

02/21/05

Lecture 15

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Optical amplification.

Gain coefficient =

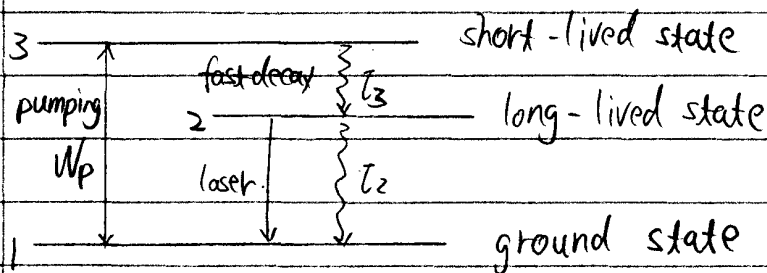
$$g = \frac{\lambda^2}{8\pi t_{sp}} g(\nu) \Delta N$$

$$\Delta N = \text{population inversion} = N_2 - N_1 \frac{g_2}{g_1}$$

Need pumping to achieve inversion

2-level doesn't work.

3-level



Analyze for equal degeneracies:

$$\frac{dN_1}{dt} = -W_p N_1 + W_p N_3 + \frac{1}{t_2} N_2$$

$$\frac{dN_2}{dt} = +\frac{1}{t_3} N_3 - \frac{1}{t_2} N_2$$

$$\frac{dN_3}{dt} = +W_p N_1 - W_p N_3 - \frac{1}{t_3} N_3$$

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Solve in steady state

$$\frac{dN_1}{dt} = \frac{dN_2}{dt} = \frac{dN_3}{dt} = 0$$

$$N_3 = \frac{\tau_3}{\tau_2} N_2$$

$$\text{So } 0 = -W_p N_1 + W_p \frac{\tau_3}{\tau_2} N_2 + \frac{1}{\tau_2} N_2$$

$$N_2 = N_1 \frac{\tau_2 W_p}{1 + \tau_3 W_p}$$

Moreover $N_1 + N_2 + N_3 = N_a$: total atomic density

However, τ_3 is very short, level 3 a negligible steady-state population.

$$\text{So: } N_1 + N_2 \cong N_a$$

$$N_1 \left(1 + \frac{\tau_2 W_p}{1 + \tau_3 W_p} \right) = N_a$$

$$N_1 = N_a \frac{1 + \tau_3 W_p}{1 + (\tau_2 + \tau_3) W_p}$$

$$N_2 = N_a \frac{\tau_2 W_p}{1 + (\tau_2 + \tau_3) W_p}$$

$$\Delta N = N_2 - N_1 = N_a \frac{(\tau_2 - \tau_3) W_p - 1}{1 + (\tau_2 + \tau_3) W_p}$$

usually $\tau_2 \gg \tau_3$

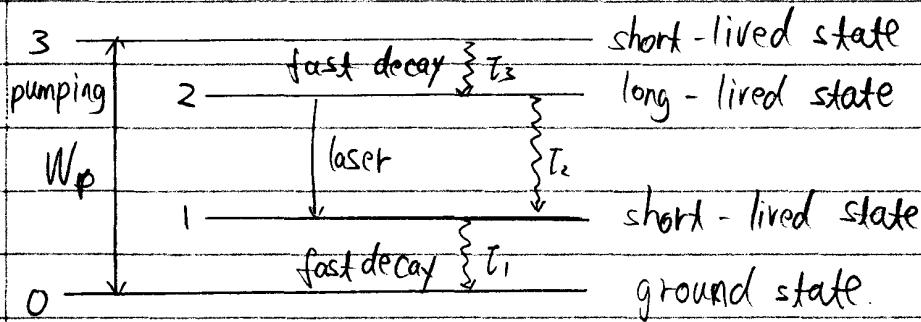
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$$\Delta N = N_a \frac{\tau_2 W_p - 1}{1 + \tau_2 W_p}$$

Population inversion requires $W_p > \frac{1}{\tau_2}$, strong pumping

This works: "3-level" laser.

Even better: 4-level laser.



Again τ_3 is very short

If τ_1 is short, state 1 is naturally empty.
should get inversion for any pumping.

