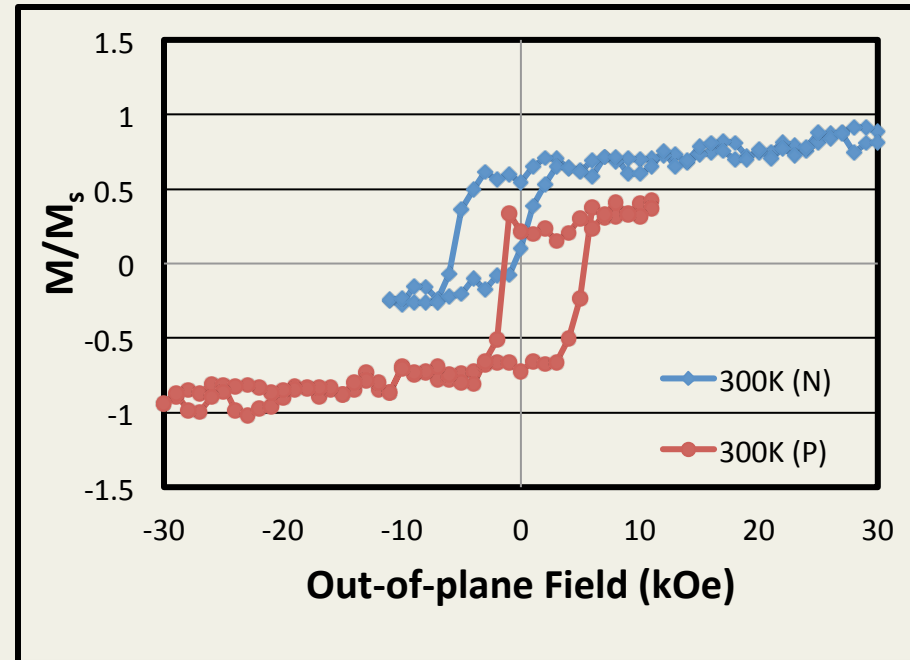
The Two-Phase Model

- Each cell is 0.5nm x 0.5nm x 0.5nm
- Each Phase I and Phase II block is 3nm x 3nm x 3nm
- Each block has 6x6x6 cells (Total 18x18x18 = 5832 cells)
- 27 blocks, 13 Phase I and 14 Phase II blocks
- Finite distance methods based on OOMMF

M. J. Donahue and D. G. Porter, **OOMMF User's Guide, version 1.0**, Interagency Report No. **NISTIR 6376**, National Institute of Standards and Technology, Gaithersburg, MD, 1999 (<http://math.nist.gov/oommf/>).

Simulation Result of TbFeCo

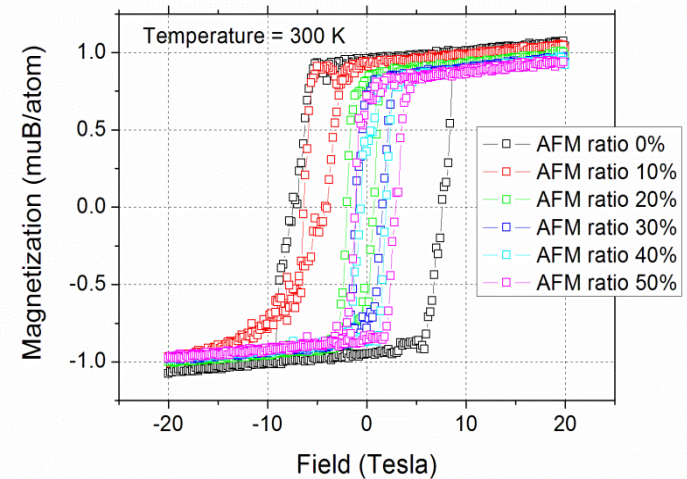
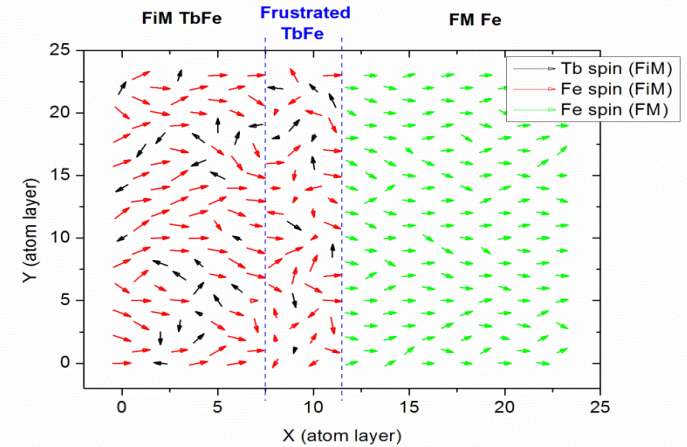
- Positive and negative exchange bias minor loops near T_{comp}
- Positive shift in magnetization accompanied by negative exchange bias
- Negative shift in magnetization accompanied by positive exchange bias



