

1. **Kerr Modulator:** Suppose an intensity modulator is constructed by placing an isotropic Kerr medium between two polarizers, as in Saleh and Teich Fig 18.1-6. Calculate the output intensity as a function of applied voltage, in terms of the medium length  $\ell$ , medium thickness  $d$ , index of refraction  $n$ , Kerr coefficient  $s$ , and light wavelength  $\lambda_0$ . (If you want to worry about polarization details, assume that the light propagates along  $z$  and is polarized along  $x$ , the electric field is applied along  $x$ , and you are using the  $s_{xxxx}$  Kerr coefficient. The polarizers are at  $\pm 45^\circ$  to  $x$ .)

2. **Biaxial Crystal:** Consider a simple example of light propagating through a biaxial crystal, where  $n_x \neq n_y \neq n_z$ . Suppose the propagation direction of the light is  $\hat{\mathbf{k}} = \sin \theta \hat{\mathbf{x}} + \cos \theta \hat{\mathbf{z}}$ . Determine the directions and effective indices for the two principal polarizations of the light.

3. **Designing a Modulator:** In section 18.1-B (see figure 18.1-5), Saleh and Teich describe how the electro-optic effect can be used in a Mach-Zehnder interferometer to construct an intensity modulator integrated with a fiber-optic system. Design a modulator of this type using the material  $\text{LiNbO}_3$ . Select the orientation of the crystal and the polarization of the guided wave so as to obtain the smallest possible half-wave voltage  $V_\pi$ . Note that for an integrated modulator, it is not easy to apply an electric field along the direction of light propagation, so you can assume a transverse field configuration.

Example 18.2-1 has some discussion of the properties of  $\text{LiNbO}_3$ . However, to be complete, you should consider all possible system configurations, and not just the one discussed in the example.

If the active region has length  $\ell = 1$  mm and width  $d = 5$   $\mu\text{m}$ , and the wavelength  $\lambda_0 = 850$  nm, calculate  $V_\pi$ . The refractive indices for  $\text{LiNbO}_3$  are  $n_o = 2.29$  and  $n_e = 2.17$ , and the non-zero electro-optic coefficients are  $r_{33} = 30.9$  pm/V,  $r_{13} = 8.6$  pm/V,  $r_{22} = 2.4$  pm/V, and  $r_{51} = 28$  pm/V.

4. **Electro-optic Phase Modulation:** The electro-optic effect can also be used for frequency modulation. For example, suppose a  $\text{LiNbO}_3$  crystal of length  $\ell$  is oriented with a laser beam propagating along  $x$  and polarized along  $z$ . An oscillating electric field  $E_1 \cos \Omega t$  is applied along the  $z$  direction. The electric field of the laser itself oscillates as  $E_L = E_0 \exp i(\omega_0 t - kx)$ .

(a) Show that after exiting the crystal, the laser field has a time dependence of  $\exp i(\omega_0 t + \delta \cos \Omega t)$ , and determine  $\delta$ .

(b) If the “instantaneous” frequency of the laser  $\omega(t)$  is defined by

$$\frac{dE_L}{dt} = i\omega(t)E_L,$$

find the range of instantaneous frequencies sampled by the laser output.

(c) In the limit  $\delta \ll 1$ , show that the laser electric field can be expressed as a sum of three components oscillating at  $\omega_0$ ,  $\omega_0 + \Omega$ , and  $\omega_0 - \Omega$ , and find their relative amplitudes.

Frequency modulation can thus be thought of either as a variation of the instantaneous frequency, or as the generation of additional frequency components at  $\omega_0 \pm \Omega$ . (This is a little counter-intuitive when  $\delta$  is small, since the instantaneous frequency never actually equals  $\omega_0 \pm \Omega$ !)

*822 students only:*

5. **Strong Phase Modulation:** In problem 4, if  $\delta$  is not small then the modulated optical field can still be expressed as

$$E_L = E_0 \sum_n A_n(\delta) \exp i(\omega_0 t + n\Omega t).$$

Determine the coefficients  $A_n$ . How large must  $\delta$  be to have equal amplitudes for the “carrier” at  $n = 0$  and the first “sidebands” at  $n = \pm 1$ ? (Hint: the answer involves Bessel functions.)