Approximation: assume W_p is weak enough that N_0 is constant. $N_0 \cong N_a$

Valid if $W_p \ll \min \left\{ \frac{1}{\tau_i} \right\}$

Then have
$$\frac{dN_3}{dt} = +W_p N_0 - W_p N_3 - \frac{1}{\tau_3} N_3$$

$$\cong \underbrace{W_p N_a}_{\equiv R} - \frac{1}{\tau_3} N_3$$

$\equiv R$ constant pumping rate.

so $\frac{dN_3}{dt} = R - \frac{1}{\tau_3} N_3 = 0$

$$\frac{dN_2}{dt} = +\frac{1}{\tau_3} N_3 - \frac{1}{\tau_2} N_2 = 0$$

$$\frac{dN_1}{dt} = +\frac{1}{\tau_2} N_2 - \frac{1}{\tau_1} N_1 = 0$$

$$N_3 = R\tau_3, \quad N_2 = R\tau_2, \quad N_1 = R\tau_1$$

$$\Delta N = N_2 - N_1 = R(\tau_2 - \tau_1)$$

get inversion as long as $\tau_2 > \tau_1$

More general, consider degeneracy

$$\Delta N = R(\tau_2 - \frac{g_2}{g_1} \tau_1)$$

$$= W_p N_a (\tau_2 - \frac{g_2}{g_1} \tau_1)$$

get inversion for any rate, as long as $\frac{\tau_2}{g_2} > \frac{\tau_1}{g_1}$

Most lasers use four level scheme.

So if we achieve $\Delta N > 0$, get gain.

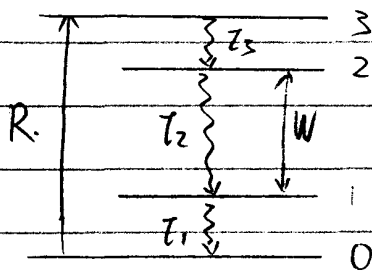
Total gain $G = e^{gd}$ for distance d .

With this gain, get laser lasing, however, gain must stop eventually, otherwise we'd get infinite power out of a laser.

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Effect called saturation.

gain reduced at high intensity,
comes from including laser light in rate equations.



Drive $2 \leftrightarrow 1$ at rate W

write $W_{2 \rightarrow 1} = W g_1$

$W_{1 \rightarrow 2} = W g_2$

$W = \sigma \frac{I}{h\nu}$

Then $\frac{dN_3}{dt} = +R - \frac{1}{\tau_3} N_3 = 0 \Rightarrow N_3 = R\tau_3$

$\frac{dN_2}{dt} = +\frac{1}{\tau_3} N_3 - \frac{1}{\tau_2} N_2 - Wg_1 N_2 + Wg_2 N_1 = 0$

$\frac{dN_1}{dt} = +\frac{1}{\tau_2} N_2 - \frac{1}{\tau_1} N_1 + Wg_1 N_2 - Wg_2 N_1 = 0$

add eqn's for 1 & 2

$R - \frac{1}{\tau_1} N_1 = 0$ so $N_1 = \tau_1 R$

Then $R - (\frac{1}{\tau_2} + Wg_1) N_2 + Wg_2 \tau_1 R = 0$

$N_2 = R \frac{1 + Wg_2 \tau_1}{\frac{1}{\tau_2} + Wg_1} = \tau_2 R \frac{1 + Wg_2 \tau_1}{1 + Wg_1 \tau_2}$

$\Delta N = \tau_2 R \frac{1 + Wg_2 \tau_1}{1 + Wg_1 \tau_2} - \frac{g_2}{g_1} \tau_1 R$

$= R \frac{\tau_2 (1 + Wg_2 \tau_1) - \frac{g_2}{g_1} (1 + Wg_1 \tau_2) \tau_1}{1 + Wg_1 \tau_2}$

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$$\Delta N = R \frac{\left(\tau_2 - \frac{g_2}{g_1} \tau_1\right)}{1 + W g_1 \tau_2}$$

write $\Delta N = \frac{\Delta N_0}{1 + W g_1 \tau_2}$

ΔN_0 = population inversion achieved with
no laser light present
≡ small signal inversion.

Use $W g_1 = W_{2 \rightarrow 1} = \frac{\Gamma^2}{8\pi t_{sp}} g(\nu) \frac{I}{h\nu}$

so $\Delta N = \frac{\Delta N_0}{1 + \frac{\Gamma^2 \tau_2 g(\nu)}{8\pi t_{sp} h\nu} I} \rightarrow 0$ as $I \rightarrow \infty$

Define $I_s(\nu) = \frac{8\pi t_{sp} h\nu}{\Gamma^2 \tau_2 g(\nu)}$

so $\Delta N = \frac{\Delta N_0}{1 + I/I_s}$

and gain $\gamma = \frac{\Gamma^2}{8\pi t_{sp}} g(\nu) \frac{\Delta N_0}{1 + I/I_s} = \frac{\gamma_0}{1 + I/I_s}$

γ_0 = small-signal gain coefficient

when $I = I_s$, gain reduced by factor of 2