Atomistic Simulations

Courtesy of Xiaopu Li

- Frustrated TbFe region
- Fe-Fe antiferromagnetic coupling



Simulations Summary

Micromagnetic model is employed to study exchange bias in a two-phase magnetic material with ferrimagnets.

Positive and negative exchange bias minor loops are obtained near T_{comp}

This model provides a platform for developing exchange bias materials using ferrimagnets

Summary

Exchange bias and bi-stable magneto-resistance states are revealed in two phase amorphous TbFeCo and TbSmFeCo thin films

A two-phase, two-sublattice micromagnetic model is employed to simulate exchange bias effect in TbFeCo films

Using this study, we can explore various FiM/FM and FiM/FM systems by tuning the composition of FiM phase, and develop desirable EB properties for applications at various temperature

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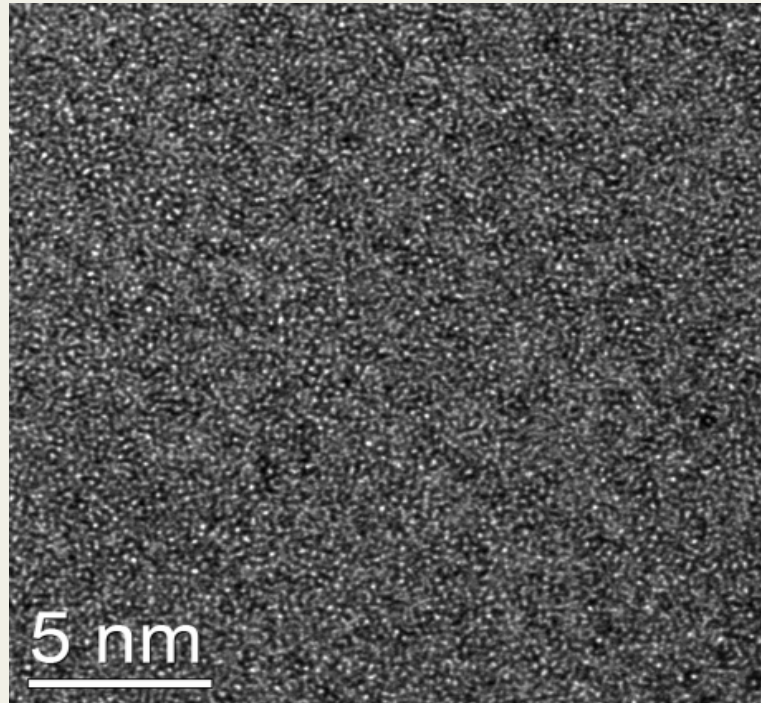


Acknowledgement

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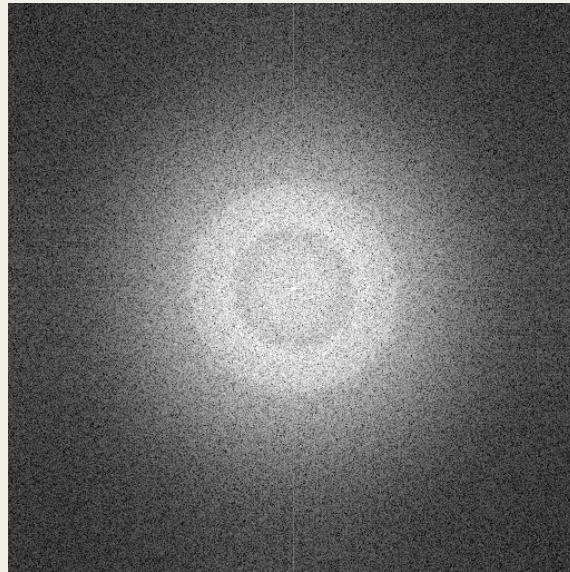


Supplementary



The HRTEM image of the amorphous
 $\text{Tb}_{26}\text{Fe}_{64}\text{Co}_{10}$ thin film by Titan 300 kV

Supplementary



Reduced FFT of the HRTEM

Derivation of effective field due to exchange interaction

$$\mathcal{H}_{\downarrow A} = -1/2 \sum \langle i, j \rangle \uparrow \downarrow J_{\downarrow ij} \mathbf{S}_{\downarrow i} \cdot \mathbf{S}_{\downarrow j} = -1/2 \sum \langle Tb \downarrow i, Tb \downarrow j \rangle \uparrow \downarrow J_{\downarrow Tb-Tb} \mathbf{S}_{\downarrow Tb \downarrow i} \cdot \mathbf{S}_{\downarrow Tb \downarrow j} - 1/2 \sum \langle Fe \downarrow i, Fe \downarrow j \rangle \uparrow \downarrow J_{\downarrow Fe-Fe} \mathbf{S}_{\downarrow Fe \downarrow i} \cdot \mathbf{S}_{\downarrow Fe \downarrow j} - \sum \langle Tb \downarrow i, Fe \downarrow j \rangle \uparrow \downarrow J_{\downarrow Tb-Fe} \mathbf{S}_{\downarrow Tb \downarrow i} \cdot \mathbf{S}_{\downarrow Fe \downarrow j}$$

We can rewrite Tb-Tb and Fe-Fe terms as follow

$$\begin{aligned} \mathcal{H}_{\downarrow Tb-Tb} &= -1/2 J_{\downarrow Tb-Tb} S_{\downarrow Tb}^2 \sum \langle Tb \downarrow i, Tb \downarrow j \rangle \uparrow \downarrow \mathbf{m}_{\downarrow Tb \downarrow i} \cdot \mathbf{m}_{\downarrow Tb \downarrow j} \\ &= const. + 1/4 J_{\downarrow Tb-Tb} S_{\downarrow Tb}^2 \sum \langle Tb \downarrow i, Tb \downarrow j \rangle \uparrow \downarrow (\mathbf{m}_{\downarrow Tb \downarrow i} - \mathbf{m}_{\downarrow Tb \downarrow j})^2 \end{aligned}$$

Using the continuous assumption

$$\mathbf{m}_{\downarrow Tb \downarrow j} \approx \mathbf{m}_{\downarrow Tb \downarrow i} + \mathbf{r}_{\downarrow ij} \cdot \nabla \mathbf{m}_{\downarrow Tb \downarrow i}$$

$$\mathcal{H}_{\downarrow Tb-Tb} \approx 1/4 J_{\downarrow Tb-Tb} S_{\downarrow Tb}^2 \sum \langle Tb \downarrow i, Tb \downarrow j \rangle \uparrow \downarrow (\nabla \mathbf{m}_{\downarrow Tb \downarrow i})^2 = A_{\downarrow Tb-Tb} \int \uparrow \downarrow (\nabla \mathbf{m}_{\downarrow Tb})^2$$

Derivation of effective field due to exchange interaction

The ferrimagnetic (Tb-Fe) term

$$\mathcal{H}_{Tb-Fe} = - \sum \langle Tb \downarrow i, Fe \downarrow j \rangle \uparrow \text{---} J_{Tb-Fe} \mathbf{S}_{Tb \downarrow i} \cdot \mathbf{S}_{Fe \downarrow j} = 1/2 J_{Tb-Fe} S_{Tb} S_{Fe} \sum \langle Tb \downarrow i, Fe \downarrow j \rangle \uparrow \text{---} (\mathbf{m}_{Tb \downarrow i} - \mathbf{m}_{Fe \downarrow j})^2$$

Using the continuous assumption to expand $\mathbf{m}_{Fe \downarrow j}$

$$\mathcal{H}_{Tb-Fe} \approx 1/2 J_{Tb-Fe} S_{Tb} S_{Fe} \sum \langle Tb \downarrow i, Fe \downarrow j \rangle \uparrow \text{---} (\mathbf{m}_{Tb \downarrow i} - \mathbf{m}_{Fe \downarrow i} - \mathbf{r}_{ij} \cdot \nabla \mathbf{m}_{Fe \downarrow i} - 1/2 \mathbf{r}_{ij}^2 \nabla^2 \mathbf{m}_{Fe \downarrow i})^2$$

$$\approx 1/2 J_{Tb-Fe} S_{Tb} S_{Fe} \sum \langle Tb \downarrow i, Fe \downarrow j \rangle \uparrow \text{---} ((\mathbf{m}_{Tb \downarrow i} - \mathbf{m}_{Fe \downarrow i})^2 - 2(\mathbf{m}_{Tb \downarrow i} - \mathbf{m}_{Fe \downarrow i}) \cdot (\mathbf{r}_{ij} \cdot \nabla \mathbf{m}_{Fe \downarrow i}) - (\mathbf{m}_{Tb \downarrow i} - \mathbf{m}_{Fe \downarrow i})^2 \nabla^2 \mathbf{r}_{ij}^2)$$

Derivation of effective field due to exchange interaction

$$\mathcal{H} \downarrow A = \int \uparrow \text{d}\mathbf{r} \left(A \downarrow Fe - Fe (\nabla \mathbf{m} \downarrow Fe)^2 + A \downarrow Tb - Tb (\nabla \mathbf{m} \downarrow Tb)^2 - 2A \downarrow Tb - Fe \mathbf{m} \downarrow Tb \cdot \nabla^2 \mathbf{m} \downarrow Fe - B \downarrow Tb - Fe (\mathbf{m} \downarrow Tb \cdot \mathbf{m} \downarrow Fe) \right) d\uparrow^3 x + 2 \oint \uparrow \text{d}\mathbf{S} \mathbf{m} \downarrow Fe \cdot \nabla \mathbf{m} \downarrow Fe$$

The last term is integrated on the boundary, so the energy density is

$$\mathcal{E} \downarrow A = A \downarrow Fe - Fe (\nabla \mathbf{m} \downarrow Fe)^2 + A \downarrow Tb - Tb (\nabla \mathbf{m} \downarrow Tb)^2 - 2A \downarrow Tb - Fe \mathbf{m} \downarrow Tb \cdot \nabla^2 \mathbf{m} \downarrow Fe - B \downarrow Tb - Fe (\mathbf{m} \downarrow Tb \cdot \mathbf{m} \downarrow Fe)$$

The effective field due to exchange interaction

$$\mathbf{H} \downarrow eff, Tb = -\delta \mathcal{E} \downarrow A / \mu \downarrow 0 M \downarrow s, Tb \delta \mathbf{m} \downarrow Tb = 2 / \mu \downarrow 0 M \downarrow s, Tb A \downarrow Tb - Tb \nabla^2 \mathbf{m} \downarrow Tb + 2 / \mu \downarrow 0$$